

- 1 → Sand casting → elimination → optimum material.
- 1. crystalline expansion ← atomic structure less rigid structure
2. metallic structure
- bronze → reactivity of copper is less (alloy with copper).

Then Free > Cu^{+2}

At age (by electrical hydrolysis) \Rightarrow Plastic Age (Polymer) and silicon

iron → active but not highly.

Ages because of their reactivity (moving to more reactive)

* leader of polymer SiO_2 SiO_2 SiO_2

• SiO_2 , C , Si

diethyl dichloride resin Polymer *

Plastic → $\xrightarrow{\text{DPI}}$ easy forming.

Plastic → Thermoplastic : can be melted and recycled many times.

Rubber → Thermosets & recycled → irreversible rxn (never get back to its origin)

• ↑ melting & recycling → ↓ quality (الجودة). M.W., viscosity

• Polymer molecular weight for them not the same

new (3500, 4950, 3501) old well degradated degradation

◦ new is rigid, all well tested (جيد) old is soft (مطاط)

◦ Aliphatic (أليفاتي)

◦ recycle for 20% - 25% because there is direct contact

100% SiO_2 , SiO_2 , SiO_2

→ rubber → crushing after cooling (to change from ductile to brittle)

+ glass transition Temp of Polymer $\xrightarrow{\text{Liq}} \rightarrow$ brittle $\xrightarrow{\text{Ductile}}$

$\xrightarrow{\text{Ductile}}$

◦ comatability, fabrication, cost

NO. Chapter #1

7structure \rightarrow properties \rightarrow processing All through characterization.

- \uparrow driving force \uparrow fast cooling \uparrow mis (miss structure)
- \uparrow cooling rate \uparrow hardness no. more hardness forming "recrystallizing" \rightarrow $\text{driven by driving force}$
- \downarrow \rightarrow $\text{Brittle} \leftarrow$ oriented \rightarrow $\text{Ductile} \leftarrow$ non-oriented

8

metals have cloud of electrons

- diamond \rightarrow $\text{covalent} > \text{ionic} > \text{metallic}$ \rightarrow $\text{diamond} < \text{silicon} < \text{aluminum}$
- it will not break because it is ductile (if the same direction of orientation)
- $\text{polymer chains} \rightarrow$ $\text{linear} \rightarrow$ orientation (axial and equatorial)
- $\text{Tungsten carbide} \rightarrow$ orientation (axial and equatorial)
- $\text{Polymers with no colours}$
- $\text{Glass brittle more than glass}$

9

internal structure gives us the property

You make maintenance after candidates.

10 \downarrow room Temp. \downarrow resistivity

Ni & Copper \rightarrow You must see structure and affect of atoms
 Ni on copper, have factors of size, electronegativity,
 valency, structure of atom.

- To be comparable you must put the same structure of the atoms

1112

crystalline \rightarrow not transparent - (adding impurities).

T_{crystal} \uparrow hard to سخون

when colouring we change the internal structure
For marine.

14

Si annealing بروج درج حرارة لها بخلافها نوى معين بنزل درجة

الحرارة (يوجبر طرق أثينا) ازالة

تبسيط المسماة المعدن

ch

chapter # 2

عندما تزداد الحرارة تزداد المسماة بين الماء وتنفلت الوارط (هناك فوار building unit في بحث) (in equilibrium with water)

ask

& receive

NO. Chapter 2

2

الروابط المترتبة على حقيقة وحيطة وفقرة

1 exist \rightarrow There is 2 but we neglected it. (Vice versa)

3

الكتلتين المتصاوِجتين في المجموعات النصفية.

when $P \neq n \rightarrow$ jib's isotope

مودار ألماني

عن ملتقى علماء انماط (فتوى فولن)

5. Atomic weight = proton or neutron.

هناك حاكم استثنائي للقوانين هل الامر وحده فقط المغير وحده

b Proton = neutron > electron

They neglect the weight of e⁻

e^- smaller of the ratios $\approx 10^{-11}$

3. It does just covalent bond - it's not stable ion - 1 δg go δg δg

جے میں بھی اپنے

we can extract from the atom more easier than p.f.r

لأنها ألمت على العواة، وخففت

رسائل طبع نسخ / نسخ الموجة

9

quarks جُمْسَقْبَل

موجوہاتیں

10

الإذنات الممنوحة في سلسلة Shell الجديدة

• distance from center of the atom is fixed. (size of e^-)

١٤

جیوس، اپ، ایجیولی) ہے جس کا لذتیں (وہیں) : ایجیوس، اپ
 (α , β particles and gamma waves) ہے جس کا لذتیں (وہیں)

عندما عالجنا على الأدواء (وزنها) و مسوقة (مدعى من المخازن) 

كذلك يمكن تحديد حجم المخزون من صادرات صناعة الورق (أي) مستهلك الورق كـ

(x-ray) وایمیونیا ایلستنیا (Istene) کالا ایسپلیکنیا (Splenectomy) دارویی

(, iW) ~~of tkr~~ $\leq 10^6$ q.u

100

- huge no. will occupy this volume -
 - spheres the atoms \rightarrow no lost efficiency of packing.
in metals max 73% 25% empty \rightarrow all compact disp.
 - ↑ shells ↑ no. sub shells ↓ energy to take e⁻ \rightarrow CSJ de J SMT

12

13

- valency e⁻ = orbit no. - octet no.

المحارن هي نفس المعمودة التي كلها لها نفس الافتراضات في العدالة حتى لو هنا لا يكترثون به ولذلك يحدوهم المعتقد

- العناصر الظاهرة لا يُؤثر على المعرفة إلا من خلال مكتملة.

كذلك فالنوع الآخر من المركبات التي تؤدي إلى التفاعل هي المركبات التي تمتلك قدرة على إثارة التفاعلات الكيميائية.

رخون کیں ملے ہو گئے۔

$$2 = S \quad 6 = P \quad d = 10$$

Capacity (g) shell ds.

- zero energy loss \rightarrow , D CS -

- قد يُستَدِّعُ لِتَركِيَّةِ غَرِيْبَةِ فِي الْأَكْتَوْنِ عَسَانِ بِرِحْلِ الشَّهِيْدِ مُحَمَّدِ.
- * كُلُّمَا زَهَبَ إِلَيْهِ حَسَبَ السَّكَلِ دَحْبَابُ الْأَكْتَوْنَاتِ طَافَةَ أَعْالَى وَدَحْبَابَ طَافَةَ أَعْلَمَ.
- * أَعْلَمُ بَخْسَرِ (بِرَارِجَةٍ) (نَزْعُ الْأَكْتَوْنِ بِنَ اللَّذَّةِ).

16 Helium zero reactivity

NO. Chapter #2

17

$$\text{Octic no.} = 0.91012(2)$$

Look to total no. of shell not of subshells.

$$\text{Max. octic no.} = 7$$

18

H is not a metal; to be stable H must take an e^-

A

Latest shell is the purpose of making bonds.

Iron is not completed shell it needs $6e^-$.

20

(eg Ar) نسبت الالكترونات في كل طبقات المدار، المدار هو المدار.

Alkaline metals اقل ايجي

Less reactive than metals.

العنصر الذي يعطي القدرة على التفاعل هو العنصر الذي يعطي القدرة على التفاعل.

العنصر الذي يعطي القدرة على التفاعل هو العنصر الذي يعطي القدرة على التفاعل.

العنصر الذي يعطي القدرة على التفاعل هو العنصر الذي يعطي القدرة على التفاعل.

العنصر الذي يعطي القدرة على التفاعل هو العنصر الذي يعطي القدرة على التفاعل.

21

Electropositivity: willing to donate e^- .

2 atoms with approximately electro positive, or -ve \Rightarrow no bonding between these 2 atoms.

23

at the top of periodic table \rightarrow highly electronegativity.

These no. of electronegativity is rounded to one figure.

24

Electronegativity Larger & darker

\Leftarrow it's a relative value

$X_A - X_B$ to know if there is bonding.

If two same elements $E_d(AB)$ is zero

25

\uparrow difference of electronegativity \uparrow probability to make bonds

e.g. NaCl big difference is 0.9 begins similarities

$\sqrt{\text{electron volt}}$ to take dimensionless no.

$$1.602 \times 10^{-19}$$

$$\sqrt{\text{eV}} + \frac{1}{\text{Jev}}$$

بارج و سيلور 0.4 جوا

$$O \ O \ r_1 + r_2$$

Distance between center to center at least must be summation of its radius.

NO.

26 secondary strength $\leq 1^\circ$ neglect if there is 7°
exist in all bonding.

27

metallic > ionic > covalent

الروابط المعدنية، روابط غير موجزة

Joined network / Mad structure

between metals & halogens because of valence e^- .

e.g.

$Na \quad 2,8,1$ shell #3

take empty shell, we don't need it

2. because of different charges.

equilibrium of two forces in bonding : attraction & repulsion.

distance is of minimum energy.

non directional \rightarrow اتجاهية

مترافق

غير مترافق

28 bonding (sharing / accepting e^- permanently)

ask

receive

no. Chapter # 2

30 it is a stable network.

31 repulsion from nucleus (as a result from protons)

- attractive & repulsion \rightarrow functional radius \rightarrow as a center to center not the radius of atom.

- attraction \rightarrow \downarrow distance \rightarrow negatively.

عندما تقترب الذرتين من بعضها البعض ينخفض طاقة الحركة الميكانيكية ويزداد طاقة الجاذبية

لذلك تكون طاقة الجاذبية إيجابية بينما طاقة التبعثر سالبة $r_1 + r_2 = \text{min}$

$L > D$ of one atom

لأنه في ذلك يكون ابعد

distance r

$\frac{dE_N}{dr} = 0$ You can have r equilibrium

بـ \therefore Net E \downarrow \therefore انتقام

32 Ionic bond \rightarrow solid state \therefore جذب كل اجزاء بـ \therefore لاصق

covalent \rightarrow gases

جذب بين ذرات \therefore اروادي

liquid

inert gases (no covalent bond)

instantaneously taking and donating.

covalent \rightarrow اذافنوا بـ \therefore انتقام

ذافنوا بـ \therefore انتقام

\rightarrow Non polar \rightarrow between the same atoms e.g. H_2, \dots

33  movement of two e-

Temporary stability.

38 CO monocarbon monoxide

39 liquids & covalent bond \therefore more than gases

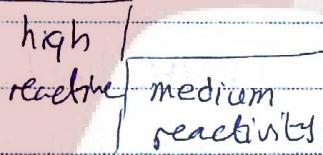
ionic bond \therefore \therefore \therefore

٤٠ - اخ بونية تعمد السباكة مثل تحليل الابعاد مذابة وسائل
 ٨، like dissolves like ٨ يتحول اذا كان يوجد في
 الماء كهربائية (النفحة) ينفكوا اي
 بطلق ابرارهم بل يخفف قلل .



نترات

بونج كلورايد



→ Na needs 7 electrons

2, 8, 1

- Na . بخط في كازم شوين
- Al highly reactive with atmosphere . ينفك كهربائي من التفاعل

• العبار الاول يحتاج الى 8

• الكترونات ضمن دينج ملء

You must fill 5 of P sub shell

٤١ e⁻ & بيسودا ديجيتا الاكتروناه ← من كل لحظة فرقة دولها يوجب
 highly conductive lines

at instant there is stable atom.

في الابونية يجي وبيوج رابطة ايماء على المعنون يعبر، اربط فقط اذكر وانحرفة سارحة .

It is net stability, no one stable at any moment.

الدوار (الدوار) اخفف ما اول

NO. Chapter # 2

40

الوارمدة المعدنية، اشباعه بذرات كبريتات الماء، كبريتات الماء موجودة في الماء.

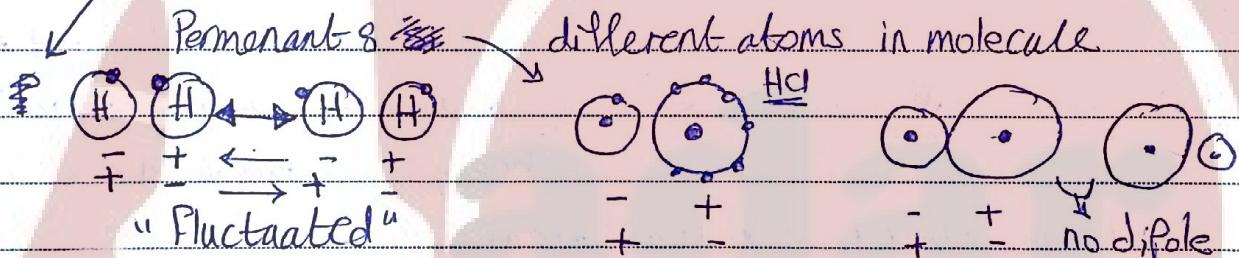
42 except Hg because it is liquid.

- All the layer is not corrosion, Fe corrosion the will be rust \rightarrow Fe_2O_3 + H_2O
- ionic & metallic \rightarrow solid state. the difference is the sliding of P crystalline structure.
- metals \nrightarrow hammer \rightarrow sliding. ionic \Rightarrow brittle bond.

43 Inert gases \rightarrow 2° bonds

- between atoms or usually between molecules
- liquid or molten state of ionic bonds \rightarrow 2° bonds.

Fluctuated \nrightarrow similar atoms of molecules.



will not differ if we here it will differ if we switch

flip the molecule.

\rightarrow no bond between 2 H atoms.

$H_2O \Rightarrow$ hydrogen bonding (same as permanent induced dipole)

45 dissimilar & covalent \rightarrow polar47 considered from 2° bonds (2° weak because between molecules)

water similar to permanent induced dipole.

48 covalent H_2O , \dots small energy.

the less it is.

Ionic forces is polar,

the more it is, will do.

metallic \rightarrow like to ∞

49. melting \rightarrow $\text{رسخ الرؤاج الموجود}$ \rightarrow migrates because of vibration & friction
 \uparrow Temp. \uparrow migration \uparrow #bonds

structure \rightarrow $\text{رسخ الرؤاج الموجود}$ \rightarrow melting because atoms migrate from the structure.

gas \Rightarrow weakest bond. (so there will be distribution).

it is gas because of low boiling point $<$ room temp.

\rightarrow it is $\text{رسخ المعاواد الضعيفة}$.

