

McCabe-Thiele Method:

Also plate to plate solution

This method is based on:

- ① Assumption of constant molar overflow (CMO), which results in straight line operating lines on molar basis.
- ② Constant column pressure [sets equilibrium data]
This makes it possible to use a y-x diagram for a graphical solution.

Operating lines:

Enriching section.

For stage n

$$y_{n-1} = \frac{L}{V} x_n + \frac{D}{V} \cdot x_D$$

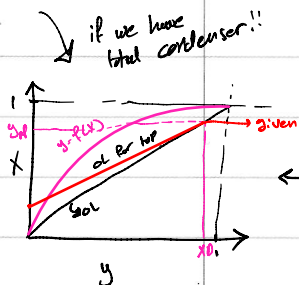
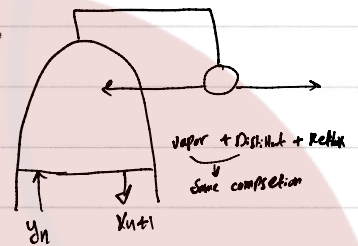
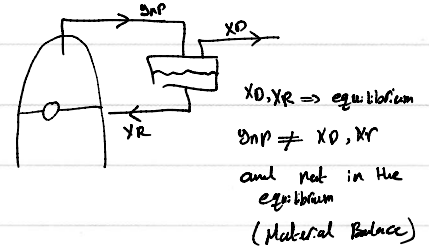
$$V = D(R+1)$$

$$y_{n-1} = \frac{L}{D(R+1)} \cdot x_n + \frac{D}{D(R+1)} \cdot x_D$$

$$y_n = \frac{R}{R+1} \cdot x_{n+1} + \frac{1}{R+1} \cdot x_D$$

For partial condensation

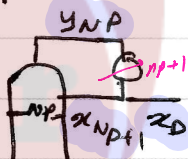
(one stage equilibrium base outside the column)



if we have total condenser!!
by this value we'll draw the operating line
-> we stop at x_D, y_D

This line intersects the 45° line at $y_n = x_{n+1} = x_D$

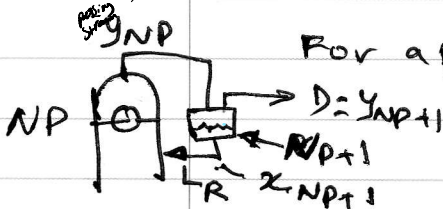
For a total condenser: $y_{NP} = x_{NP+1} = x_D$



For a partial condenser: $y_{NP} \neq x_{NP+1} \neq x_D$

$$y_{NP} = \frac{L}{V} \cdot x_{NP+1} + \frac{D}{V} \cdot x_D$$

$$\begin{cases} x_D = y_{NP+1} \\ x_{NP+1} = f(x_D) \\ = f(y_{NP+1}) \end{cases}$$



$$y = \frac{P}{P+1} x + \frac{x_D}{P+1}$$

$$y = \frac{\bar{L}}{V} x - \frac{x_B B}{V}$$

Exhausting Section:

$$y_m = \frac{\bar{L}}{V} \cdot x_{m+1} - \frac{B}{V} \cdot x_B$$

This line intersects the 45° line at

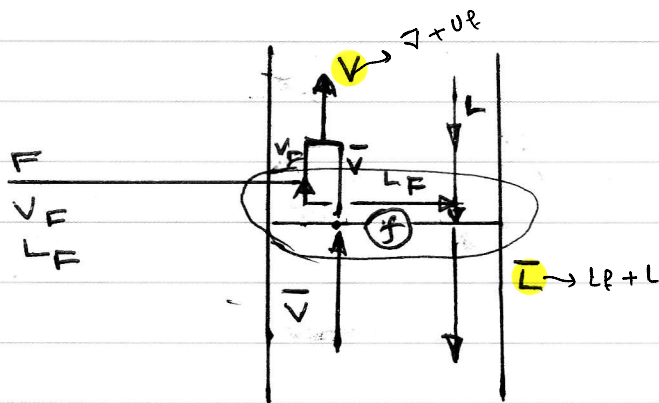


$$y_m = x_{m+1} = x_B$$

or x_B

Note: For a saturated liquid feed the two operating lines intersect at x_f .

