



0905322- Chemical Engineering Thermodynamics I Lecture 6: Equations of State

Ali Khalaf Al-Matar (aalmatar@ju.edu.jo)
Chemical Engineering Department

The University of Jordan
Amman, Jordan
2019

Outline

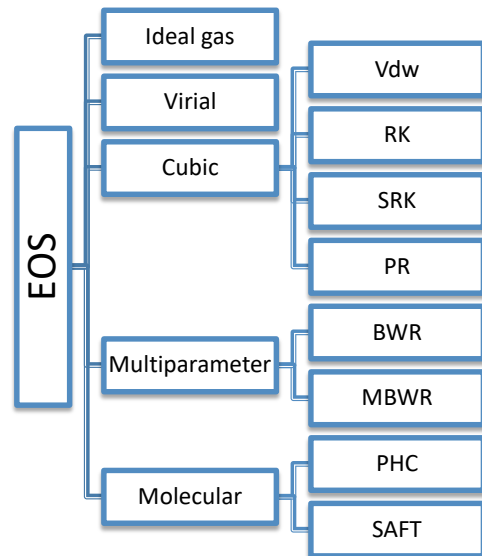
- Volumetric Equations of State
- Ideal Gas (IG) EOS
- Virial EOS
- Generalized Compressibility Factor Chart
- Corresponding States Principle (CSP)
- Cubic EOS
- BWR and MBWR

Volumetric Equations of State

- A mathematical formula that relates the pressure (P), temperature (T), and specific volume (v) of a substance is called an equation of state (EOS).

$$f(P, v, T) = 0$$

$$v = v(T, P)$$

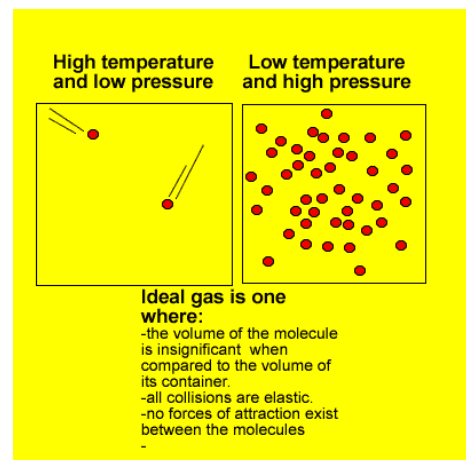


Ideal Gas (IG) EOS

- The easiest yet the least accurate.
- Applies to gas phase only.
- Two main assumptions:
 - Molecular size is zero!
 - No molecular forces.

$$Pv = RT \Rightarrow Z = \frac{Pv}{RT} = 1$$

- Parameter is R called universal gas constant with a value of 8.314 J/mol.K.



Virial EOS

○ A series expansion around the IG limit.

○ Pressure form

$$Z = 1 + B'P + C'P^2 + \dots$$

○ Volume form

$$Z = 1 + \frac{B}{V} + \frac{C}{V^2} + \dots$$

$$B' = \frac{B}{RT}$$

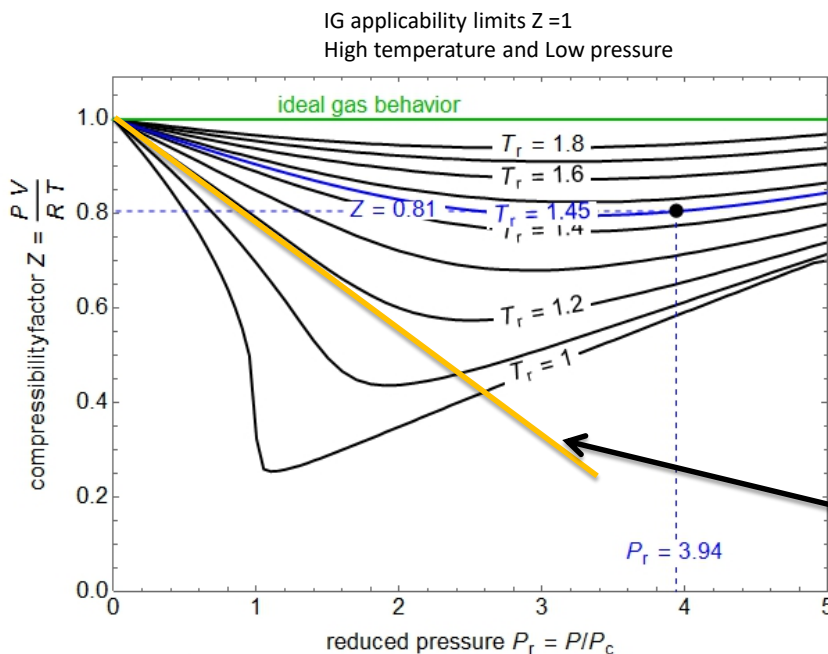
○ More accurate than the IG EOS.