50. deepest min. energy \rightarrow strongest bonding (\downarrow Peale \rightarrow weaker bonds).
 min. energy \rightarrow $\text{رسخ المعاواد القوية}$

X-axis. \downarrow اقرب اى

y-axis \downarrow ابعاد اى

[\uparrow width \downarrow bonds]

narrow & deep \Rightarrow strong bonds and vice versa

52 \downarrow min. energy \rightarrow more expansion ^(contraction) why ??
 expansion \rightarrow \uparrow distance between atoms \rightarrow الارتفاع
 \rightarrow \downarrow α (deep of min. energy & narrow).

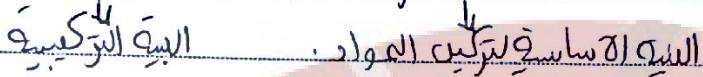
Bring the sheet from elearning.

ask

& receive

NO. Chapter #3

1 molecule building block



ionic \rightarrow crystalline structure lamina \rightarrow chains \rightarrow building block \sim molec. atoms \downarrow

\rightarrow semicrystalline " "

crystalline \rightarrow amorphous

\downarrow melting Temp. no melting Temp. if you \uparrow Temp. there will be degradation
molten state no liquid state impossible to build a structure again -

10/10/2017

2 crystalline \rightarrow 100% (with no space of semicrystalline \rightarrow abus which it not possible amorphous), "Polycrystalline".

3 single crystal \rightarrow one nuclei e.g. diamond. (rare case)

amorphous \rightarrow very small crystal size. we can't consider it as a crystal.

Bulk density (volumetric density) \downarrow \rightarrow \downarrow \rightarrow \downarrow

linear density \downarrow

planar density \downarrow

4 You can't make amorphous \rightarrow crystalline

\uparrow # competitors \downarrow size of crystals.
 $(\uparrow$ # crystals).

$\begin{array}{|c|c|} \hline \text{Big size} & \text{limit no. of chains} \\ \hline \end{array}$

$\begin{array}{|c|c|} \hline \text{Small size} & \\ \hline \end{array}$

nucleating agent to be the center of crystals \rightarrow \downarrow time

long time to become crystal without agent.

nucleation

1. nucleation 2. growth

\uparrow nucleation

\uparrow growth

\downarrow sized

FIVE APPLE

(vice versa).

crystals

crystalli-

- sharp cooling → no enough time to make crystals → small crystals size
- not necessary that crystal is better than amorphous.

Tsize ↑ tensile properties (\downarrow area of surface)

$M_{\text{lin}} \text{ g/cm}^2$

crystals → does not give optical properties

- لاتي عن

- No way to make amorphous → crystalline

nucleation agent "abil" مثل انتشار

b دلالة

amorphous → irregularity in general

الشكل غير منتظم

length of molecule differs

chains, mol. in chain object

- maybe the building block have 1 sphere, but there is no building block with 1 sphere

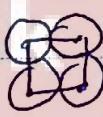
the portion of sphere at the edge = $\frac{1}{8}$ (3 cuts around circle)

Body → full atom → 100% portion

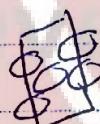
Face → $\frac{1}{2}$ portion

simple → $\frac{1}{8}$ portion

as



Simple cube structure



receive

just

The closest distance = D of atoms.

unit cell → Building block

ذيلها ينبع (الزجاج) من كل جزء

4 mainly structures of building blocks

✓ another materials, may contain all these shapes.
metals.

8. ✓ lattice \rightarrow 1 layer

bonds between all things.

lamina \rightarrow chains (bonds between chains).

repetition / building \leftarrow $\text{w}_{\text{in}} \text{ s}^{\text{in}}$ ✓

pattern lamina \leftarrow $\text{w}_{\text{in}} \text{ c}^{\text{in}}$ ✓

✓ symmetry when putting lines there is mirror image.

NO. Solving sheet #1 (From problems of the book)

11/10/2017

1 a. d shell uncompleted \rightarrow Transition metal.

(11) b. inert gas

c. halogen

d. alkaline earth metal

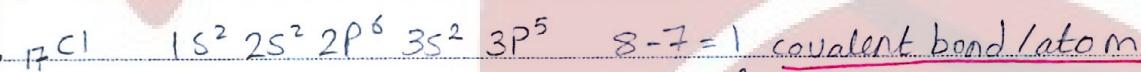
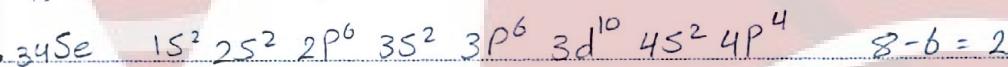
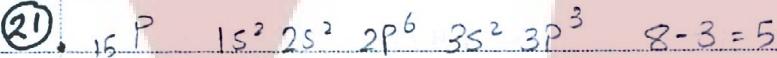
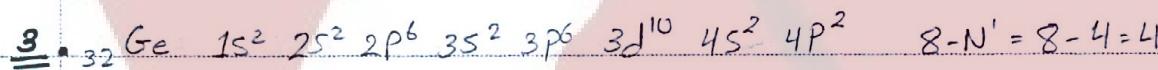
e. transition metal.

f. alkali metal.

$$2 \quad (13) AF = \frac{1}{4\pi \times 8.85 \times 10^{-12}} \times \frac{(1.6 \times 10^{-19})^2 \times 2 \times 1}{(1.6 \times 10^{-9})^2} = 11.8 \times 10^{-10} N$$

covalent shared = 8 - valence

الكترونة
العدد الأعظم



4 $TiO_2 \quad \% IC = (1 - e^{(-0.25[3.5-1.5]^2)}) \times 100\% = 63.2\%$

$ZnTe \quad \% IC = (1 - e^{(-0.25[2.1-1.6]^2)}) \times 100\% = 6.05\%$

$CsCl \quad \% IC = (1 - e^{(-0.25[3-0.7]^2)}) \times 100\% = 73.4\%$

$InSb \quad \% IC = (1 - e^{(-0.25[1.9-1.2]^2)}) \times 100\% = 1.0\%$

$MgCl_2 \quad \% IC = (1 - e^{(-0.25[3.0-1.2]^2)}) \times 100\% = 55.5\%$

5

- (22) 1. metallic 2. covalent (C & H) with some Van der Waals 3. ionic with some secondary bond 4. Xe on \rightarrow inert gas \Rightarrow Van der Waals 5. (copper & tin) \rightarrow metallic covalent 6. covalent (perhaps some Van der Waals) 7. covalent with some ionic.

6 $(14) EN = EA + ER = \frac{-A}{r} + \frac{B}{r^n} = -Ar^{-1} + Br^{-n}$

1. $\frac{dEN}{dr} = Ar^{-2} + -nBr^{-n-1} = \frac{A}{r^2} + \frac{-nB}{r^{n+1}} = 0$

2. $\frac{A}{r^2} = \frac{nB}{r^{n+1}} \quad Ar_0^{n+1} = nBr_0^2 \therefore r_0^2 A = \left(r_0^{n-1} = \frac{nB}{A}\right)^{\frac{1}{n-1}} \quad r_0 = \left(\frac{nB}{A}\right)^{\frac{1}{n-1}} = \left(\frac{A}{nB}\right)^{\frac{1}{n-1}}$

Find value of standard molar enthalpy of atomization

NO.

$$3. E_0 = \frac{-A}{r_0} + \frac{B}{r_0^n} = \frac{-A}{\left(\frac{A}{nB}\right)^{\frac{1}{1-n}}} + \frac{B}{\left(\left(\frac{A}{nB}\right)^{\frac{1}{1-n}}\right)^n} = \frac{-A}{\left(\frac{A}{nB}\right)^{\frac{1}{1-n}}} + \frac{B}{\left(\frac{A}{nB}\right)^{\frac{n}{1-n}}}$$

15 $E_N = EA + ER = -\frac{1.436}{r} + \frac{5.8 \times 10^{-6}}{r^9}$

$$\frac{dE_N}{dr} = \frac{1.436}{r^2} + -52.2 \times 10^{-6} r^{-10} = 0 = 1.436 r^{-2} + -52.2 \times 10^{-6} r_0^{-10}$$

$$(1.436 r_0^{-2} = 52.2 \times 10^{-6} r_0^{-10}) \div 1.436 r_0^{-2}$$

$$1 = 36.35 \times 10^{-6} r_0^{-8} \quad r_0^8 = 36.35 \times 10^{-6} \quad r_0 = 0.279 \text{ nm}$$

$$\rightarrow E_0 = -5.147 + 0.566 = \boxed{4.58 \text{ eV}}$$

NO. Chapter #3

9 * Lattice:

الكتل المعدنية، والمعادن، هي building block في المستوى الجزيئي.

10 * Packed ← same radii atoms

أمثلة على ذلك

• metals → same radii of atoms → more packed

الآن

11 grain boundary, impurities → make polycrystalline

similar amorphous not completely amorphous (grains).

العنصر الأول الذي يدخل في التكوين هو جسم معين يعطيه خصائص.

- in alloy of metals the radii are compatible (no big difference in rad the atom) but in ionic there is big radii.

when there is difference in foreign atom $> 15\%$ $< 15\%$ not compatible
difference it will make

12 simple cube → diagonal is not in touch



identical spaces

not in touch > 8 atoms.

8 atoms in edges, every atoms 3 times of cutting - each atom
every atoms participate in $\frac{1}{8}$ portion -

② still vacant in centers.

corners → 3 times cut Face → Just 1 time cut -

14 atoms participating 9 atoms only.

③ insertion of complete atom at the centers

9 → 5 atoms participating 2 atoms only.

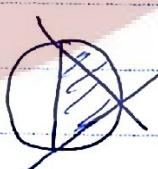
④ 3 atoms support

$7+7+3$ atoms

participating 2

$$\left(\frac{1}{6} \times 6 + \frac{1}{2} \times 1 \right) 2 + 3 = 6 \text{ atoms}$$

$$\frac{1}{3} \times \frac{1}{2} = \frac{1}{6}$$



13 ✓ 83 elements ~~one~~ Just have simple cube structure (1 Just "P")

✓ Packing.F: actual no. of atom exist in certain volume

✓ Low density

14 ✓ coordination number 8-

✓ largest no. of atoms that touches a single atom, Direct touch.

✓ Total no. of equivalent atoms = 1

✓ volume of the atoms = $\frac{4}{3} \pi r^3$

✓ volume of the cube = $a^3 - (2r)^3 = 8r^3$

✓ P.c = $\frac{\text{exist volume of atoms}}{\text{volume of cube}}$

17/10/2017

18



$$16r^2 = a^2 + a^2$$

$$2a^2 = 16r^2$$

$$a^2 = 8r^2$$

$$a = \sqrt{8r}$$

$$a = 2\sqrt{2}r$$

20

Al has low density & less reactivity

✓ coordination 4x3 = 12 (huge)

✓ Face bigger 25%. From simple

23

✓ It's more than BCC more dense

BCC

FCC has higher density, inc
by 200

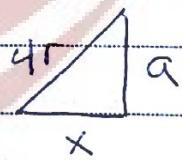
27

✓ missing wire → internal (1) main internal diagonal

if 8r/c

$$x^2 + a^2 = 16r^2$$

$$x^2 = 16r^2 - a^2$$



$$\textcircled{2} \quad x^2 = a^2 + a^2$$

$$16r^2 - a^2 = 2a^2$$

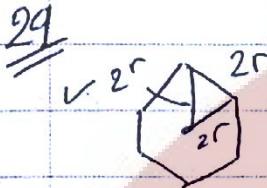
$$3a^2 = 16r^2$$

$$a = \sqrt{\frac{16}{3}} r = \frac{4}{\sqrt{3}} r$$

FIVE APPLE

* ✓ There is a relation between packing efficiency & coordination no.

↑ coordination no. ↑ P.E



عُلُوٌّ سِبْعَةٌ مُكْبَطٌ

[H-W]

height = edge \times (A) coefficient

is 1.63

مُرْجِعٌ

✓ dislema في voidage voids، P.E > 74.05% في يوجد معه 8 coordination $3+6+3 = 12$

as support

✓ B.C.C = hexagonal in coordination & P.E

33 ✓ You must know what is the building block unit.

24/10/2017

35 ✓ because of the packing S of crystalline structure (distance between atoms).

✓ S composites according to the adding materials.

(..., ديك) will obey & rules. ✓

36 You can have large single crystal - عکس ، snowflake - ✓

Polycrystals - عکس crystal lattice، snowflake لایه لایه و متریال افرا - ✓

✓ single crystal \rightarrow The most strong

misregularity عکس جسمانی grain boundary in cells \rightarrow forming of defect. ✓

impurities، stress concentration areas \rightarrow The reason of failure.

37 ✓ metals no single crystalline structure

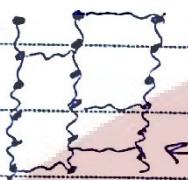
✓ isotropic \rightarrow homogeneous properties (properties are same في اجزاء في الماء)

✓ anisotropic \rightarrow opposite.

building block unit → anisotropic

NO. _____

- ✓ e.g. shopping bags are anisotropic



no of bonds horizontally < vertically

different properties.

single orientation \rightarrow

vertical axis is minimized

longitudinal & transverse

- ✓ isotropic \rightarrow like mesh.

- ✓ anisotropic \rightarrow unidirectional orientation

38 nuclei \rightarrow driving force \rightarrow molecules move \rightarrow growth in 3D \rightarrow

study initially it is a sphere but crystals does imbenign so it will grow on the other directions

- ✓ straight line of the growth are equals, if not it will be ellips and other shapes.

small size & large no.

- ✓ grain boundaries \rightarrow defect \rightarrow sharp cooling \rightarrow grains (smectic)

- ✓ grain boundaries are misregularity, whereas in crystal just 1 will resist tensile force.

(Poly...) \rightarrow يعد لبلورات، تبلورات في طبقات.

bulk is collection of these layers.

we are interested in bulk

(long \rightarrow short) lamina in its self lamella رايخ

39 ✓ may there will be impurities, voltage on grain boundaries.

ذريات وجزيئات

- ✓ on the crystals it self is isotropic

- ✓ No all image \rightarrow anisotropic

40 ✓ high resistance in diagonal (internal) direction, it will differ than edges. because of con.

- ✓ it is anisotropic

✓ building block \rightarrow aniso distance between atoms are different

46 ✓ • Polymorphism more than one crystalline structure in materials.

