

Question 1: [7 points]

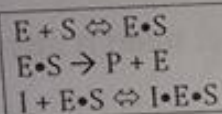
(a) [5 pts] Fill in the space:

1- The class of enzyme that catalyzes the reaction  $A + B + E \rightarrow AB + E$  is called Ligase.

combination → ✓

2- Holoenzyme ✓ refers to enzyme-cofactor complex, and the inactive form of the enzyme-cofactor complex for a specific reaction is called Apoenzyme ✓.

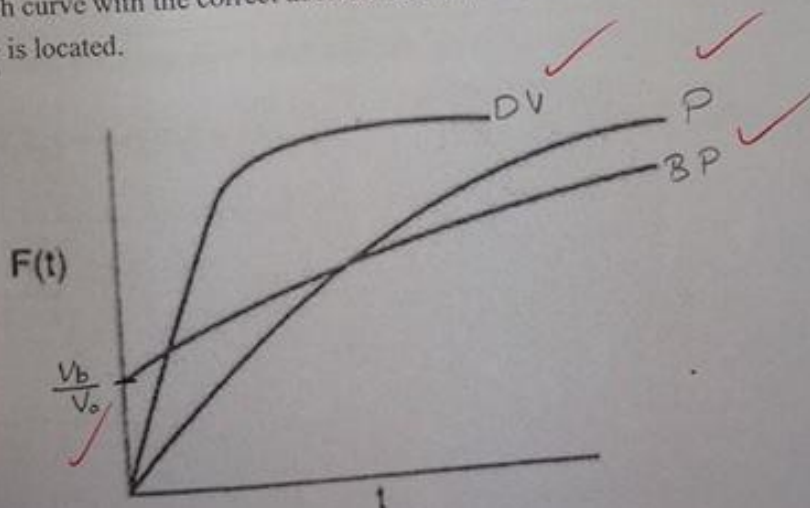
3- The following reaction steps describe the Uncompetitive ✓ enzyme inhibition.



4- One drawback to the step injection technique is needs large amount of tracer  
so if the tracer was expensive → using of pulse injection is better.

5- Only for ✓ reactions, knowledge of the RTD is sufficient to predict conversion.

b) [2 pts] The figure below shows a comparison of  $F(t)$  for CSTR under perfect operation (P), bypassing (BP), and dead volume (DV). The labeling is missing! Label each curve with the correct abbreviation (P, BP, and DV), and show where  $\frac{V_b}{V_0}$  is located.



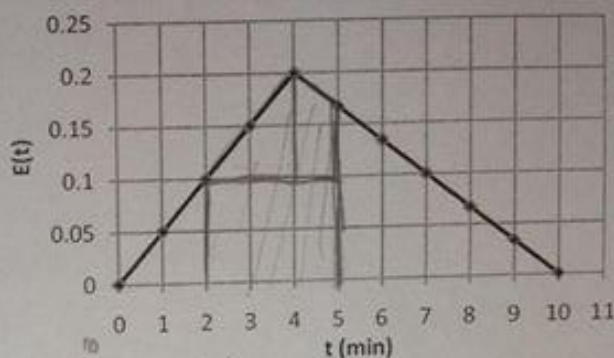
Question 3: [10 points]

2.5

An isothermal pulse test on a piece of reaction equipment gave the following results: The output concentrations rose linearly from zero to 0.5 mmol/L in 5 minutes, and then fell linearly to zero in 10 minutes after reaching the maximum value.

The RTD resulted from this experiment is as shown:

$$\begin{aligned} E(t) &= 0.05t & \text{for } 0 < t < 4 \text{ min} \\ E(t) &= (1-0.1t)/3 & \text{for } 4 < t < 10 \text{ min} \\ E(t) &= 0 & \text{for } t > 10 \text{ min} \end{aligned}$$



- (a) What is the mean residence time  $t_m$ ?  $t_m = \int t \cdot E(t) dt$   
 (b) What fraction of the material spends between 2 and 5 min in the reactor?