Feed line (q-line)



Overall Balance:-

$$F + L + \bar{V} = V + \bar{L}$$

$$(\bar{V} - V) = (\bar{L} - L) - F$$

$$\textcircled{A} \quad \bar{L} = L + qF$$

q : fraction of feed which is liq.
 $\rightarrow \frac{1}{F}$ or $(1-V)$

$$\textcircled{B} \quad \bar{V} = V - (1-q)F$$

stripping $y = \frac{\bar{L}}{V} \cdot x - \frac{B}{V} \cdot x_B$

Enriching $- (y = \frac{L}{V} x + \frac{D}{V} \cdot x_D)$

reverses the line
 from 45° line
 (axis change)

$$(\bar{V} - V) y = (\bar{L} - L) x - (B x_B + D x_D)$$

$$\textcircled{B} \rightarrow (\bar{V} - V) = (q - 1) \cdot F$$

$$\textcircled{A} \rightarrow (\bar{L} - L) = qF$$

$$\frac{\bar{L} - L}{q}$$

$$Bx_B + Dx_D = z_F \cdot F$$

$$y = \frac{q}{q-1} x - \frac{z_F}{q-1}$$

substitute:

$$(q-1) y = q x - z_F$$

$$y = \frac{q}{q-1} x - \frac{z_F}{(q-1)}$$

q-line equation.

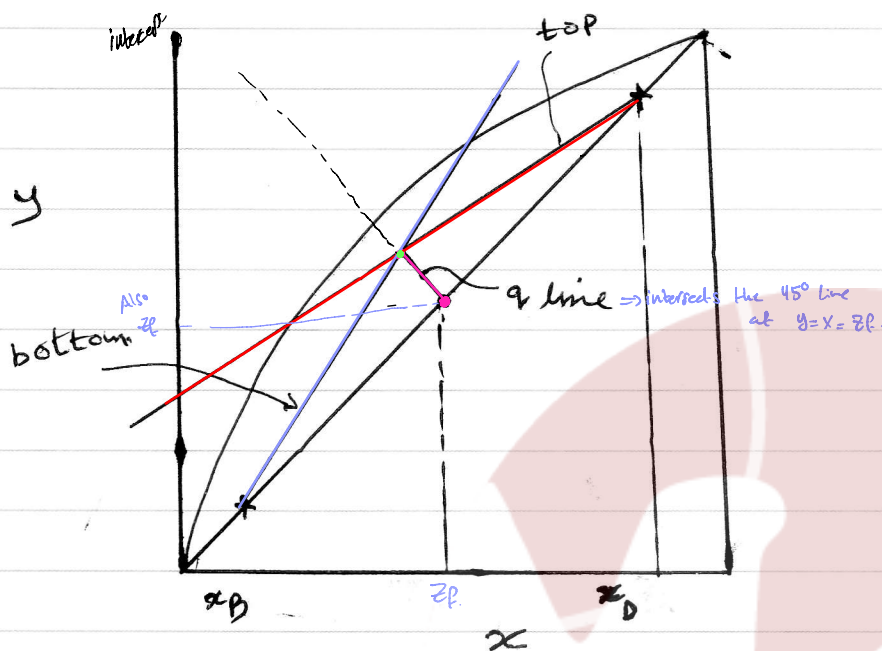
This line is the locus of the points of intersection of stripping and enriching operating lines

Slope = $\frac{q}{q-1}$

Intercept = $-\frac{z_F}{q-1}$

and passes through $y = x = z_F$

→ positive quantity
q-1 → -ve
with another -ve
+ve



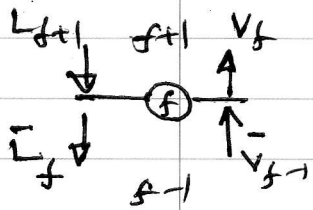
Thermal Condition of feed: → type of the feed (std -)