✓ • e.g. C diamond, buckyball, graphite, am, olas (carbon nanotubes).
graphite: soft (no bonds between the two layers)

① e.g. of metals Fe, ^{1.}perlite, ^{2.}semimrite, ^{3.}an austenite

There is a change \xrightarrow{BCC} often at room temp. or combination

$\xrightarrow{700}$ FCC of them

$\xrightarrow{1400}$ BCC

\uparrow Perlite \rightarrow ductile iron

\downarrow Perlite \uparrow semimrite \rightarrow brittle

49 ✓ a sort of arrangement but there is mismatch (it has certain properties)

↳ \downarrow \uparrow \downarrow \uparrow \downarrow \uparrow \downarrow \uparrow \downarrow

② Polyethylene for shopping bag \rightarrow linear low density \rightarrow crystalline

high $\xrightarrow{=}$
low $\xrightarrow{=}$

cross lengthed \rightarrow not crystalline

50 ✓ imp. For analysis of material (unknown material to know what it is)

③ elemental analysis \rightarrow all y'all \rightarrow e' gawx ipsaw u) jizell \rightarrow building unit

✓ direction from certain point (reference change \rightarrow length & direction will remain be different) (origin) reference point \rightarrow in other \rightarrow direction \rightarrow 1.1.

51 ✓ symmetry will help us in these shapes.

✓ "The idea is the mirror image"

52 ✓ building block units are the same of the material.

✓ we measure according to the building blocks (unit cell R_b^3)

unit \rightarrow def

✓ no exact measurements.

✓ using right hand rule, $y \rightarrow$ $x \rightarrow z$ in positive.

x \rightarrow y \rightarrow z

53 ✓ point atom in structure

✓ you have to define the centroid.

54 ✓ Point 3 number only, موجي 3 عدد direction --> / vertical planes

{ دو افقیں . in

[$\bar{1} \bar{1} 0$] → line $\bar{1} \bar{1} 0$ → point

no -1 → we ~~can't~~ write it $\bar{1} ($ کے لئے اگلے)

(= bar sign shows -ve by convention)

✓ You are free to use the origin.

✓ You care about the fraction. (x y z اسکے)

→ Point nothing direction [] Family directions < >

unit cell

unit cell

in unit cell

unit cell

[100] [200] [300]

[100] [100] [100]

→ Families of direction <100>

same direction (on same axis)

can be described with the same direction.

29/10/2017

55

direction

Point جن سے

✓ we need reference point اپنے

58 ✓ Family directions. کہیں سے کہیں کہیں

✓ can be the same by rotation axis.

e.g. 111 : another یہ اسے family

✓ on 8 building blocks

60 ✓ no fractions پرائی plane & lines, walls, blocks, building blocks.

smallest integer no. → ()

✓ parallel planes → Family of planes.

✓ in planes you are not free to choose reference points

جو کو اپنے چڑھاتے ہوں گے کو اپنے گھر کو لے جائیں کو

one کو اپنے گھر کو لے جائیں

دوسرا بھی, کو اس کو اپنے گھر کو لے جائیں

✓ - plane parallel to line \rightarrow intersect Point = $\infty \Rightarrow \frac{1}{\infty} = 0$

- ✓ avoid to choose reference point make you to expand the plane
- ✓ each figure have one easy ~~one~~ reference point.

✓ Parallel $\rightarrow \infty$

b2 ✓ Family of planes \rightarrow ~~one~~ ∞ points

31 / 10 / 201

b3 ✓ a_1, a_2, a_3 \rightarrow ~~one~~ ∞ points
كل محور ينبع

calculation ~~one~~ ∞ center point.

✓ at least I want 3 points. ✓ fraction on points \rightarrow direction of line

• Take a_1, a_2, a_3 from calculation

✓ $w = 0$ - height

إذا المعاو

a_1 its projected to $ü$ point

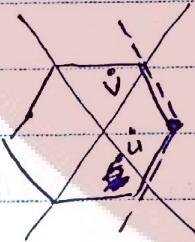
→ standard projection level

a_2 its projected to j point

[Parallel lines] \rightarrow Parallel a_1 / Pass point

Parallel a_2 / "

ask & receive



$$w = w = 0 \quad \text{go to the equation on side } \#65$$

$$j = 1$$

$$ü = 1$$

$$\therefore u = \frac{1}{3} \quad v = \frac{1}{3} \quad t = \frac{\sqrt{2}}{3} \left(\frac{1}{3} + \left(\frac{1}{3} + \frac{1}{3} \right) \right)$$

if Point

$$\left[\begin{array}{ccc} \frac{1}{3} & \frac{1}{3} & \frac{\sqrt{2}}{3} \\ 0 & 0 & 0 \end{array} \right] \Rightarrow \left[\begin{array}{ccc} 1 & 1 & \sqrt{2} \\ 0 & 0 & 0 \end{array} \right]$$

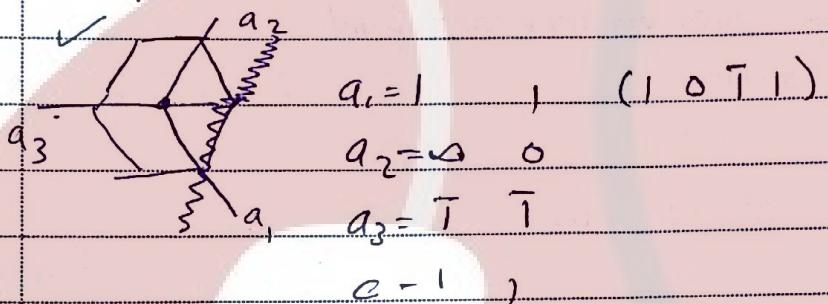
direction

in previous you need 3 points (In point & directions)

NO.

67 You need the four point a_1, a_2, a_3 w/ (c)
• as well as c height.

$\frac{1}{4}$ = $\frac{1}{2}$ circle will $c=1$ lies in plane 111



W, 1920, 15, 11, 120, 11, 20 plane is

68 no. of atoms center \rightarrow #diameters in the direction (#atoms)

1st You must know the building block unit.

2nd radius or diameter of the atom.

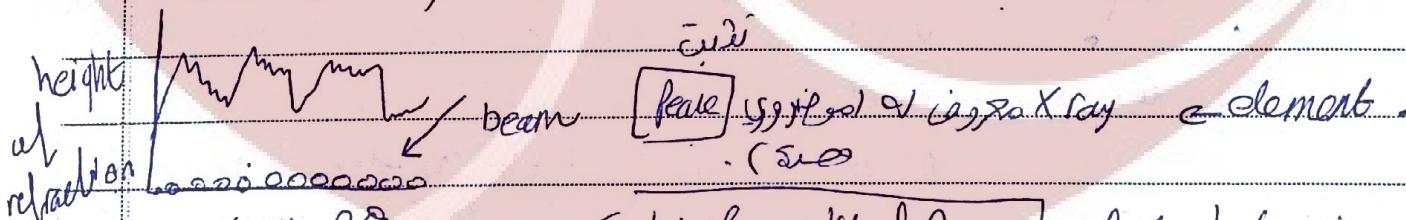
3rd



69 no 100% planar density. (0, 111, 125) 01, 111 carbonyl carbon
zonal zonality

71 refraction of x-ray by different angles
elemental analysis 2/11/2016

The sample may be powder.



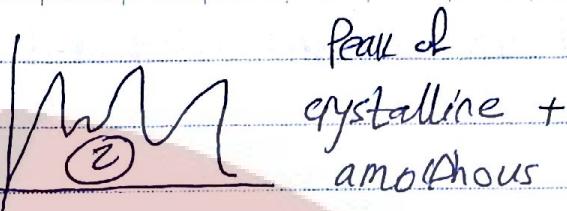
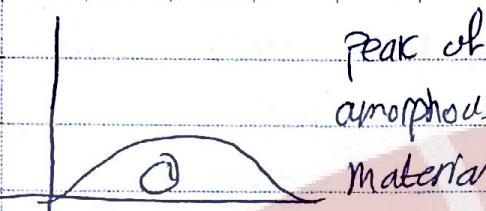
[high width of peak] related to size

of crystals and crystallinity

High \Rightarrow high crystallinity

High \Rightarrow narrow
($\sim 5^{\circ}$)

FIVE APPLE



% Percentage of crystallinity : Area (1) - Area (2)

You can know the types of crystals from reflection of beam

→ All comes from building block units → different refractions -
(X-ray - spectrometer) ...

✓ reflection \leftarrow XRD, all beam \rightarrow

✓ mechanical properties because of the internal structure -

- very brittle, ductile, very ductile . mechanical properties is
✓ \rightarrow interpretation of internal structure - reflection

✓ failure because of creep need ~~not~~ time -

✓ $\cdot \uparrow$ yield \downarrow yield \rightarrow resisting area.

$$\text{Ultimate stress} = \frac{\text{Force}}{\text{Area of resistance}} \quad \cdot \text{well yield } \Rightarrow$$

Yield stress elastic stage

designed by dividing by safety factor

• crystalline, amorphous, ... even though metallic bonds
semicrystalline

! conductivity in amorphous is more than crystalline
(transfer of electrons) grain boundary \rightarrow \downarrow

graphite $>$ mass

no material $\leq 100\%$ pure

FIVE APPLE

ideal structure \rightarrow no bonds

crystalline structure \rightarrow many bonds

End of chapter

5/11/2017

1. in all materials there is misregularity & impurities
 naturally "we"
 what do impurities do, where they will be, why there is no another
 building block of materials? crystalline struc. \rightarrow size limitation
 impurities \rightarrow solute (minor) with low quantity / solvent (major material)
 impurity = foreign material different than the other material
 Limitation of amount of impurities (for solubility) \rightarrow original

solid solution \rightarrow $\text{Ag} \rightarrow$ small areas of agglomeration \rightarrow we avoid this by adding
 impurities, \rightarrow small size will be

- Adding Foreign material, 3 possibilities:

\rightarrow L₁ foreign atom in the building block
 or L₂ in space in building block \rightarrow stress
 or concentration area, there will be distortion
 \rightarrow agglomeration

- There is 4 factors for compatibility

- Ni on Ag \rightarrow isomorphous material

They play \rightarrow because they are compatible

isomorphic second solid \rightarrow solute & solvent are in order and
 morphous phase \rightarrow 1. nucleate because of driving force \rightarrow freezing
 solidification \rightarrow 2. growth (\rightarrow it is still small without growth)
 \rightarrow \uparrow # nuclei \uparrow rate of growth \rightarrow \downarrow small sizes (competition)
 Total # chains constant (it is limited)

when there is impenetrable \rightarrow growth will stop.

By the end of the day there will not be sphere shapes.

but there will be growth on the other directions.

- Defects Point (1 atom) & vacancy (\rightarrow hole)

line defect

plane defect (area defect)

volume defect (IT is the voidage) of impurities -

e.g. air bubbles / agglomeration of impurities / space

solidification \rightarrow rigid chain
NO.

\uparrow Temp. \rightarrow migration & chains \rightarrow molten structure

1. \uparrow Temp. \uparrow Vacancy (migration of atom) \star melting Temp. \rightarrow failure of
~~but~~ \Rightarrow disrupts rigid chains \Rightarrow \leftarrow crystalline structure Temp.
For amorphous structure there is
no melting Temp. but there is
(solid \rightarrow liquid) Temp. for crystalline
and amorphous (softening Temp.)
amorphous \rightarrow no melting / crystallizing
crystalline $\xrightarrow{\text{no}}$ glass transition \Rightarrow

7/11/2017

3 ✓ nucleating agent to have crystal. about it $\&$ nucleation sites ✓
sites \rightarrow

- ✓ \uparrow Temp. (crystalline) \uparrow driving force \uparrow rate of nucleation \uparrow #nucleas
- ✓ \uparrow growth \uparrow not isothermal crystallization
- ✓ if isothermal constant growth rate Time \checkmark straight line
if not no straight line \downarrow slope \rightarrow growth rate
- ✓ \uparrow # grain boundaries \Leftrightarrow \uparrow nucleation
fine crystals \rightarrow high length of grain boundaries

5 ✓ growth rate of nucleus the same \rightarrow straight line boundaries
(they all were born on the same time)

6 ✓ point P
impingement. ✓ different growth rate because of different borns
growth rate of 3 & 2 > 1

7 ✓ same time born but different ~~time~~ growth rate because they are
different crystals.

8 ✓ at the center there are not actual spherical because of
defects (~~defects~~ of impurities) \rightarrow They are impurities & alter chains
rejection \downarrow long diffusion time to form

✓ They are weak area (stress concentration area).
(impurities & grain boundary)

FIVE APPL
less no. of bonds

- 9 • The defects all mechanical properties depends on it.

10 • No 100% structure there will be defects (except single crystals)

 - Properties will respect to another
 - Samples must be the in the same conditions

11 carbon on Fe (perlite, ---)

phase diagram ~~is~~ ^{is} biphasic?

Detection of microfuge structure by phase diagram.

To know about atomic force microscope ---

- 12 1. point → one single atom in the building block.
3. Area → Top view of in 3D → void areas → volume defects

- 13 ✓ tension^{or} compression in vacancy } ① Vacancy
✓ it become stress conc-area.

or self substitution \rightarrow In our] ⑦ salt interstitial
regions like $\text{Ca}_3\text{Al}_2\text{O}_5$
- Al_2O_3

- 17 ✓ any atom \Rightarrow foreign added \rightarrow impurity
✓ size of impurity comparable $\pm 15\%$ of original atom substitution
 "substitutional impurity" $\xrightarrow{\text{size comparable}}$ $\xrightarrow{\text{valence}}$
 "interstitial impurity" Foreign impurity too small $< 15\%$.

e.g. C_8Fe_1
too small
 $\ll 15\%$

- ✓ They all make disturbance because the atoms were in min. energy and distance \Rightarrow "stress conc. area"

- 18' high energy to exist.

✓ Substitutional impurity $\pm 15\%$.

✓ \uparrow Temp. \uparrow vibration (\uparrow energy) \uparrow vacancy leave \downarrow breakage of bond.

• melting temp. physically increasing no. of vacancy \rightarrow failure of structure
most of these atoms not on their locations.

14. possible no. of atoms to be in vacancy = N_v ?

✓ You have to convert temp. to Kelvin.