○ Applies to gas phase only.

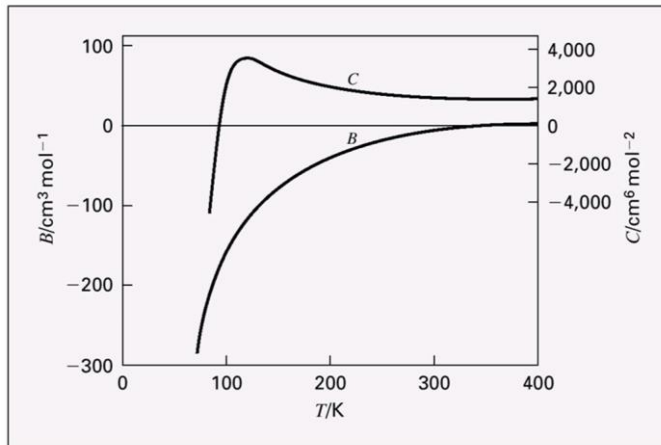
Virial Coefficients

The virial coefficients are function of temperature only. They are related to molecular forces from statistical mechanics

B is related to two body interactions. C is related to three body interactions and so on.



Effect of T on Virial Coefficients



- For $-ve B$: $Z < 1$ (Attractive forces)
- For $+ve B$: $Z > 1$ (Repulsive forces)
- Boyle's temperature $B = 0$; $Z = 1$ (Attractive = repulsive forces)

Second and third virial coefficients for nitrogen (Fig. 3-10 in Smith and van Ness)



Pitzer's Correlation for the Second Virial Coefficient

○Applies to nonpolar gases

$$Z = 1 + \frac{BP}{RT} = 1 + \hat{B} \frac{P_r}{T_r}$$

$$\hat{B} = \frac{BP_c}{RT_c} = B^0 + \omega B^1$$

$$B^0 = 0.083 - \frac{0.422}{T_r^{1.6}}, \quad B^1 = 0.139 - \frac{0.172}{T_r^{4.2}}$$

$$Z = Z^0 + \omega Z^1$$

$$Z^0 = 1 + B^0 \frac{P_r}{T_r}, \quad Z^1 = B^1 \frac{P_r}{T_r}$$

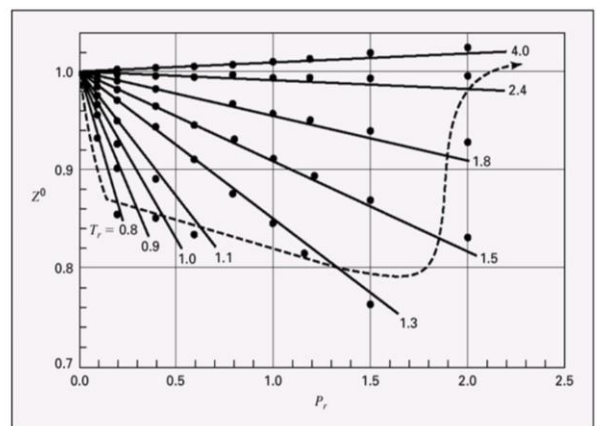


Figure 3.14: Comparison of correlations for Z^0 . The virial-coefficient correlation is represented by the straight lines; the Lee/Kesler correlation, by the points. In the region above the dashed line the two correlations differ by less than 2%.

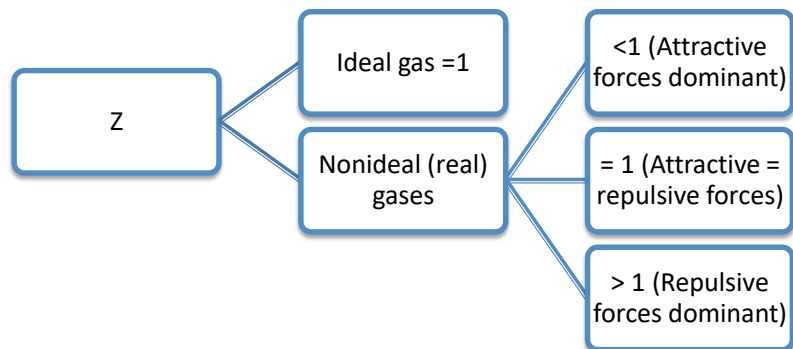


Generalized Compressibility Factor Chart

- The compressibility factor Z can be thought of as the ratio of the volume of the nonideal (real) gas to that of an ideal gas at the same conditions.

$$Z = \frac{Pv}{RT} = \frac{v_{\text{nonideal}}}{v_{\text{Ideal gas}}}$$

$$Pv = ZRT$$



Corresponding States Principle (CSP)

- The Z factor for all gases is approximately the same at the same reduced pressure (P_r) and temperature (T_r).

$$Z = Z(T_r, P_r)$$

- This is the two parameter CSP.
- The chart is for the majority of hydrocarbon gases with $Z_c \sim 0.27$.