The second order liquid phase reaction  $2A \rightarrow B$  is carried out in the system.

The entering concentration is 2 mol/L and the specific reaction rate ( $k$ ) is 0.2 L/(mol · min).

- (c) For this reaction, what is the conversion after 8 minutes in an ideal batch reactor?  
 (d) What is the conversion predicted by the segregation model?

t	E(t)	t · E(t)
0	0	0
1	0.05	0.05
2	0.1	0.2
3	0.15	0.45
4	0.2	0.8
5	0.167	0.835
6	0.133	0.798
7	0.1	0.7
8	0.067	0.536
9	0.033	0.297
10	0	0
11	0	0

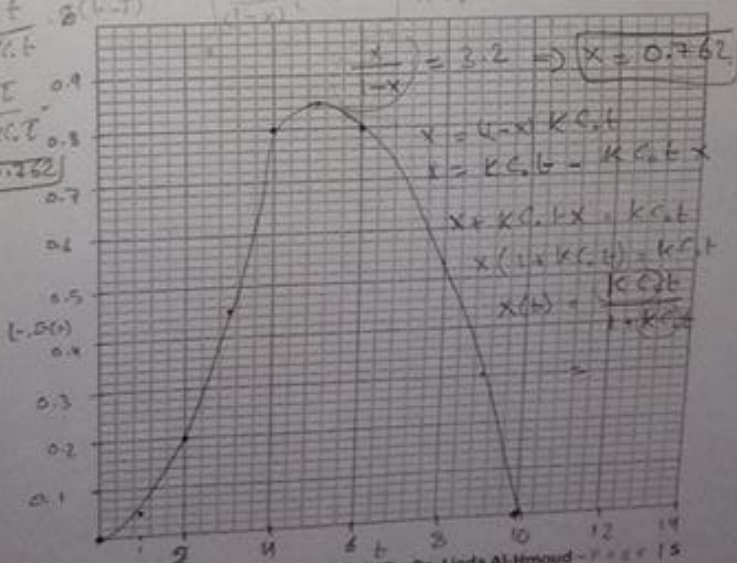
$$AUC = \int t \cdot E(t) dt = \frac{1}{2} \cdot 10 \cdot 0.835 = 4.175$$

$$t_m = 4.175$$

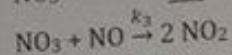
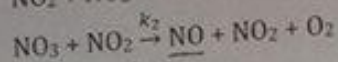
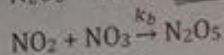
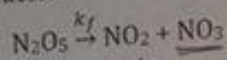
or from integration

$$\begin{aligned} t_m &= \int t \cdot (0.05t) dt + \int t \cdot \frac{(1-0.1t)}{3} dt \\ &= 1.062 + 3.6 \\ &= 4.67 \end{aligned}$$

$$\begin{aligned} \bar{x} &= \int x(t) E(t) dt \\ N_0 \frac{dx}{dt} &= -r_A V \\ C_{A0} \frac{dx}{dt} &= k C_{A0}^2 (1-x)^2 \\ \frac{1}{(1-x)^2} dx &= k C_{A0} dt \end{aligned}$$



B. [6 points] If the reaction  $2\text{N}_2\text{O}_5 \rightarrow 4\text{NO}_2 + \text{O}_2$  follows the following mechanism, where  $\text{NO}_3$  and  $\text{NO}$  are active intermediates:



Use the pseudo-steady-state-hypothesis to derive the rate law ( $r_{\text{O}_2}$ ).