✓ \uparrow Temp \uparrow exp. N_s is constant $\Rightarrow \uparrow$ Temp $\uparrow N_v$

15. ✓ Q_V every atom needs 0.9 ev to introduce to the structure

✓ vacancy \ggg self interstitial

above certain Temp. there is not enough no. of atoms to hold the structure

2. if the ratio of $\frac{N_s}{N_v} = 1$ that means that we are at molten state

How increase the Temp. calculate the vacancy and the ratio.

then find melting point and compare it with these two points

• small \Rightarrow vacancy \Rightarrow melting point is low
melting is before 1

19. ✓ Solute \rightarrow Impurities

✓ Solvent \rightarrow hoste / major / solvent

• completely free of 100% cost \downarrow \uparrow impurities as well as \downarrow the
any impurities.

✓ Unintentionally \Rightarrow impurities intentional \Rightarrow scuff

• maybe when you change one property the other properties will be
~~deteriorated~~, with limit (\dots \rightarrow this is called limits of solubility)
deteriorated

• You have to do experiments on alloy.

• Alloy is any thing more than 1 component.

• impure \rightarrow alloy

• another element with the metal \rightarrow alloy

✓ the different is fraction of composition.

Any steel & 6 metals. many alloys of steel they differ in composition and different properties

- stainless steel is one
- all the steel additives \rightarrow the additives \rightarrow iron & steel
- silver is the most ductile element
- \rightarrow You can make from it \rightarrow You can make from it

20 ✓ solid solution high compatibility of solute & solvent

✓ no limitation \rightarrow solid solution is the only composition
second phase there will be agglomeration if you add

- structure size, high amount of solute
- there is limitation of solubility

Solubility \rightarrow amount of solute

homogeneous \leftarrow no \leftarrow no \leftarrow no

solubility exist in tables.

✓ substitutional impurities \rightarrow homogeneous \rightarrow maintain crystal structure

✓ interstitial impurities \rightarrow heterogeneous \downarrow

if compatibility in size

solid solution \leftarrow \uparrow solubility \leftarrow substitution \leftarrow 1 \rightarrow 0.98 ✓ ✓

2nd phase \leftarrow \downarrow solubility \leftarrow distortion \leftarrow limited \leftarrow interstitial \leftarrow 1 \rightarrow 1.12 ✓

solid solution solute & solvent

12/11/2017

21 ✓ \uparrow Temp \uparrow solubility \circlearrowright We are talking about molten phase

✓ compatible here is no solubility in solid phase -

22 compatible compatible impurities (with p/c limit $\pm 15\%$)

✓ substitutional impurities not interstitial

Ni minor Si, Cu major Al, Mg, Zn, Cr, Li, Ti
almost the 4 factors are compatible

23 complet solubility ← مُوَسِّط يتحققوا كلّيًّا بحالٍ من الحالات التي تتحققوا في الماء.

✓ We don't expect 100% solubilities.

✓ If there is high electronegativity there will be an ionic bond. $\text{Na}^{+}\text{Cl}^{-}$
Valency high just for the Solute. (valency solute > solvent).

24 Ag & Al ±15 ✓

Ag & Al Al: less Al: high
1. both comparable 2. same structure 3. Ag: higher 4. Ag: lower
Both partial solubility [Al] answer.

$$\checkmark \boxed{2} \frac{1.2n-Cu}{Cu} \quad Z_n: 9.225 \checkmark \quad 2. \alpha \quad 3. 1.6 \checkmark \quad 4. 2 \leq \alpha \\ Al: 11.972 \alpha \quad \checkmark \quad 1.5 \alpha \quad 3 \cancel{\alpha} \quad \checkmark$$

[AI] answer

because there is limitation in the location -

• interstitial impurities does not exceed 10% percent.

25 interstitial impurity

No. Vacancy is huge There is a large substitution distortion.

26 ✓ nature & the structure of solvent (dependence) : e.g.: on BCC is easier than FCC.

✓ HCP of Faces > BCC > FCC

✓ >10% is not preferable \rightarrow ↑ stress \rightarrow ↑ probability of failure

28 ✓ most of alloys more than 2 elements
in order to know the weight of each element ✓ IMP.
 \rightarrow mass \rightarrow mole fraction

weight is more used \rightarrow dotell law^s industrially but science mole fraction

weight is more used \rightarrow do full legal industrially but science mole fraction never ever write mole fraction for flow sheet -

30 edge defect \rightarrow linear defect ✓ dislocation ایزو \rightarrow shifting of layers ✓
screen defect \rightarrow shifting of layers ✓

Linear & screw mixture of dislocation $b \neq g$, $g \cdot b = 0$

- 3) ✓ volume, mass or constant applied force, \rightarrow length changes
 ✓ not necessarily length are exposed to same magnitude of force
 ✓ the weaker deformation layer has deformation -
 ✓ Sliding of layers because of extension of bonds between layers.

elastic behavior \rightarrow small \rightarrow large \rightarrow small \rightarrow original shape

Then \rightarrow plastic deformation

\rightarrow elastic & it return to its original shape. Fully recoverable deformation (elasticity differs between materials). e.g. rubber (high elastic/tg)

\rightarrow plastic & permanent deformation

unrecoverable. Then net \rightarrow recoverable \rightarrow permanent elongation ($\frac{\Delta L}{L}$) or by reduction of cross section area strain $\Delta \{ \frac{1}{L} \}$

\uparrow permanent strain \uparrow deformation

• Forces - longitudinal axes

\searrow shearing \rightarrow on axes

\hookrightarrow it is creep as a layer

line edge screw as structure

✓ = actual image combination between edge & screw

14/11/2017

✓ = deformation: permanent ~~&~~ dislocation (plastic region) (change in struc.)

- 2 stresses \rightarrow ultimate

yield stress (less than ultimate)

* stress = force / cross sectional area resisting the force

32 ✓ difference between edge & screw &

الذارى موجة ورقة بـ

✓ Burger's vector (You must know the dislocation line)

هذا موجة ذارى

deformation
line ازاجة
line

لذلك ينبع من موجة ذارى ازاجة بـ

* Region near line of dislocation have the largest displacement

- line of dislocation: deformation field is large near the dislocation

33 ✓ b has magnitude \rightarrow There is dislocation

(والموجة تختلف في كل مكان) كم هو

لها ازاجة ازاجة

40 ✓ screw & helical, look at the top view

كما ازاجة الموجة

✓ according to the applied shear there is min. max. dislocation

(there is graduality in displacement)

- mixture of edge & screw

dislocation in side view of the metals.

44 - You can see it by microscope by microtoming! (taking

16/11/2017

layers of the material to see the internal view). Then you do imagination for 3D structure

✓ it not only screw neither edge.

- But you have ductile material you freeze it in order not to scratch it when taking layers. e.g. CO_2 , N_2 it will be converted to brittle. sometimes you adjust the surface by chemical materials.

46 ✓ impurities & chains / grain boundaries ~~stress conc.~~
Area of defects. it is not line but surface

thickness is negligible 3D-D 2D

✓ if there is a large defect it may be volume defects not surface.

✓ \downarrow size of crystals \uparrow grain boundaries \uparrow area defects

✓ but not stress conc. area because the rest is homogeneous

ذارى موجة ازاجة

FIVE APPLE

stress conc. area \leftarrow rest, الذارى

① Slow cooling / isothermal

\uparrow size \rightarrow defect but heterogeneous \rightarrow stress conc-area

\rightarrow in industry is not for short time

- You must make isothermal at high Temp. to have large size \rightarrow long time \rightarrow 0.2×10^3 to 0.25×10^3

- in industry \rightarrow small grains not crystals (no growth occurs)

\hookrightarrow "smallest str." \rightarrow very high cooling rate. Small size

\cancel{ut} because the change of orientations of lamellae

② quick cooling \rightarrow no. of crystals \rightarrow few chains \rightarrow high competition.

\rightarrow You may see less no. of bonds between crystals

Vacancy,
agglomeration.

\rightarrow grain boundaries less strength of bonds but other is bonds.
(Few no. of di-bonds).

49 - voidage as an air bubble in glass

- 3 dimensions can be noticeable (thickness is considerable)

- if uniform body \rightarrow same cross sectional area \rightarrow 1 magnitude of stress

Tension

100KN

if not uniform \rightarrow stress conc-area $\uparrow A \downarrow$ stress

- I want as large as possible area. \rightarrow if

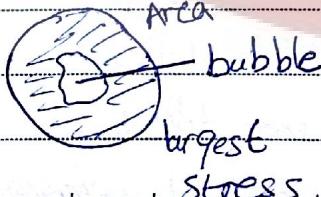
stress = applied force

resistance area \rightarrow the smallest area

$$\text{e.g. } \frac{100 \text{ KN}}{0.1 \text{ m}^2}$$

first region
failure

no uniform
stress.



the voidage
make stress
conc-area

volume defect

⇒ maybe as a result of manufacturing, water vapor, agglomeration of impurities, or impurities not on the structure of the solvent

↖ solute ↖ agglomeration
2nd phase

segregation →

↖ conductivity → if you have voidage or other structure will make discontinuity of electrons.
e.g.: graphite in Fe

50

↖ Atoms at any Temp. have vibration (except at very low Temp.)

⇒ ↑ Temp. ↑ vibration (because of vacancy) → ↑ migration of atoms.

↳ ↗

↑ Tension on the bond (there will be ↑ fatigue)

↖ (Tension & compression due to vibration will cause bonds to relax & will ↑ frequency of failure. This is because of fatigue.)

e.g. on circuit board (the wire inside)

Thermal stress ← vibration

like Applied Force (Tension, compression)

End of Chapter #4

ask

receive

"Mechanical Properties"

- ✓ it is by experiments; this experiments is standard (standard procedure) ~~Fabrication~~ ~~size~~ ~~size~~ ~~size~~ ~~size~~ ~~size~~
- Also, Procedure of the test.
- The result must be "in agreement" with a certain tolerance.
- You must know how to interpolate the curve -
interpolate

2 - Testing for standards for dimensions & procedure -

19/11/2017

- ✓ some materials have elastic region only.

3 : ~~Seilling opposite to external force~~

- strain: ~~all in one~~ deformation

- ✓ whatever the force applied there will be strain but not permanent.

- stress \rightarrow extension \rightarrow Failure \leftarrow strong bonds & brittle.

- linear relation, constant slope -

- if there is elastic + plastic \leftarrow elastic but not linear

For rubber

- ✓ elastic is reversible process.

4 ✓ Force is increased \rightarrow more separation between layers (to make mass is constant elongation) \rightarrow thinner cross section

$L_F - L_i \rightarrow$ extent extension ΔL

- ✓ permanent deformation because of sliding (there is sliding and extension), the matter reorganize it self can return

- * elastic is reversible & plastic remains.

- modulus of elasticity can't be used just in elastic region. ("hook's law")

linear relation between stress & strain

^{+ve} ↑ ^{-ve} ↓ NO.
✓ Tensile & compression → same definition the different is the sign

✓ Plastic & no way to recover the deformation -

5 ✓ Tensile force & Applied force + resisting Across

✓ Tensile stress ← outward or longitudinal applied force is equivalent to longitudinal force.

✓ - or You can put the name instead of sign

↙ ΔL tensile the → Pameber / compression vice versa -

↪ applied force 90° with surface → no shear stress

✓ - Shear → applied force not + on surface → vertically → tensile
↘ horizontally → shear

✓ - Tangential Force → shear stress.

✓ Tensile & shear → same definition.

7 • any force on any surface base

✓ max. stress on min. cross sectional area

8 Liquid propane gas + gas

stress ← ; ball & bowl

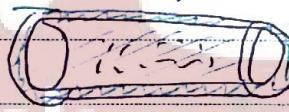
Diameter is being given

↓ liquid → other volume filled with gas.

* how many stresses do we have in pressurized vessel?

Area

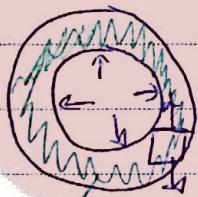
for 6H



• gas on wall : compression everywhere -

1. gas on the ends : tension σ_L (longitudinal stress)

cross sectional area



2. $5h$ (hoop stress)

$6L + 6h$

3. compressive stress on the wall

Area for $6L$

min. thickness

* hydrostatic pressure --- applied, applied etc

design for columns or structures

max. stress →
max. thickness ↓

FIVE APPLE

9 ✓ We measure & deformation by strain.

- $\Delta L/L_0$ variation in length \rightarrow yield stress

- $\Delta D/D_0$ variation of diameter

Across sec. will give the depth of

- no elongation and inflation at the same time

↑ longitudinal stress in compression (shrinkage)

- elongation with lateral

✓ lateral strain = 0.3 for metals ν : Poisson's ratio

longitudinal strain $b_{\text{long.}} > b_{\text{lateral}}$

For metals $0.1 < \nu < 0.3$

- shear deformation of angle "shear strain angle θ "

θ almost small they take tan

10 lower, upper yield point / toughness / modulus of

elasticity - all from tensile or stress strain test.

• جعله

✓ the two ends hexagonal to \rightarrow target \rightarrow sand paper

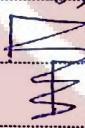
Jawas Jawas Jawas Jawas sand paper

✓ gauge length must be of uniform cross sectional area and it is the min. cross sectional area.

✓ At the ends the angle is curved (ellipse) not 90°



no graduation



nicely Test of this

gradually decreasing

max & min area. in stress conc. application

دليلاً (Pellet) \rightarrow ; lots

- Zero displacement at the initial points to calculate ΔL or instant $\Delta L/L$ strain force

- Force is hydraulic pump
- reading for force (by load cell) and ΔL (by extensometer)
- ↙ not all the materials make failure.
- $\sigma = \frac{F}{A_0}$ (engineering stress)

L_0, A_0 is known

$$[KN] F \quad | \quad \Delta L [mm] \quad | \quad F/A_0 = \sigma \quad | \quad \text{strain} (\Delta L/L_0) \text{ unitless}$$

data collected $\sigma = F/A_{\text{inst}}$

why A_0 ?

✓ engineering stress strain curve F/A_0 (Just one transducer).

True stress strain curve $(F/A)_{\text{instant}}$

I want two transducers (For diameter & variation of length)

reduct. \rightarrow just using one is giving ability to go up to 28 mm
of area

- stress & strain ratio is constant \rightarrow You can determine Area of elastic range \rightarrow they are proportional

✓ magnitude of E is high because ϵ is low. (low variation of ΔL)
compared with σ .