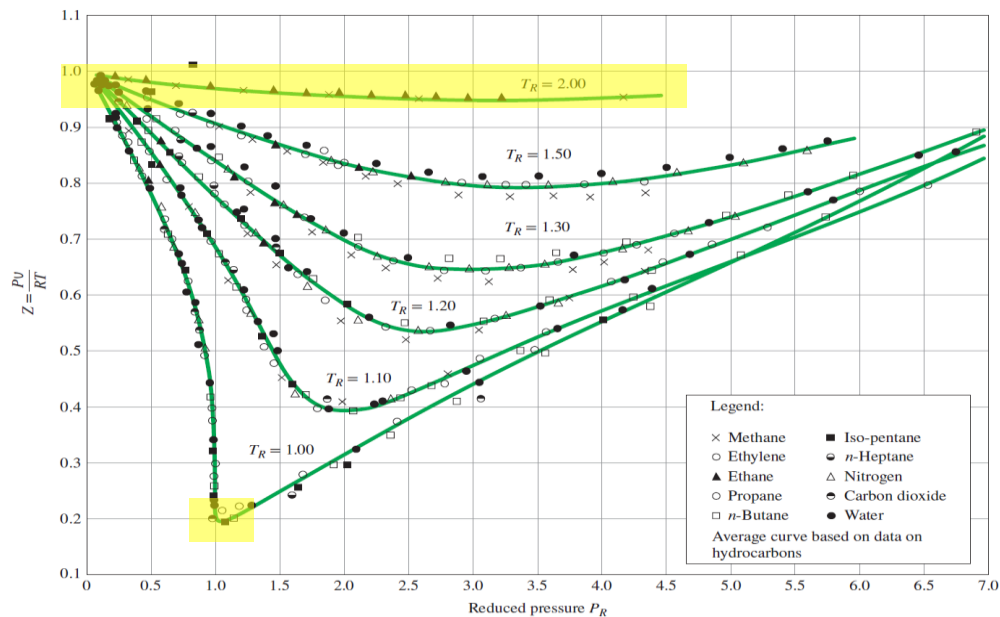


FIGURE 3-48

Comparison of Z factors for various gases.

Source: Gour-Jen Su, "Modified Law of Corresponding States," *Ind. Eng. Chem. (international ed.)* 38 (1946), p. 803.

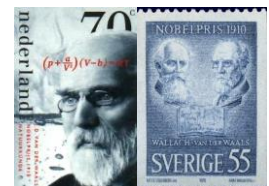
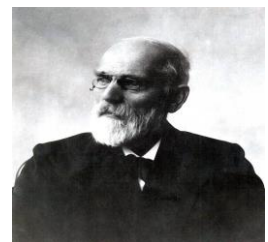
Van der Waal's (vdW) EOS

- Developed in 1873.
- vdW relaxed the assumptions of the ideal gas:
 - Molecules do have a volume.
 - Molecules do have intermolecular forces that are manifested as a pressure exerted on the container wall.
- The first EOS to apply for both the vapor and liquid phases.

$$P = \frac{RT}{v-b} - \frac{a}{v^2}$$

Attractive

Repulsive



vdW EOS Parameters

- The vdW EOS has two parameters
 - A volume correction called **covolume** (b).
 - A pressure correction called **energy parameter** (a)
- Substance specific.
- Obtained from the conditions at the critical point.

$$\left(\frac{\partial P}{\partial v}\right)_{T=T_c} = \left(\frac{\partial^2 P}{\partial v^2}\right)_{T=T_c} = 0$$

$$a = \frac{27}{64} \frac{(RT_c)^2}{P_c}, \quad b = \frac{1}{8} \frac{RT_c}{P_c}$$

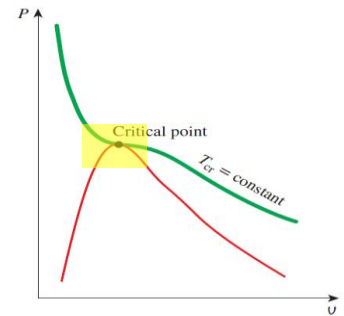


FIGURE 3-55

Critical isotherm of a pure substance has an inflection point at the critical state.