From MB $(\bar{V} - \bar{V}) = (\bar{L} - \bar{L}) - F$

Enthalpy: $F h_F + L_{f+1} h_{L,f+1} + \bar{V}_f h_{\bar{V},f-1} = \bar{V}_f h_{\bar{V},f} + L_f h_{L,f}$

section 11 page 10

Based on assumption of CMO



$$L_{f+1} = L ; \bar{L}_f = \bar{L}$$

$$V_f = V ; \bar{V}_{f-1} = \bar{V}$$

$$h_{V_f} = h_{\bar{V}, f-1} ; h_{L, f+1} = h_{\bar{L}, f}$$

$$\therefore F h_F + (\bar{V} - V) h_{V_f} = (\bar{L} - L) \cdot h_{\bar{L}, f}$$

Substitute for $(\bar{V} - V) = (\bar{L} - L) - F$.

$$\Rightarrow \underline{F h_F} + \underline{(\bar{L} - L) \cdot h_{V_f}} - \underline{F h_{V_f}} = \underline{(\bar{L} - L) \cdot h_{\bar{L}, f}}$$

$$\frac{\bar{L} - L}{F} = q$$

$$(\bar{L} - L) (h_{V_f} - h_{\bar{L}, f}) = F (h_{V_f} - h_F)$$

$$\frac{\bar{L} - L}{F} = \frac{h_{V_f} - h_F}{h_{V_f} - h_{\bar{L}, f}} = q \text{ of feed.}$$

$\xrightarrow{\text{Enthalpy to vaporize 1 mole}}$
 $\xrightarrow{\text{Latent heat of vaporisation.}}$
 $\xrightarrow{\text{sat vap}} \quad \xrightarrow{\text{sat liq}}$

values of q :

- $q > 1$
- $q = 1$
- $0 < q < 1.0$
- $q = 0$
- $q < 0$

Feed Condition

- cooled liquid
- Saturated liquid
- vapor + liquid.

Saturated vapor

superheated vapor $1 > \text{slope} > 0$

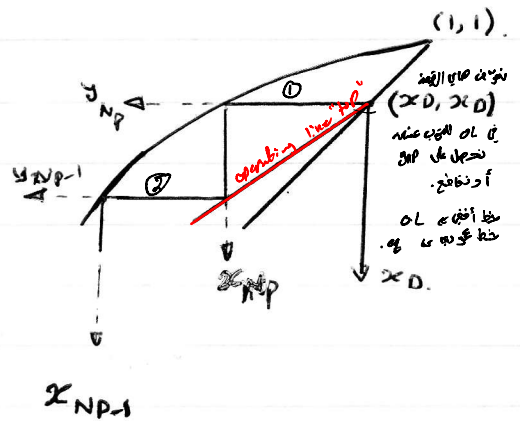
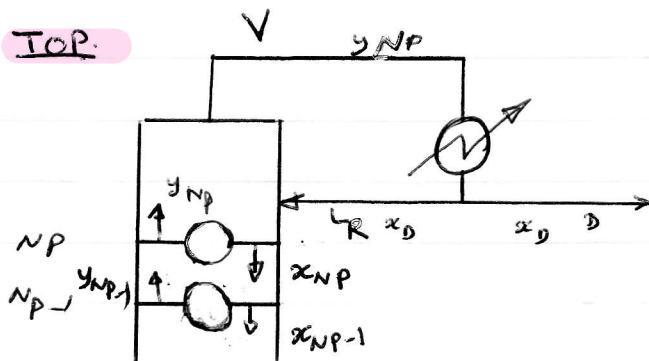
Slope of q -line

- > 1
- ∞
- < 1

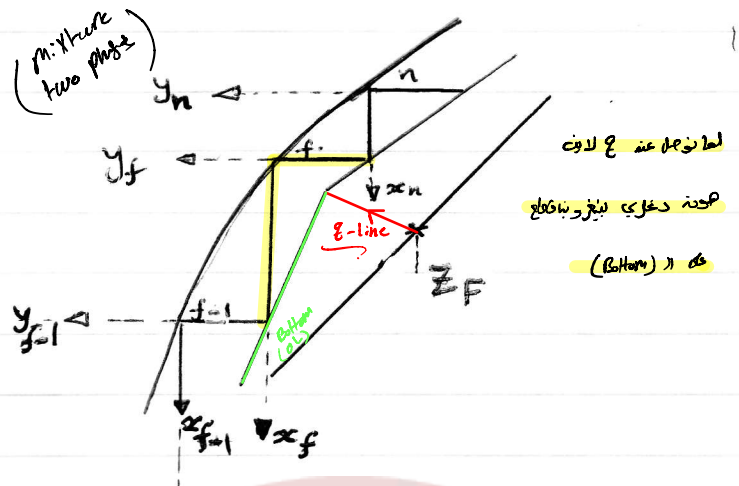
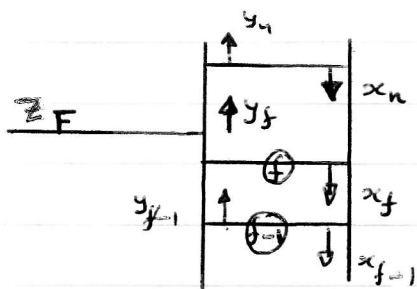
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ask :: believe & recieve