(high Force against small area)

E in mega Paskal (110×10^9) in table 110 Just and above 10^9

✓ reduction is normal to applied force (extension ΔL) & reduction
of width & thickness) \rightarrow small dsiv over

✓ \rightarrow (longitudinal) and (lateral) \rightarrow normal stress strain - longitudinal
answering lateral strain.

✓ Just in elastic region

reduction = $\frac{1}{3}$ extension

All things we are talking about in elastic region.

NO. _____

Expansion El - ve ε + ve ν + ve

compression El + ve ε - ve ν + ve

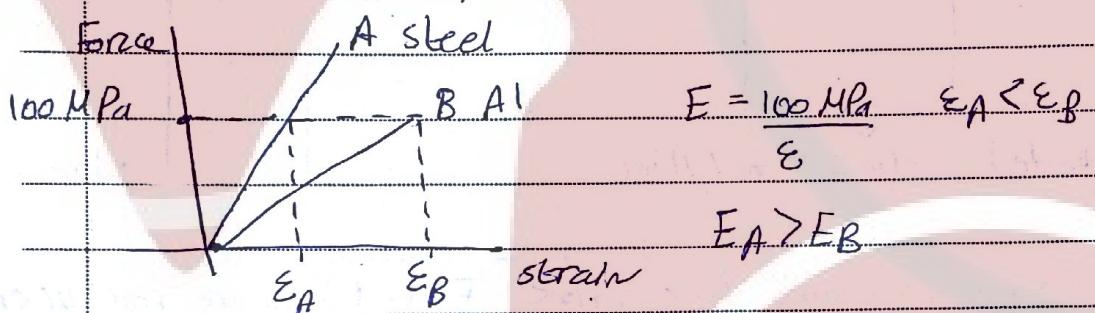
big jump to do failure or yield at $\nu = 1$

ν is unitless

13 ✓↑ brittle, more resistance, ston stronger bonds

✓↑ resistance to force

✓↑ strain ↓ strength of bonds



- ↑ response of νE

✓ line of linear proportionality near y axis ↑ E ↑ bonds

14

(coupled)

twisting Point B is fixed in the same position

Point A change its position

elastic \leftrightarrow b2 A \rightarrow 2, 1, 3

Deformation recovered - elastic range

unrecovered (permanent) - plastic

deformation by α angle = shear strain \rightarrow shear stress

✓ what is the area, solid or hollow?

✓ rigidity \propto elasticity \propto ν

23/11/2017

15 - metals \rightarrow strong bonds \rightarrow high hardness

✓ Penetration \rightarrow small area

✓ When you want to test a material you must use a harder material otherwise the thing will be opposite.

$$\text{16} \quad \begin{array}{l} \text{① stress} = \frac{\text{force}}{A} \quad \text{② strain} = \frac{\Delta L}{L_0} \quad \text{③ Poisson} < 1 = - \frac{\text{latent}}{\text{normal}} \end{array}$$

$$\text{④ Hooke's law Just in elastic region } E = \frac{F}{\epsilon}$$

$$-\text{Derivation of } S = \frac{FL_0}{E A_0} \Rightarrow S = \frac{F}{E} = \frac{F/A_0}{E} = \frac{\Delta L}{L_0} \quad \Delta L = \frac{FL_0}{A_0 E}$$

$$S = \frac{F}{A_0} \quad \epsilon = \frac{\Delta L}{L_0} \quad E = \frac{F}{\epsilon} \quad \left. \right\} \quad E = \frac{F/A_0}{\Delta L/L_0}$$

$$S = -\frac{\epsilon L}{\epsilon} \sim DD/D_0$$

✓ Torsion \Rightarrow by σ_{xy}

Solid or hollow bars will obey it.

✓ G $\% \text{ modulus of rigidity}$, you can calculate it from another modulus.

IT is unrecoverable extension.

✓ end linear proportionality

✓ Permanent deformation subtract from it the elastic deformation to get the value.

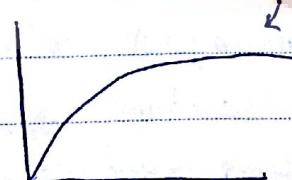
✓ some metals don't have yield point.

✓ design according to yield point not ultimate strength.

✓ "Proof stress": For materials which don't have yield point.

in small loadings it's stress is

• in slide 20 \rightarrow no yield point / in slide this curve there is yield.



FIVE APPLE

critical design stress is \rightarrow critical design stress
clearance \rightarrow clearance \rightarrow expansion \rightarrow $\Delta L = \epsilon L_0$

expansion \rightarrow $\Delta L = \epsilon L_0$

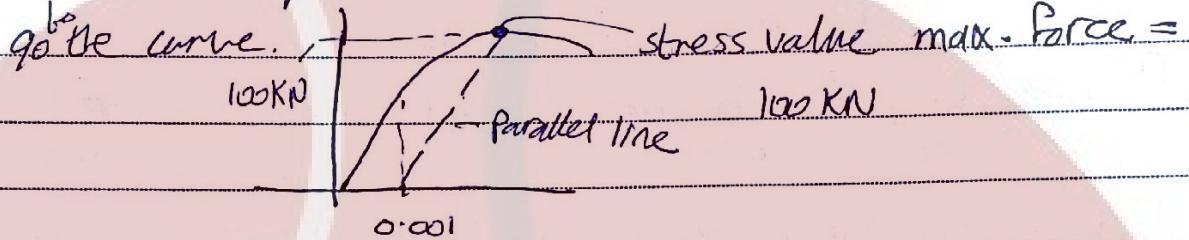
contraction & extension
we don't want permanent deformation.

NO. _____

✓ if the design very critical \rightarrow elastic region.

Q When there is deviation from linearity \rightarrow plastic deformation starts

✓ I don't want permanent deformation ≥ 0.001 "Proof"



if the force was 90KN no plastic deformation, if 101 there will be

✓ stress & high yield point

Q because I ductility (low hardness)

✓ polymers almost very low yield point (easily plastic deformation).

✓ plastic: LDPE (low ~~ductile~~, --)

engineering plastic such that PC, Nylon

✓ elastic region: nothing to be noticed optically

- highly hard bcuse the line close to y axis.

✓ Ultimate strength is if you exceed suddenly reduction in stress ~~area~~ some ~~area~~ where in cross sectional area.

✓ You must not exceed ultimate strength to avoid fracture

✓ Very danger if you exceed.

✓ on 80 stress if the material fracture?

Ans: original Ac ~~is~~ \Rightarrow its own yield curve \Rightarrow its

~~yield stress is equal to actual ultimate~~

✓ true stress strain curve

if you measure gauge length inst. At ~~one~~, ~~one~~

homogeneous structure \Rightarrow yielding, all ~~not~~ no =

because it is alloy we don't know where the atoms begin

even though pure metals there may be ~~there is~~ imperfection.

26/11/2017

20 ✓ Necking just in ductile material

✓ In plastic - it is ~~resistant~~ ductile

21 ✓ Ultimate stress \rightarrow tensile strength

✓ not all polymers are ductile there is brittle materials

✓ e.g. composite is concrete

✓ composite mix. of polymer with $\begin{cases} \text{metals} \\ \text{ceramic} \end{cases}$

22 representation how much deformation is produced

by two ways elongation or compression ΔL for the same F ↑ dudility

✓ cross sectional area reduction or

RA & EL & compression yields lit loss \downarrow to have it +ve
in compression $\frac{A_f - A_0}{A_0} \times 100\%$

23 ✓ Toughness & Resilience \rightarrow in elasticity Just

↓ absorbed energy of material through elastic deformation

✓ measurement of absorbed energy before the fracture point -
integrated area elongation \rightarrow $\sigma \propto \epsilon$

✓ generally ductile metals have large toughness more than brittle material

24 ask for recieve

✓ You can measure it at $\frac{1}{2} \times \text{height} \times \text{base}$ because of linearity in
elastic region.

25 tensile test uses plastic areas if yield zone

✓ Stress hardening in yield stress, near elasticity region -

✓ As much you make tests the point of end of elasticity will increase
"stress hardening" (increasing limit of proportionality).

✓ Why? rearranging according to the situation (recrystalliz. E_{bd})

✓ I must be in yield region only (in lower not upper).

✓ instead of 100 MN \rightarrow 110 MN it is good.

26 ✓ Hardness \rightarrow measurement of the surface strength -

✓ resistance of the surface to any permanent -

✓ indentation \rightarrow ایندنتیشن

✓ indenter and applied Force .

✓ indentation : indenter \rightarrow دستگاه برداشت

① 3, 4 testing for measuring hardness (specified by standards)

② 3 plat surface (polished)

③ diameter of the ball is standard also the load .

✓ surface of metal < surface of ball deformation on plate

steel ball with Al plate \checkmark if opposite deformation will occur \rightarrow on the ball .

✓ ball made of tungsten carbide or diamond .

Imp. ✓ \uparrow diameter of deformation \downarrow hardness no .

\uparrow indentation

✓ Test until $d = D$ The restriction point :-

$d = D \rightarrow$ repeat the test again with less load "Failed test"

- why ? because if $d = D$ I will not know the depth , maybe the magnitude is more large

27 ✓ Brinell is the most famous , easy you just must know D d

[P] Kg $P = \underline{\text{mass}} \text{ of indenter} + \underline{\text{load}} \text{ of force in } \underline{\text{kg}}$
not weight .

\sqrt{d} by calliper .

28 ✓ no body make true stress strain curve , it is hard to make

30 After certain limit you can't increase the hardness you will enter plastic deformation region .

اجزء اولیه سطح میگیرد و این نتیجه ایجاد شد که در سطح تراویح است .

• سطح اولیه پوشاننده است و این نتیجه ایجاد شد که در سطح تراویح است .
این ایجاد شد که سطح اولیه پوشاننده است و این نتیجه ایجاد شد که در سطح تراویح است .

FIVE APPLE

$\checkmark \uparrow$ Temp. \uparrow rate of deformation & magnitude .

31 • 10 samples for each material, you have to exclude the highest and the lowest value if they are far away from the range (expectation) then you take the average value.

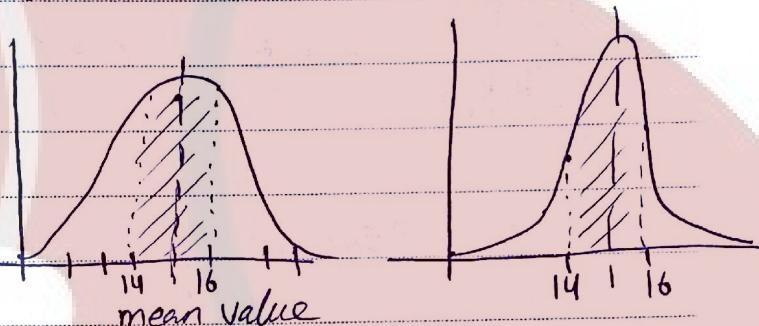
✓ $\sigma \approx 1.5$ standard deviations

by standard deviation

1 unit \approx 1 s.d. \approx

from the mean

bulk \rightarrow interval



✓ I don't want wide curve.

② working on 6 standard deviation is better than 1 \approx more variation
bigger variation \rightarrow it is over-weight

✓ narrow deviation \rightarrow better representation of materials.

28/11/2017

31 ✓ if $\sigma \approx$ does not make sense \rightarrow error -

32 ✓ ultimate stress \rightarrow higher value in engineering stress, dangerous it makes failure, after time hunder deformation "Creep phenomenon"

✓ critical design \rightarrow work on yield stress ordinary \rightarrow ultimate

③ Factor of safety \rightarrow decreasing stress to half at min.

④ at least $N = 1$

✓ yield stress of carbon steel

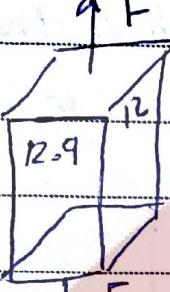
lower and upper yield if the material is hard.

All the previous are 1 Type of Failure.

End of Ch. # 5

Sheet #2

no. Solving suggested problems

① 

$F = 3600 \text{ N}$ material of construction: Al

strain? $\epsilon = \frac{\Delta L}{L_0}$ Hooke's law can be applied.

$E = 6 \times 10^9 \text{ GPa}$

$E = \frac{F}{\epsilon} = \frac{F}{E} = \frac{F/A}{E}$

$E = \frac{3600 \text{ N}}{12 \times 12.9 \times 10^{-6} \text{ m}^2} = 69 \times 10^9 \text{ Pa}$

② $E_{\text{Titanium}} = 108 \text{ GPa}$ $D = 3.9 \times 10^{-3} \text{ m}$ cylinder

elastic deformation $F = 2000 \text{ N}$ $L_0?$ $\Delta L = 0.42 \times 10^{-3}$ max.

if $\Delta L = 0.5$ recovered 0.42
unrecovered 0.08

$$\epsilon = \frac{F}{A} = \frac{2000 \times 0.25}{\pi \times (3.9 \times 10^{-3})^2}$$

This is the max. to before permanent deformation.

$$\epsilon = \frac{\Delta L}{L_0} = \frac{\Delta L}{L_0}$$

~~$\Delta L / \epsilon$ constant to varies~~ $\Delta L / \epsilon$ constant to varies

if ΔL cons. ΔL if ϵ const ΔL

③ square Al $L = 0.02 \text{ m}$ length = 0.1 m $F = 8900 \text{ N}$

$\Delta L = 0.1 \times 10^{-3}$ elastic deformation $E?$

$$\epsilon = \frac{\Delta L}{L_0} = \frac{6}{E} \Rightarrow E = \frac{6}{\epsilon}$$

$$E = \frac{8900}{(0.02)^2}$$

$$\epsilon = \frac{\Delta L}{L_0} = \frac{0.1 \times 10^{-3}}{0.1} = 10^{-3}$$

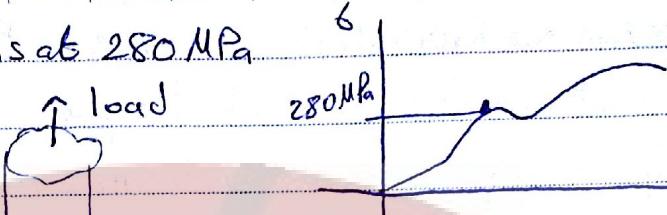
(4) plastic deformation begins at 280 MPa.

$$E_{\text{Bronze}} = 115 \text{ GPa}$$

$$A = 325 \times 10^{-6}$$

load?

$$\sigma_{\text{max}} = 280 \times 10^6$$



$$\textcircled{a} \quad F_{\text{max}} = 280 \times 10^6 \times 325 \times 10^{-6} =$$

\textcircled{b} if $L_0 = 120 \text{ mm}$ ~~is it~~? ΔL_{max} ?

$$\epsilon = \frac{\Delta L}{L_0} = \frac{\Delta L}{6 \text{ max}} \quad \Delta L = L_0 \cdot 6 \text{ max} \div E \\ = \frac{120 \times 280 \times 10^6}{115 \times 10^6}$$

(5) cylinder, copper $E = 110 \times 10^9$ $\sigma_{\text{yield}} = 240 \times 10^6$ load = 6660 N $L_0 = 0.38$
diameter? $\Delta L_{\text{max}} = 0.5 \times 10^{-3}$ in plastic deformation

You can't use Hooke's law.

$$\epsilon \text{ according to this force} = \frac{0.5}{0.38}$$

assume we are at the elastic range
if $\sigma_{\text{actual}} < \sigma_{\text{yield}} \rightarrow$ elastic region

Assume that 6660 N will not cause and vice versa.

$$\text{plastic deformation} \Rightarrow \sigma = E\epsilon = 110 \times 10^9 \times \frac{0.5}{380} = 144.7 \times 10^6$$

since σ in elastic

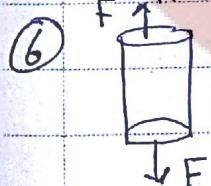
$$\sigma = \frac{F}{A} \quad A = \frac{F}{\sigma} = \frac{6660}{144.7 \times 10^6}$$

$$A = \frac{1}{4} \pi d^2$$

If it is in plastic you can't solve ~~it's 8 digits~~ it's ~~it's~~

if $\sigma = 344.7$ $\sigma - \sigma_{\text{yield}} \rightarrow$ plastic deformation.