TABLE A-1						
Molar mass, gas constant, and critical-point properties						
Substance	Formula	Molar mass, M kg/kmol	Gas constant, R kJ/kg·K	Critical-point properties		
				Temperature, K	Pressure, MPa	Volume, m ³ /kmol
Air	—	28.97	0.2870	132.5	3.77	0.0883
Ammonia	NH ₃	17.03	0.4882	405.5	11.28	0.0724
Argon	Ar	39.948	0.2081	151	4.86	0.0749
Benzene	C ₆ H ₆	78.115	0.1064	562	4.92	0.2603
Bromine	Br ₂	159.808	0.0520	584	10.34	0.1355
<i>n</i> -Butane	C ₄ H ₁₀	58.124	0.1430	425.2	3.80	0.2547
Carbon dioxide	CO ₂	44.01	0.1889	304.2	7.39	0.0943



Cubic EOS

- vdW is the first cubic EOS (in volume or compressibility factor) successful in qualitatively describing both vapor and liquid phases.
- Yet, it is not accurate.
- Various modifications
 - 1949 Redlick-Kwong (RK) EOS: energy parameter, a , is function of T .
 - 1972 Soave-RK (SRK)
 - 1976 Peng-Robinson (PR)



Cubic EOS

Redlich-Kwong (RK)
$P = \frac{RT}{v-b} - \frac{a/\sqrt{T}}{v(v+b)}$
$a = 0.42748 \frac{(RT_c)^2 \sqrt{T_c}}{P_c}$
$b = 0.08664 \frac{RT_c}{P_c}$

Soave-Redlich-Kwong (SRK)
$P = \frac{RT}{v-b} - \frac{a(T)}{v(v+b)}$
$a(T) = 0.42748 \frac{(RT_c)^2}{P_c} \alpha(T)$
$\sqrt{\alpha(T)} = 1 + \kappa \left(1 - \sqrt{\frac{T}{T_c}} \right)$
$\kappa = 0.480 + 1.57\omega - 0.176\omega^2$
$b = 0.08664 \frac{RT_c}{P_c}$

Peng-Robinson (PR)
$P = \frac{RT}{v-b} - \frac{a(T)}{v(v+b) + b(v-b)}$
$a(T) = 0.45724 \frac{(RT_c)^2}{P_c} \alpha(T)$
$\sqrt{\alpha(T)} = 1 + \kappa \left(1 - \sqrt{\frac{T}{T_c}} \right)$
$\kappa = 0.37464 + 1.5422\omega - 0.26992\omega^2$
$b = 0.07779 \frac{RT_c}{P_c}$



Cubic EOS Coefficients

$$Z^3 + \alpha Z^2 + \beta Z + \gamma = 0$$

	vdW	SRK	PR
α	$-1 - B$	-1	$-1 + B$
β	A	$A - B - B^2$	$A - 2B - 3B^2$
γ	$-AB$	$-AB$	$-AB + B^2 + B^3$
Z_c	0.3750	0.3333	0.3074

$$A = \frac{aP}{(RT)^2} \quad B = \frac{bP}{RT}$$

Initial Guess for solution

Vapor (Vapor like): ideal gas ($Z = 1$).

Liquid: Reduced covolume ($Z = B$).



Benedict-Webb-Rubin (BWR) EOS

○Original BWR

$$P = \frac{RT}{v} + \left(B_0 RT - A_0 - \frac{C_0}{T^2} \right) \frac{1}{v^2} + \frac{bRT - a}{v^3} + \frac{a\alpha}{v^6} + \frac{c}{v^3 T^2} \left(1 + \frac{\gamma}{v^2} \right) e^{-\frac{\gamma}{v^2}}$$

(b) When P is in kPa, \bar{v} is in m^3/kmol , T is in K, and $R_u = 8.314 \text{ kPa}\cdot\text{m}^3/\text{kmol}\cdot\text{K}$, the eight constants in the Benedict-Webb-Rubin equation are as follows:

Gas	a	A_0	b	B_0	c	C_0	α	γ
n-Butane, C_4H_{10}	190.68	1021.6	0.039998	0.12436	3.205×10^7	1.006×10^8	1.101×10^{-3}	0.0340
Carbon dioxide, CO_2	13.86	277.30	0.007210	0.04991	1.511×10^6	1.404×10^7	8.470×10^{-5}	0.00539
Carbon monoxide, CO	3.71	135.87	0.002632	0.05454	1.054×10^5	8.673×10^5	1.350×10^{-4}	0.0060
Methane, CH_4	5.00	187.91	0.003380	0.04260	2.578×10^5	2.286×10^6	1.244×10^{-4}	0.0060
Nitrogen, N_2	2.54	106.73	0.002328	0.04074	7.379×10^4	8.164×10^5	1.272×10^{-4}	0.0053