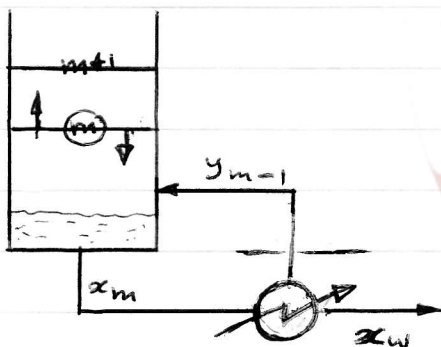
Important portions in fractionation column:



Feed:



Reboiler and bottom stage:



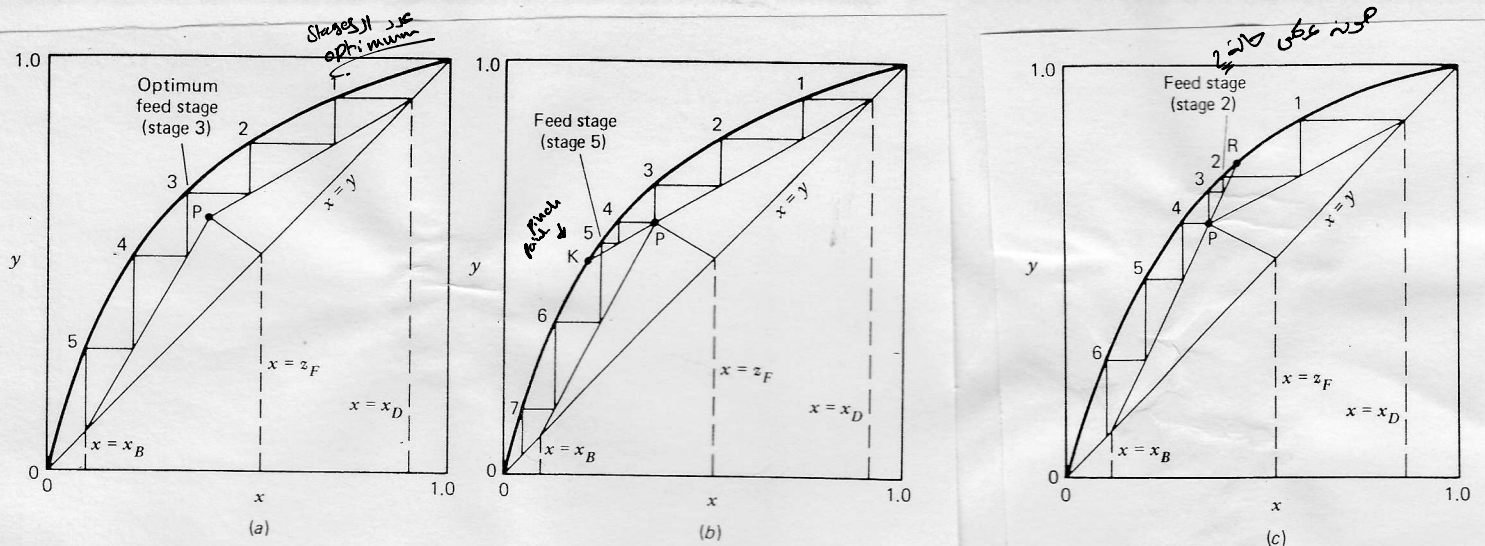


Figure 8.13. Location of feed stage (because of convenience, stages are stepped off and counted in top-down direction). (a) Optimum feed-stage location. (b) Feed-stage location below optimum stage. (c) Feed-stage location above optimum stage.