$$r_{\text{O}_2} = k_2 [\text{NO}_3] [\text{NO}_2]$$

$$r_{\text{NO}_3} = k_f [\text{N}_2\text{O}_5] - k_b [\text{NO}_2] [\text{NO}_3] - k_2 [\text{NO}_3] [\text{NO}_2] - k_3 [\text{NO}_3] [\text{NO}] = 0$$

$$[\text{NO}_3] = \frac{k_f [\text{N}_2\text{O}_5]}{k_b [\text{NO}_2] + k_2 [\text{NO}_2] + k_3 [\text{NO}]}$$

$$r_{\text{NO}} = k_2 [\text{NO}_3] [\text{NO}_2] - k_3 [\text{NO}_3] [\text{NO}] = 0$$

$$[\text{NO}] = \frac{k_2 [\text{NO}_2] [\text{NO}_2]}{k_3 [\text{NO}_3]}$$

$$[\text{NO}] = \frac{k_2 k_f [\text{N}_2\text{O}_5] [\text{NO}_2] (k_b [\text{NO}_2] + k_2 [\text{NO}_2] + k_3 [\text{NO}])}{(k_b [\text{NO}_2] + k_2 [\text{NO}_2] + k_3 [\text{NO}]) \cdot k_3 \cdot k_f [\text{N}_2\text{O}_5]}$$

$$[\text{NO}] = \frac{k_2}{k_3} [\text{NO}_2]$$

$$\Rightarrow r_{\text{O}_2} = \frac{k_2 k_f [\text{N}_2\text{O}_5] [\text{NO}_2]}{k_b [\text{NO}_2] + k_2 [\text{NO}_2] + \frac{k_3 k_2}{k_3} [\text{NO}_2]}$$

$$r_{\text{O}_2} = \frac{k_2 k_f [\text{N}_2\text{O}_5] [\text{NO}_2]}{k_b [\text{NO}_2] + 2 k_2 [\text{NO}_2]} \quad \times$$

Question 2: [13 points]

11.5

A. [7 points] The enzymatic hydrolysis of starch was carried out with and without maltose added.

Starch  $\rightarrow$   $\alpha$ -dextrin  $\rightarrow$  Limit dextrin  $\rightarrow$  Maltose

Enzyme.

The following data were obtained:

No Inhibition		Maltose Inhibition ( $I = 12.7 \text{ mg/L}$ )	
$C_S \text{ (g/L)}$	$-r_S \text{ (relative)}$	$C_S \text{ (g/L)}$	$-r_S \text{ (relative)}$
12.5	100	10	77
9.0	92	5.15	56
4.25	70	2.0	30
1.0	29	1.67	26

(a) Calculate  $V_{max}$  and the Michaelis-Menten constant  $K_M$  for starch hydrolysis

(b) Using Lineweaver-Burk plot ( $\frac{1}{-r_S}$  vs.  $\frac{1}{C_S}$ ), determine the type of maltose inhibition, then calculate  $K_I$ .

$$-r_S = \frac{V_{max} \cdot C_S}{K_M + C_S} \rightarrow \frac{1}{-r_S} = \frac{K_M}{V_{max}} \cdot \frac{1}{C_S} + \frac{1}{V_{max}}$$

$\frac{1}{C_S}$	$\frac{1}{-r_S}$
8	0.010
11	0.011
0.235	0.014
1	0.034

$$\frac{1}{V_{max}} = 0.008 \rightarrow V_{max} = 125$$

$$\text{slope} = \frac{\Delta y}{\Delta x} = \frac{0.034 - 0.008}{1 - 0} = 0.026$$

$$\text{or } \frac{\Delta y}{\Delta x} = \frac{0.026 - 0.008}{0.7 - 0.46} = 0.025$$