3/12/2017



$$\sigma = E \epsilon_{\text{lateral}}$$

$$\epsilon_{\text{longitudinal}} = -\epsilon_{\text{lateral}} / D$$

$$\sigma = E \epsilon_{\text{longitudinal}}$$

$$F = \sigma A_0$$

$$3.25 \times 10^4 \text{ N}$$

$$\textcircled{7} \quad E = 1.705 \times 10^{11} \text{ Pa}$$

"necking"

NO. Chapter #5

- 1 - Previous we have studied two types of failure, Tension [3/12/2017]

- 80% of Failure because of Fatigue. compression

→ Ship example ... what is the reason of Failure?

→ resen. reasons 3 Types 1. Fatigue 2. Creep 3. impact

• دعوة المؤمنين التي ترجم الى الملة والخطب

 There is stress frequently occurring (below yield stress) failure under this loading.

very small stress frequently occurring. "Fatigue limit" how many cycles I need to make failure

- The chip is not failed but the wires because of heating & cooling
will due to stress / result cause Tension \leftarrow compression.

Tension / compression Thermal (internal)
 physical (external)

- Also if you make twisting & torsion (C.W & C.C.W) or bending up & bending down.

- creep : at very low force for an interval of time -

2 - Failure starts at spot (weave area) propagation of crack

3 - Failure : separation of component, not deformation

+ there is fracture in brittle material.

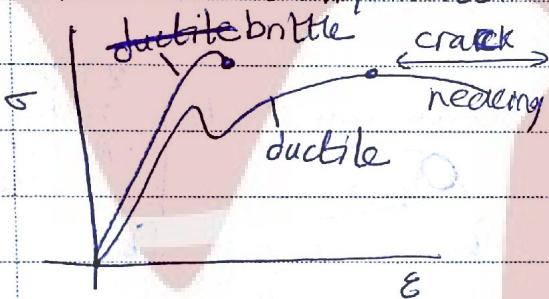
- without crack formation no fracture internal crack - D-spat

--> مختصر: دستاں کی

- slow propagation in ductile material (Further crack propagation below fracture) until there is very small area resistance

the brittle material is opposite.

- generally metals are ductile at room temp. (You can convert it by variation of temp.) \downarrow Temp. ductile \rightarrow brittle if there is crack
- glass transition temp. if \downarrow Temp is bigger \rightarrow ductile brittle is smaller \rightarrow brittle (like glass). dangerous
- You must keep the sample above glass transition temp.
- e.g. polycarbonate at room temp. is below glass transition temp. = 80°C if above 80°C it can be bend.
- Here we are talking in room temp.



- 4 - Toughness - one of the ways to differentiate between ductile & brittle
 - some stress strain tests are in over \rightarrow stress strain curve neck at room temp.

الواحدة المثلثية

- 5 - very ductile material \rightarrow A big difference in fracture area, like tip big
 \uparrow reduction \uparrow ductility

no variation between initial & final cross sectional area \rightarrow C

elastic deformation returns Flat surface [90° angle of propagation]

there is reduction in cross sectional area \rightarrow B [Cup & Cone] 45°

the difference between C & B \rightarrow surface of fracture

the reason

- 6 - reduction of A at ultimate stress.

- b: internal crack

- d: \downarrow ductile material \rightarrow 45° \rightarrow reason of cup & cone
 brittle

- c: all crazes begins at 90° almost negligible distance the as area (craze)
 increase the angle changes 90° \rightarrow 45°

5/12/2017

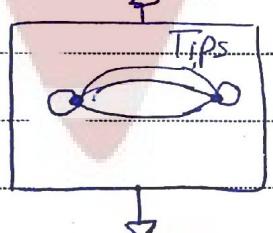
7 - crack of ductile material at grain boundaries.

- DANGER
But brittle material high propagation (higher than ductile) it begins at angle 90° and ends on 90° & The reason of flat surface.
& no necking, no noticeable deformation of cross sectional area.
in ductile you can notice necking.
All types of defect maybe the cause of crack.

8 - There maybe exist breaking of crystals in brittle material.

crystallographic planes do not

10 - experimental work



$\frac{2\pi}{3}a/2$
length of
propagation
(crack)

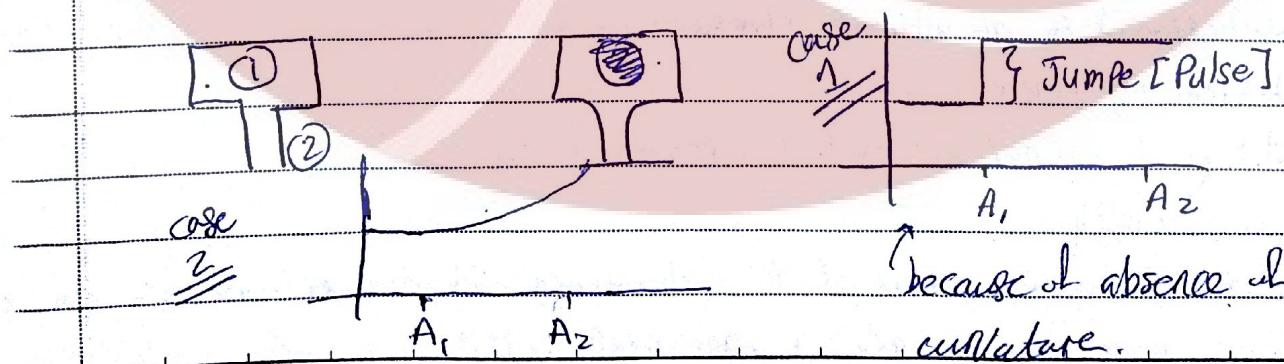
- 3 values of stresses

11 initially $St = a$. Then
 σ_m \downarrow $a > St \Rightarrow \sigma_m$ will increase

But there is limit

$$\sigma_0 = \frac{E}{A_0} \quad \& \quad \sigma_m$$

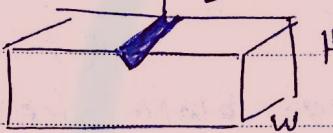
12 - don't make sharp reduction but make fillet to reduce stress conc.
You make it gradually from min. Area to max., if you make it 90°
it will have failure faster \leftarrow Pulse is just suddenly



- suddenly moving in stress \rightarrow exist stress conc. area at this point \rightarrow failure gradually \rightarrow stress conc. not at the point \rightarrow failure at the gauge length.
- avoid stress conc. area.

13 - For imp. applications. (e.g. bottles, ...) grove according to STAM (standards)

- The sample is rectangular bar grove to help for fracture.



U or V shape.

1. Charpy

2. isode

3. Free Falling

grove
out

الكتل المعدنية ذات الصلة بالمواد المترسبة

almost the same, the difference is the way of clamps.

عالي / منخفض يرجع إلى تفاصيل التفاصيل التي تختلف

والفرق في النتيجة إذا ما أخذ قياس

U/Io Test

- The idea is the potential energy. Pgh

$\Delta E_p =$ energy absorbed by the sample. But there is Friction (losses)

You can measure it in the absence of sample
(Friction \rightarrow loss, lossless)

- It is a comparative test.

- You know the area \rightarrow You can calculate impact energy.

14 some times the material is so much ductile

7/12/2017

convert it to brittle (cool it, or Δ Temp. of your sample environment) \rightarrow so brittle material

تحویل ضربة

increasing Temp. for certain period of time then immediately test it (take Temp. at the instant of test) increasing temp. to make chains flexible.

NH₃ / N₂

freezing of chains (rigid). \rightarrow Temp. loss

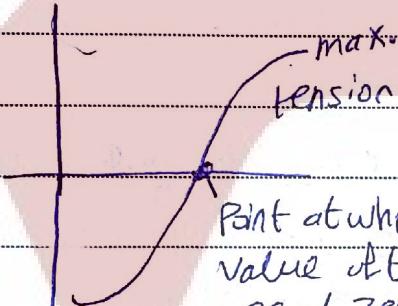
15 room temp. doesn't mean ductile or brittle it depends on glass transition temp. (transition temp. in which material changes its behavior from brittle \Rightarrow ductile).

FIVE APPLE

16 - value of stress below ultimate stress, if it is frequent the reason of failure \rightarrow Fatigue

Fatigue \rightarrow ultimate limit

- "cyclic actions" +ve & -ve signs (bending up & down, twisting right & left, tension & compression) \leftrightarrow fatigue

17

This layer does not elongate

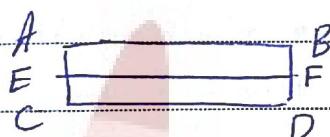
\rightarrow "neutral axis"

Point at which the
value of the function
equal zero

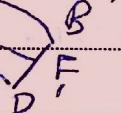
overall all

compression

- uniform geometry \rightarrow neutral axis in the middle (symmetrical)



+ve extension



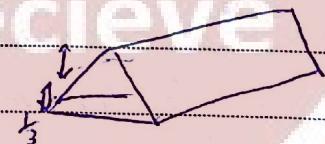
-ve extension

$$\overline{AB} \neq \overline{A'B'} \quad \overline{CD} > \overline{C'D'}$$

$$\overline{EF} = \overline{E'F'} \text{ displacement = zero}$$

- if the shape is not symmetrical

neutral axis not at the middle it is $\frac{1}{3}$ from base.



For non
symmetrical

\leftarrow neutral axis

* if neutral axis at zero line,
symmetrical shape
vice versa

٩ - σ live design stresses

- σ_{min} take it without the sign.

١٩

نـزاع دیناریا \rightarrow دیناریا

counter \rightarrow عـارضـيـه

force downward \leftarrow bearing \rightarrow دیناریا و دیناریا

- tension & compress. if gear rotating \rightarrow

- every point on surface at time tension and then compression. Frequently.

- Fracture سـعـدـيـه او قـدـرـيـه

80% σ_{max} , Fracture دـيـنـارـيـه

Fatigue limit دـيـنـارـيـه

- \uparrow load \downarrow σ_{max} to reach fracture

- there are materials which don't have fatigue limit.

20 - this stress is below ultimate stress much lower than yield or ultimate. in elastic range.

21 - usually very ductile material \rightarrow no fatigue material, at the end there is failure - vice versa.

✓ reaching \leftarrow propagation of crack \rightarrow behaviour until final fracture.

22 - on the same surface just we make 1 force, but there is solving 8

① tension & compression forces on the same surface at the same instant "shot peening" deformation under microscope, if make 2 forces \Rightarrow دـيـنـارـيـه

② carburizing is rich source of carbon (for metals)

- دـيـنـارـيـه Fatigue limit

10/12/2017

- 23 - creep even though less than ultimate stress
 - as well as there is live weight(s) there is creep
 - creep & failure under very small loads, which causes
 creep by the time less than U.S (even in elastic)

- ↑ load / ↑ Temp / material of construction \Rightarrow ↑ creep
 - The sample shape similar to that of tensile but shorter

 gauge length

 extensometer (ϵ_L)

 weight \downarrow $\Delta L = 0$ at time = 0 (supported before testing)

initial tension \rightarrow elastic strain.

(*) $\rightarrow G(E) = \text{height}(\epsilon)$

FIA

- in the 3 tests you must approach the fracture.

* primary: (decreasing rate of strain) until approach steady value

secondary: ΔL const. slope \rightarrow cons. creep rate $\&$ ϵ increasing

"we'll also have a point in, where ΔL is increasing again"

$$\text{time} \times \text{slope} = \Delta L$$

tertiary: variable rate of strain (increasing)

most dangerous step, Failure is possible.

- rate at the end of primary = rate of secondary \rightarrow You can calculate the time.

- brittle \rightarrow more time

not on all loads there is creep

- limit value of force (if force is smaller \rightarrow ~~initial~~ ^{creep} small ΔL)

(deformation less) - always σ increases ΔL less in σ \propto ΔL -

24 - lead (Pb) is very ductile, very soft is used in labs.

- you don't want to exceed melting temp. / 2

the factor of safety, Temp. = 0.4 * melting temp.

NO.

- \uparrow Temp. \downarrow Time to Failure.

- as temp \uparrow be aware of the load (even though small).

25 - it is in secondary stage

- ~~$\uparrow \sigma$~~ $\uparrow \epsilon$ \leftarrow ~~σ~~

26 - it is similar to fatigue brittle

- ductile material variation $\Delta L \rightarrow$ very change in cross sectional area.

- same behavior of extension but constant σ with time varying.

- brittle \rightarrow fastly failure (no big deformation).