Source: Kenneth Wark, *Thermodynamics*, 4th ed. (New York: McGraw-Hill, 1983), p. 815, table A-21M. Originally published in H. W. Cooper and J. C. Goldfrank, *Hydrocarbon Processing* 46, no. 12 (1967), p. 141.



Modified Benedict-Webb-Rubin (MBWR) EOS

○Modified BWR (MBWR)

$$P = \sum_{n=1}^9 \frac{a_n}{v^n} + e^{-\frac{\gamma}{v^2}} \sum_{n=10}^{17} \frac{a_n}{v^{2n-17}}, \quad \gamma = 1 / \rho_c^2$$

$$P = \sum_{n=1}^9 a_n \rho^n + e^{-\gamma \rho^2} \sum_{n=10}^{17} a_n \rho^{2n-17}$$

Download the student version of NIST's [refprops](#) software and check the pure component options available.



EXAMPLE 3–13 Different Methods of Evaluating Gas Pressure

Predict the pressure of nitrogen gas at $T = 175 \text{ K}$ and $v = 0.00375 \text{ m}^3/\text{kg}$ on the basis of (a) the ideal-gas equation of state, (b) the van der Waals equation of state, (c) the Beattie-Bridgeman equation of state, and (d) the Benedict-Webb-Rubin equation of state. Compare the values obtained to the experimentally determined value of $10,000 \text{ kPa}$.

SOLUTION The pressure of nitrogen gas is to be determined using four different equations of state.

Properties The gas constant of nitrogen gas is $0.2968 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K}$ (Table A–1).

Analysis (a) Using the ideal-gas equation of state, the pressure is found to be

$$P = \frac{RT}{v} = \frac{(0.2968 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K})(175 \text{ K})}{0.00375 \text{ m}^3/\text{kg}} = \mathbf{13,851 \text{ kPa}}$$

which is in error by 38.5 percent.

(b) The van der Waals constants for nitrogen are determined from Eq. 3–23 to be

$$a = 0.175 \text{ m}^6\cdot\text{kPa}/\text{kg}^2$$

$$b = 0.00138 \text{ m}^3/\text{kg}$$

From Eq. 3–22,

$$P = \frac{RT}{v - b} - \frac{a}{v^2} = \mathbf{9471 \text{ kPa}}$$

which is in error by 5.3 percent.



(c) The constants in the Beattie-Bridgeman equation are determined from Table 3–4 to be

$$A = 102.29$$

$$B = 0.05378$$

$$c = 4.2 \times 10^4$$

Also, $\bar{v} = Mv = (28.013 \text{ kg/kmol})(0.00375 \text{ m}^3/\text{kg}) = 0.10505 \text{ m}^3/\text{kmol}$. Substituting these values into Eq. 3–24, we obtain

$$P = \frac{R_u T}{\bar{v}^2} \left(1 - \frac{c}{\bar{v} T^3} \right) (\bar{v} + B) - \frac{A}{\bar{v}^2} = \mathbf{10,110 \text{ kPa}}$$

which is in error by 1.1 percent.

(d) The constants in the Benedict-Webb-Rubin equation are determined from Table 3–4 to be

$$a = 2.54$$

$$A_0 = 106.73$$

$$b = 0.002328$$

$$B_0 = 0.04074$$

$$c = 7.379 \times 10^4$$

$$C_0 = 8.164 \times 10^5$$

$$\alpha = 1.272 \times 10^{-4}$$

$$\gamma = 0.0053$$

Substituting these values into Eq. 3–26 gives

$$P = \frac{R_u T}{\bar{v}} + \left(B_0 R_u T - A_0 - \frac{C_0}{T^2} \right) \frac{1}{\bar{v}^2} + \frac{b R_u T - a}{\bar{v}^3} + \frac{a\alpha}{\bar{v}^6} + \frac{c}{\bar{v}^3 T^2} \left(1 + \frac{\gamma}{\bar{v}^2} \right) e^{-\gamma/\bar{v}^2} = \mathbf{10,009 \text{ kPa}}$$

which is in error by only 0.09 percent. Thus, the accuracy of the Benedict-Webb-Rubin equation of state is rather impressive in this case.