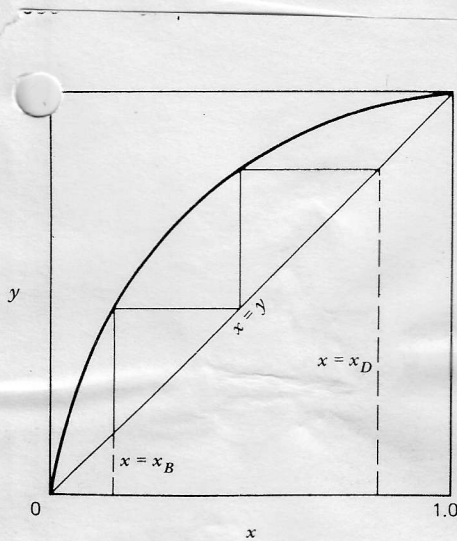


Figure 8.14. Minimum stages, total reflux.

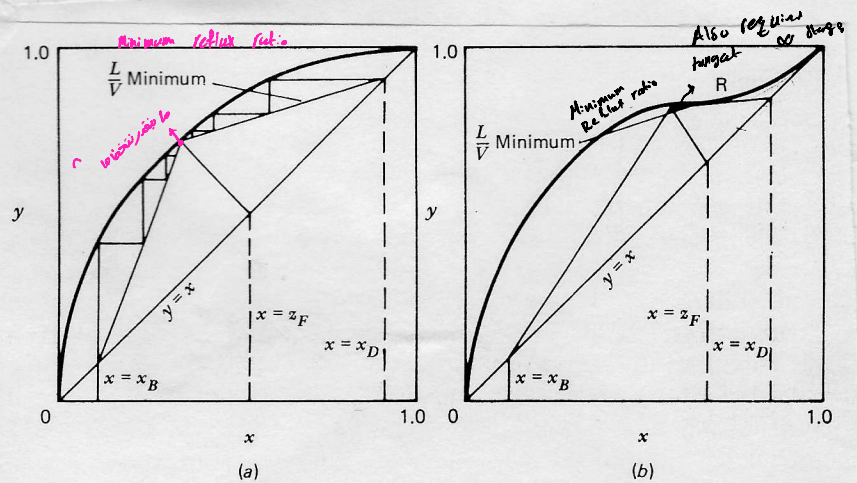


Figure 8.15. Minimum reflux ratio conditions. (a) Intersection of operating lines at equilibrium curve. (b) Operating line tangent to equilibrium curve.

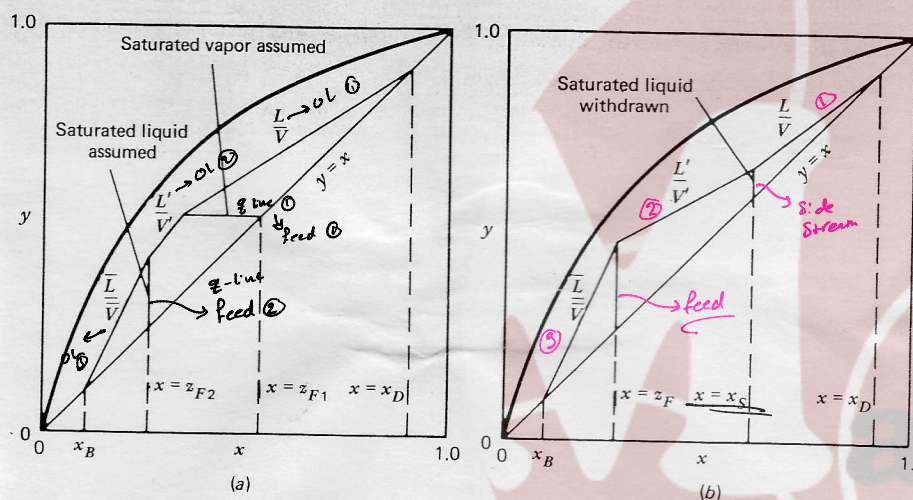


Figure 8.20. Variation of operating conditions. (a) Two feeds (saturated liquid and saturated vapor). (b) One feed, one side stream (saturated liquid).