- \uparrow Temp. \downarrow σ (Laws. \rightarrow stress const.).

ask

End of chapter

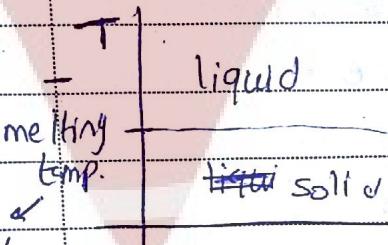
receive

10 marks on first + second 30% on final material.

No. Chapter #7

"Phase diagram"

- phase diagram of metals changes as it changes for multi-component
- alloy: at least 2 elements exist.
- metals may be a gas in special cases { apart from this metals exist e.g. mercury $\text{Sn} \text{Al} \text{Fe} \text{Cu} \text{Zn} \text{Si}$ } in solid/liquid state.



- no phase diagram for pure metals
- we'll take phase diagram for 2 elements in this course.

suddenly
changing
solid \rightarrow liquid
vice versa

composition

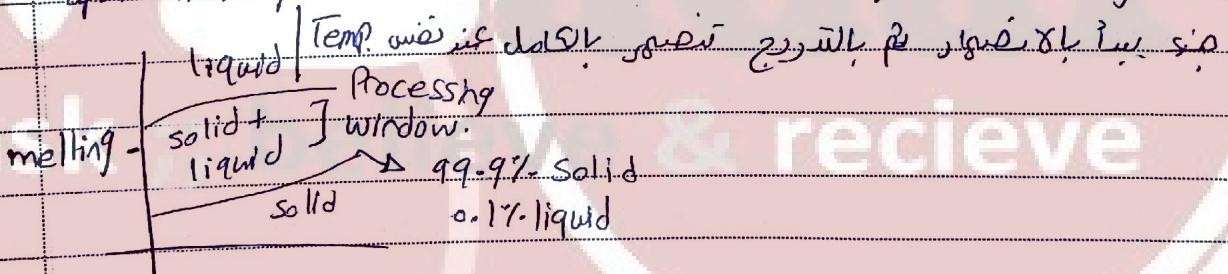
"unary system" liquid or solid, no in ~~beta~~ between

- 4 element you can't imagine phase diagram.

suddenly if it is pure material [Pure metals \rightarrow sharp melting temperature]

but we don't have pure materials (there is impurities)

- apart from pure metals \rightarrow we have alloy \rightarrow range of melting temp.



2

may be there is more than 1 phase in the same state $\begin{cases} \text{liquid} \\ \text{solid} \end{cases}$
structure of metal

2 phases exist $\begin{cases} \text{e.g. Fe & C} \\ \text{in solid state} \end{cases}$ when solidification $\begin{cases} \text{Fe gives 2 phases} \\ \text{structures: Ferrite, cementite} \end{cases}$

carbides

phase & microstructure

12/12/2017

- to have interstitial, substitutional impurities you must melt the material - (by any method).
- quenching, gradual. - (methods of solidification).
- component \Leftrightarrow any element in the structure
- generally we deal with ~~the~~ components not elements.
- \Rightarrow compounds : at least two elements but actually it is more
Binary system (α + β)
- \uparrow #elements \uparrow difficulty of representation
(interpretation)
- no iron with Perlite or cementite only it is mixed (both exist) -
Perlite

2 Phases ~~in~~ /solid state , we have 2 phases α & cementite
different composition & C & different struc.
so the properties differ.

α alone uniform properties (phase)

in one state there is more than 1 phase

- e.g.

ice
liquid

 water
2 states \rightarrow liquid \rightarrow 1 phase

- e.g. excess of C \rightarrow 6-7% Si

graphite : one component

\otimes	\odot
\otimes	\odot

1 state 3 phases
cementite
2 components

5 - in isomorphous system can change - solvent \rightleftharpoons solvent

e.g. Ni & copper they are compatible

at 50% composition solute & solvent not known

e.g. C & Fe & not isomorphous.

- 6 - by phase diagram you will know the microstructure
- 7 - >902 BCC \rightarrow FCC
- Cast iron \uparrow C composition & Pearlite contain cementite more than Ferrite
 Phase diagram is useful \rightarrow ductility
- I'm interested in the ~~mix~~ Proportionality of phases
 You can't test 1 phase.
- $C < 2.1\%$ \rightarrow steel $> 2.1 \rightarrow$ cast iron
- 8 - each material has final equilibrium state
 - at certain temp. ratio of solid to liquid keeps constant
 molten material when cooling (liquid \rightarrow solid)
 isothermal temp. "equilibrium state" not "final eq. state"
 assume cons. pressure
- if Temp. changes phase structure \rightarrow metastable
- at phase diagram we will be at metastable \leftarrow eq. $\xrightarrow{\text{cooling}}$
 at room temp. \rightarrow equilibrium
- 10 - controlling P, Temp, composition
 almost constant
 - we will just deal with two components
- 14/12/2017
- (
 - solid
 - molten
 - crystallization/crystallization) } 3 lines
 - metastable at final will be isothermal crystallization.
 - 1 x axis you can read two compositions
 - alloys melts at high temp.
 - All pure components the same behavior
 suddenly changing from ~~to~~ solid = liquid state

- Some materials we are not interested which one is solute, solvent because of limited solubility does not exist "isomorphous"
e.g. Ni & copper they are compatible

- alloy \rightarrow no sharp melting temperature
at Temp. in between / not straight line between the 2 Temp.

- (solid solid going to solid solid transition)
- "Processing window" of crystallization.
 - impurities are in the building block of solvent. You can't distinguish between solute & solvent
 - gradually not sharp

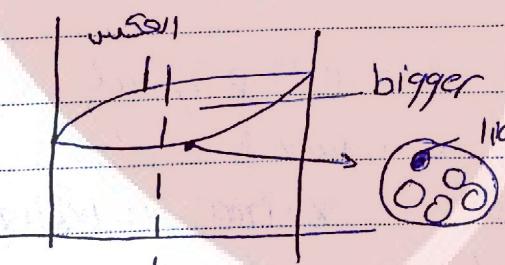
"Cored structure" (solid solid cored solid)

- . same as solidification, crystallization, every shell have different composition.

- The outer shell starts to melt then finally at core
 \uparrow conc. of Cu \downarrow conc. of Ni Not homogeneous

sharp melting temp. if the shell and the lower shell and so on until you reach the core are the same composition exactly the same behavior of pure component but it is not exist in industrial.

- 15 - Part solid & Part liquid \rightarrow metastable equilibrium
- no melting Temp. is for neither the two components, it is in between.



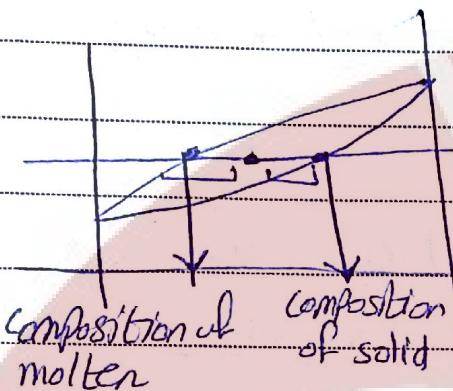
same composition of
a long as we have 1 phase
In the state But in solid liquid region
not the same composition



Ni % Cu % as long as Temp. is constant
the composition is kept constant
what is the composition?
Lever rule

consmp. Ni different than Cu

- Lever rule idea comes from a game (see-saw)



$$\text{composition} \times \text{distance} = \text{composition} \times \text{distance}$$

$$\text{composition} \times \text{distance} = \text{composition} \times \text{distance}$$

$\text{distance} \approx \text{solid} + \text{liquid}$, i.e.

$\uparrow \text{Temp.} \uparrow \text{distance of solid}$

$\uparrow \text{comp. of liquid.}$

* Lever rule is used whenever there is more than 1 phase (solid/liquid region)

You can use it in solid if there is more than 1 phase.

- in F-C 2 phases in solid state \rightarrow You can use Lever rule.

- You care about phase rule state

- in liquid always 1 phase (again homogeneous)

Lever rule $\frac{\text{weight of solid}}{\text{total weight}} = \frac{\text{distance of solid}}{\text{total distance}}$

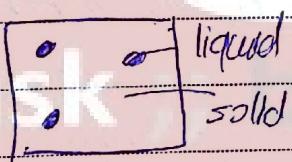
$\Rightarrow 10\%$ in solid \rightarrow 10 cm

17/12/2017

Lever rule $\frac{\text{weight of solid}}{\text{total weight}} = \frac{\text{balance of liquid}}{\text{total liquid distance}}$

$\frac{\text{balance of liquid}}{\text{total liquid distance}} = \frac{\text{liquid distance}}{\text{total distance}}$

22



in liquid state 35% Ni 65% Cu

in solid state " "

both liquid & solid be total " "

- You can do it by vision

arm of liquid \rightarrow solid arm of solid \rightarrow liquid.

- isomorphous 1 state, 1 phase in liquid & solid

2 states, 2 phases in existing solid & liquid.

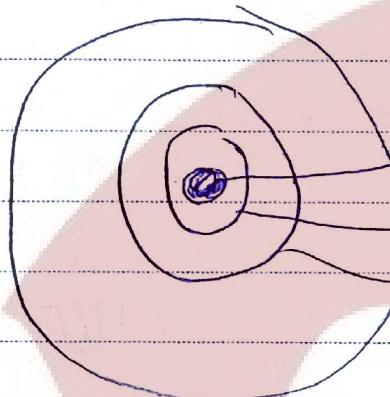
23 * composition rich of material that have higher melting point

Almost ~~the~~ weight fraction of solid is negligible.

① composition of shell

increase Ni in solid state

② latest shell composition



46% Ni 35%
42% for as iso
35% liquid & solid.

liquid (पानी)

rich in copper because
lower melting Temp.

But average weight fraction 35% Ni

35% Ni \leftarrow 0.1 degree solidus line सूखा लाइ-

- 0.1/2/1 के बीच जो भी निम्न अवकाश -

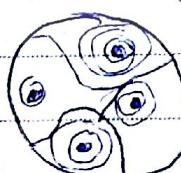
\equiv Isomorphous phase diagram the same microstructure, even though different composition of materials.

- α phase \Rightarrow solid

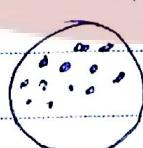
25 return to Figure in slide B 65% Ni



28. $\cdot \uparrow$ diffusivity \uparrow अलादा होना
 $\cdot \uparrow$ viscosity harder solidification. Growth rate / nucleation
 \cdot Industrially quenching 1000 degree/min. like smectic structure



without
quenching
slow cooling



with
quenching

1, 2, sheets of crystal fast

different compositions
of shell.

FIVE APPLE

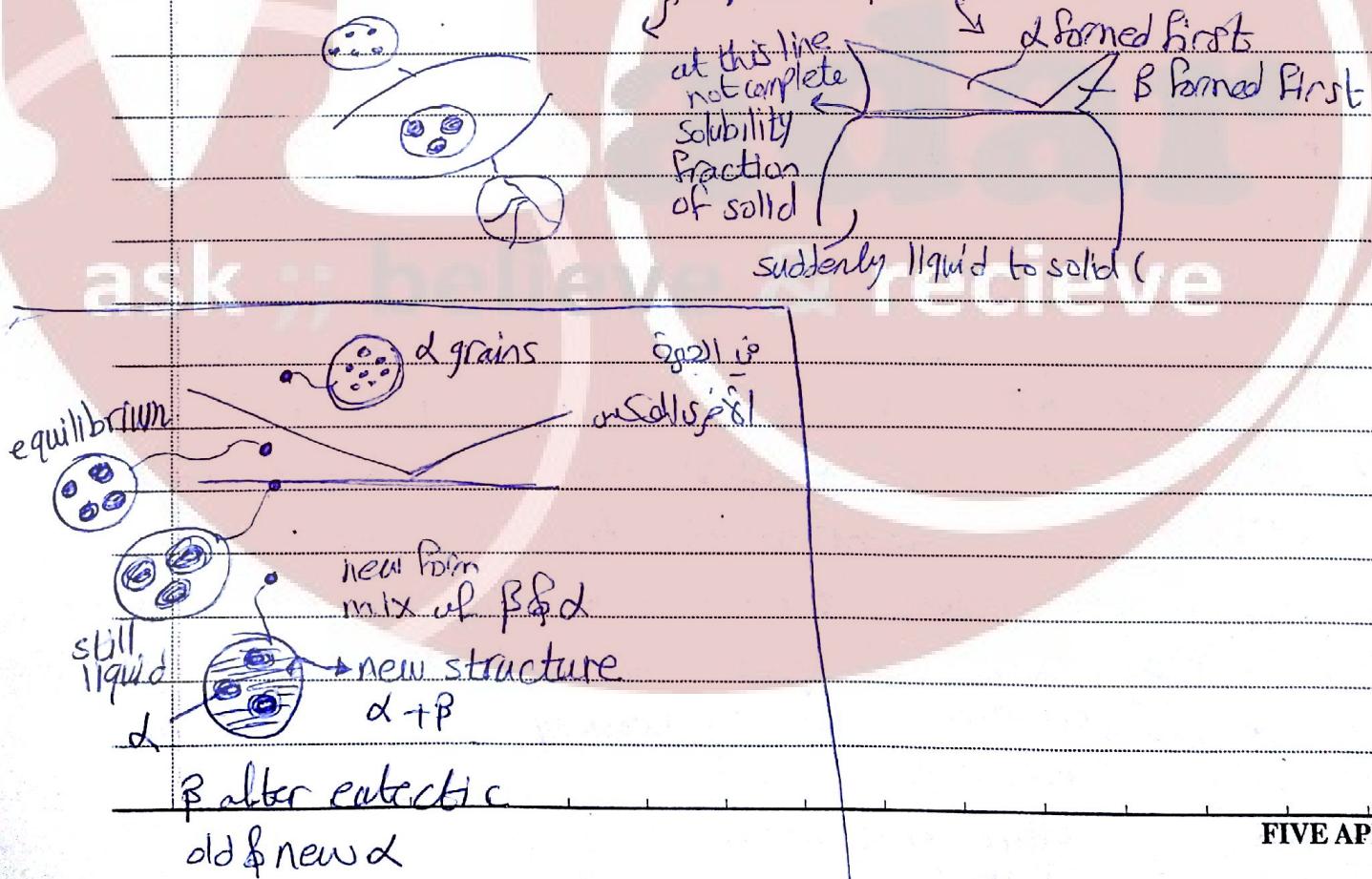
Isomorphous second phase.

NO. _____

- 30 - For not compatible compounds (not isomorphous, not highly soluble in each other) it is a second phase
- Here 6 regions not 3 as previous:
- α high percentage of copper. negligible Ag.
 β rich with Ag (mainly Ag) negligible Cu.
- Eutectic composition \rightarrow sharp ~~no~~ Temp. cu
 $L + \alpha / L + \beta$ eutectic regions
- β Cu in Ag
 α Ag in Cu
- below 400 Temp. at any Temp. two phases together exist in equilibrium.
- Eutectic line is horizontal in phase diagram.
- at 71.9 (CE) behave like pure metals.
 $L \propto$ more solid fraction.

[19/12/2017]

* Difference between isomorphous & eutectic

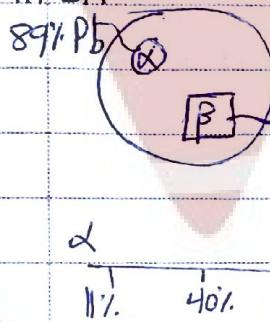


- Any region 2 phases you can apply lever rule to calculate fraction weight in L+d / L+β / α+β regions.
- L + β exist together just at eutectic point.
- Solid is one phase solid from liquid
- Solvus solid to solid ($\alpha \rightleftharpoons \beta$)

33. 2-2 Pb in Sn solubility.

quantity of solubility of Pb in Sn not the same as Sn in Pb.

11% Sn



$$\alpha = \frac{99-40}{99-11}$$

$$\beta = \frac{40-11}{99-11}$$

α	β
11%	89%

34. L + α

Slow diffusion

contain α+β (that will be formed below eutectic line)

- Two types of α → strong (before eutectic)
weak (after eutectic).

- 2 phases, 2 states.

Boundaries
[liquid or solid line → (boundary) weakly p/s
solid weakly in boundary]

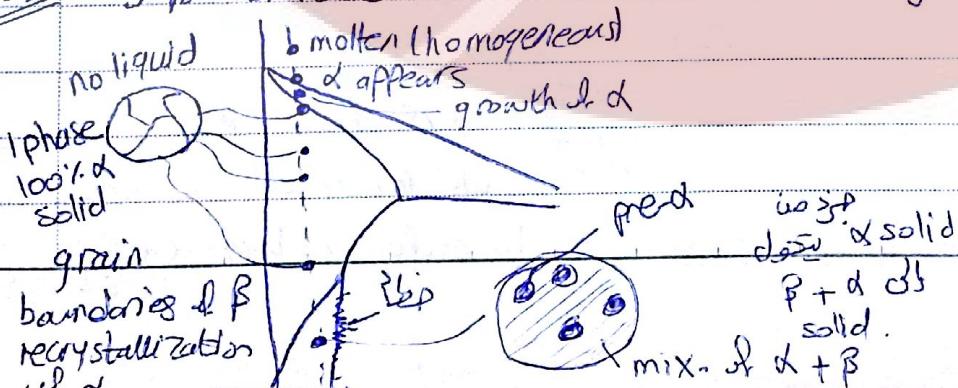
α 17% Sn 83% Pb
L 40% Sn 54% Pb

17% 40% 40%

Total 40% Sn 60% Pb

There will not be generation, consumption of Sn, Pb

- ### 35. 5 Possibilities for solidification (5 regions)



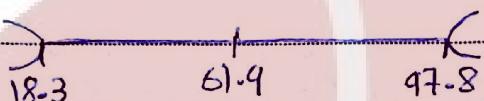
FIVE APPLE

37 - at eutectic line suddenly liquid \rightarrow solid ($\alpha + \beta$)

- uniform layers of $\alpha + \beta$ with different orientations, structure \leftrightarrow (عوالي اولى) (التيار المترافق)

- Find concentration below eutectic line

Just one eutectic composition



39 At eutectic there is a fraction liquid

eutectic composition (النسبة المئوية في الخط)

max. amount of Pre α Just above eutectic line

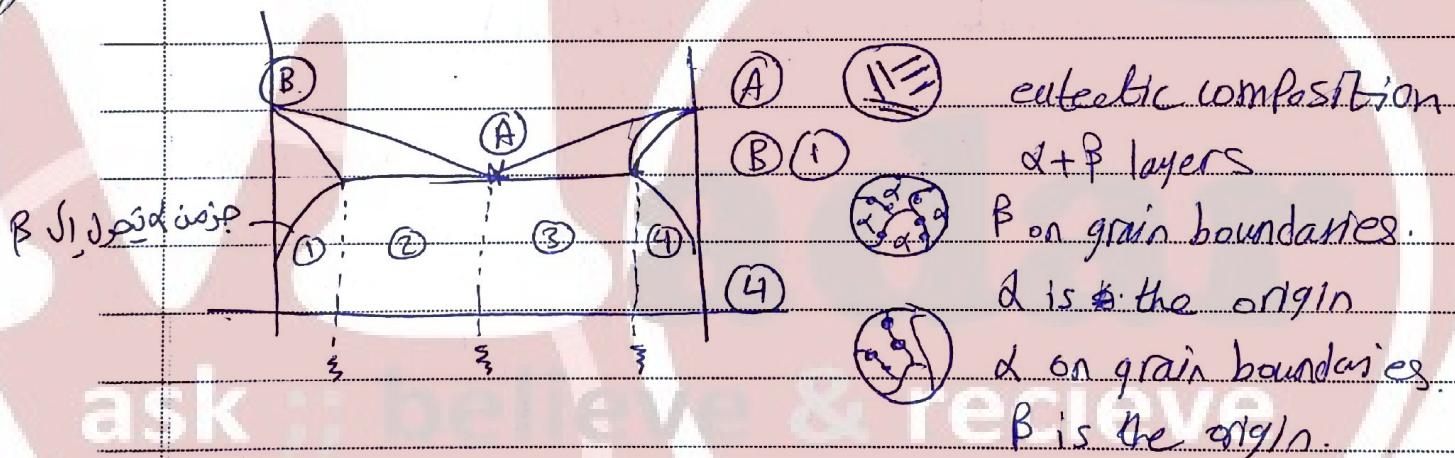
max. amount of Post β Just below

$$\text{Post } \beta - \text{Pre } \alpha = 100 - \text{Post } \beta = \text{Pre} + \text{Post } \beta$$

$$100 - \text{Pre } \alpha = \text{Post } \beta$$

$L + \beta / L + \alpha \rightarrow$ 2 states, 2 phases

21/12/2017



eutectic composition

$\alpha + \beta$ layers

β on grain boundaries.

α is not the origin

α on grain boundaries

β is the origin

②

liquid converted suddenly to eutectic

③

layers of $\alpha + \beta$.

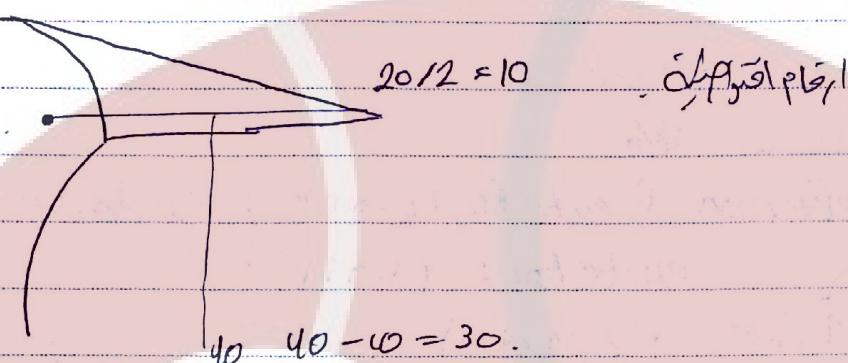
liquid converted suddenly

to eutectic (layers $\alpha + \beta$)

FIVE APPLE

40 differ in physical & chemical properties

41 2.2



42 - eutectic is the simplest graph of alloy (no intermetallic compound).

(intermetallic compound) سبب علیجه، دستی ایشان -

2 مساوی 2 در یک Phase diagram هست

- This compound exist at room temp. at any composition.

new compound differ than components present previously -

43 - There is extension of this phase diagram.

- above 6.7 conc. \rightarrow mix. with graphite \rightarrow مول اپدیس

- ① 2 states, 2 phases, L to eutectic composition (8 + Fe₃C)

- & rich iron, low composition of carbon.

- $\uparrow \alpha \rightarrow$ near left position manufactured \rightarrow Flexible.

$\downarrow \alpha \rightarrow$ near right position manufactured \rightarrow قدرتی \rightarrow Cast iron.

- low carbon steel & high carbon steel

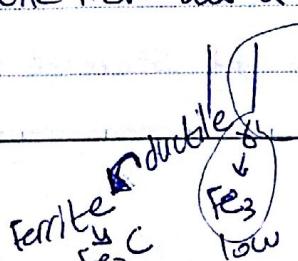
$\rightarrow \alpha \rightarrow$ low \rightarrow Fe₃C \rightarrow high



- $\delta \rightarrow$ metastable Ferrite. α - (α + δ) same structure

FCC \leftarrow δ $\xrightarrow{\text{cooling}}$ BCC \leftarrow α $\xrightarrow{\text{cooling}}$ δ, 1380 \rightarrow این کار را در 1380 درجی

- ductile iron all & (low conc.)



L \rightarrow Fe₃C \rightarrow cast iron (high c)

3 types of Fe

 $\alpha \rightarrow \text{Fe}_3\text{C}$ ductile $\gamma \rightarrow \text{Fe}_3\text{C}$ ~~low~~ $\text{L} \rightarrow \text{Fe}_3\text{C}$ high

- 44 At A \Rightarrow definition of eutectic ($\text{L} \rightarrow \text{S}$) \Rightarrow suddenly changing.
 At $B_0^\circ \Rightarrow$ euctetoid ($\text{S} \rightarrow \text{S}$)
 (1 phase \rightarrow 2 phases)

24/12/2017

- In iron, Ferrite & semimite \Rightarrow Pearlite (below eutectoid line).
- pre post \leftrightarrow hypo hyper
above after
- 47 reaching austenite ($\approx 900^\circ\text{C}$) \rightarrow changing structure
- at 1400 $\text{FCC} \rightarrow \text{BCC}$ $\{\$ not stable
at 912 $\text{BCC} \rightarrow \text{FCC}$ $\}$ high temp.
- To have steel, the original structure must be austenite
(line in slide no. 46) γ in Fe_3C or w.i.
brittle iron $\leftarrow \text{L} \leftarrow \text{Fe}_3\text{C}$ or w.i. \leftarrow 131
- 49 higher conc. in γ because of bigger voidage (FCC) than (BCC)
ind

strong \leftarrow Phase \rightarrow -

- steel is more flexible \rightarrow conc. of Fe_3C \uparrow ductility
- high carbon steel \rightarrow brittle \rightarrow can't be bonded.
- mechanical prop. differs in different region in phase diagram

- 50 - not all types of steel is magnetic -
- magnetic \leftarrow liquid \leftarrow semimite or w.i.
 \downarrow magnetic \leftarrow austenite
 - magnetic \rightarrow w.i. \rightarrow stainless steel

hyper + Post

NO.

- cast iron + ferrite \rightarrow the more magnetic.

51 - within the range of steel, low carbon steel

$\alpha = 0.022\% \text{ C}$ iron (g/w) $\text{Fe}_3\text{C} = 6.7\% \text{ C}$

$$\text{Post Total } \alpha = \frac{6.7 - 0.4}{6.7 - 0.022} \times 100 \quad (1)$$

$$\text{Re } \alpha = \frac{0.76 - 0.4}{0.76 - 0.022} \times 100 \quad (2)$$

(1) - (2) \rightarrow Ferrite formed in pearlite

Phase diagram \leftarrow Final phase

End of chapter

↳ plz note that the phase diag. is ZnCu \leftarrow it needs further treatment, e.g. annealing

removal of residual stresses in sample
be relaxation (\uparrow temp not to melting)
then cooling in certain procedure

Cast iron fabricated \leftarrow as

"Casting" سلحشور

قطعه میں پر بھیج، پس اسکے \rightarrow (ZnCu) on Fe clay نہیں

NO. Chapter 11

3 - non ferrous limited because of low availability and also ^{also} ~~use up~~ 26/11/2017

4 - eutectic composition
high carbon \rightarrow above
below \rightarrow low carbon steel

- austenite \rightarrow ^{no wts}

- Steel are not just iron, carbon

- plain \Rightarrow 10 \rightarrow no additives other than carbon.

5 - Fe existing carbonics in all types I want the oxide even
 \searrow sulfide though sulfide I make it oxide
oxide

- Fabrication of equipment

by lining \rightarrow ^{brick} \searrow external shell is steel
breaks as insulation

- they put large amount of C (as coal) with the material \rightarrow ignition of carbon \rightarrow crushing

give CO & CO₂ I want CO for rxn

- emission of large quantities of CO \rightarrow ^{brick} \searrow gives

- Limestone \rightarrow ^{lime} \rightarrow inc organic material

- slag & complex structure density << density of iron

bottom layer when melting (iron-molten) (slag \rightarrow ^{upper})

molten iron rich in carbon, later there will be treatment
"pig iron"

CO source

\downarrow SW \rightarrow cast iron

ductile & more resistance to tension -

10 annealing \rightarrow recrystallization, another structure with another properties.

- 11 - You have to start with big iron (rich in C)
- 12 - metastable zone (high σ_{sol} and) at isothermal temp. → crystallization
- Cooling is more important than the composition of additives.
- 13 - Disadvantages

Corrosion is also its biggest drawback.

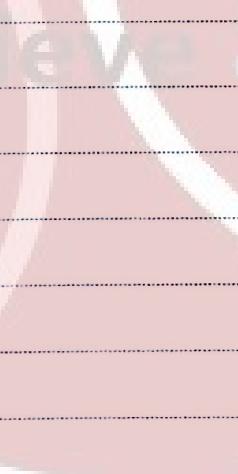
- even though stainless steel there is corrosion not at room temp.

14 e.g. Frame of windows (Al Frame), slot \rightarrow two oil jets

- by forming plate with standard width, length and different thickness.

- at cold working \leftarrow (2 draw) \rightarrow σ_{sol} , σ_{int} \rightarrow sometimes \uparrow Temp. of material (to become brittle) "die" deformation

- small size causes \rightarrow small area of impact stress

ask  receive