$$\frac{K_M}{125} = 0.025 \rightarrow K_M = 3.125$$

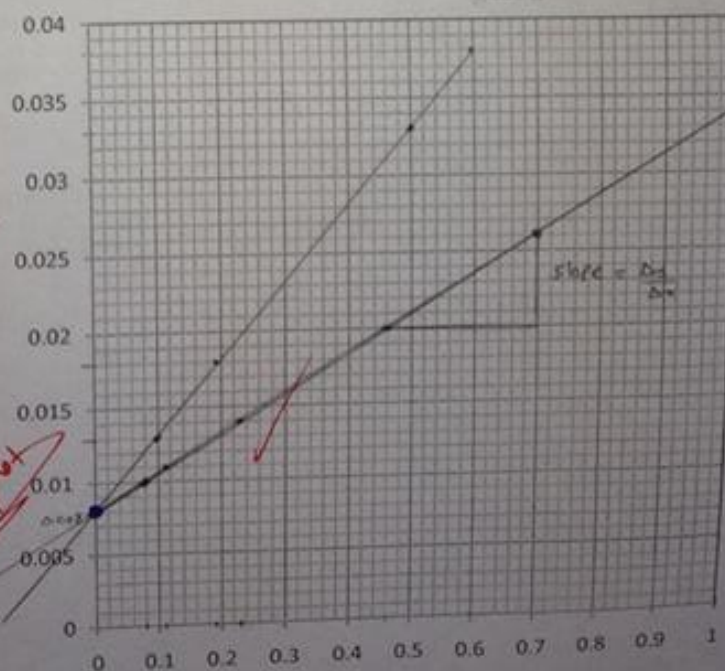
$\frac{1}{C_S}$	$\frac{1}{-r_S}$
0.1	0.013
0.144	0.018
0.5	0.033
0.549	0.038

Same intercept  $\Rightarrow$  Competitive

$$-r_S = \frac{V_{max} \cdot C_S}{C_S + K_M \left[1 + \frac{I}{K_I}\right]}$$

$$77 = \frac{125 \cdot 10}{10 + 3.125 \left[1 + \frac{12.7}{K_I}\right]}$$

$$\Rightarrow K_I = 12.766$$



$$10 + 3.125 \left(1 + \frac{12.7}{K_I}\right) = 16.239 \Rightarrow 1 + \frac{12.7}{K_I} = 1.499$$

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The University of Jordan  
Faculty of Engineering & Technology  
Chemical Engineering Department

(0905422) Chemical Reaction Engineering II

Second Semester – 2016/2017

## Midterm Exam

Name: \_\_\_\_\_

ID # \_\_\_\_\_

Dear students:

Answer all questions to the best of your ability and knowledge.

Start with the easiest question first. Use only the available space.

*Good Luck!*

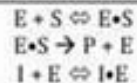
### Question 1: [12 points]

(a) [5 pts] Fill in the space:

1- PSSH refers to \_\_\_\_\_.

2- The class of enzyme that catalyzes the reaction  $AH_2 + B + E \rightarrow A + BH_2 + E$  is called \_\_\_\_\_.

3- The following reaction steps describe the \_\_\_\_\_ enzyme inhibition.



4- \_\_\_\_\_ refers to enzyme-cofactor complex, and the inactive form of the enzyme-cofactor complex for a specific reaction is called \_\_\_\_\_.

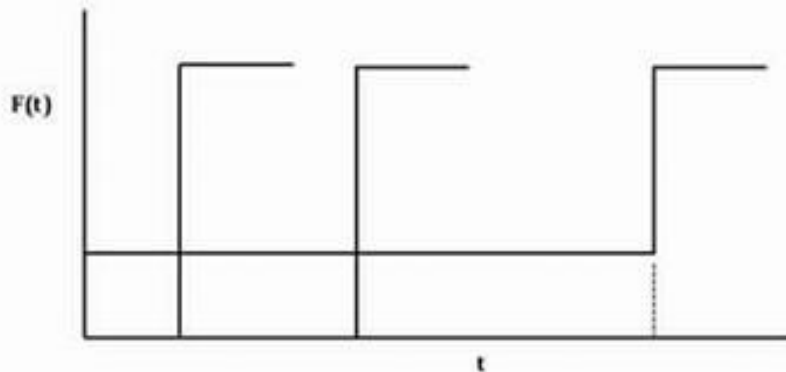
5- In maximum mixedness model, mixing occurs at \_\_\_\_\_ point.

(b) [4 pts] There are two models for substrate-enzyme interactions, what are they? Draw a sketch to show how each one works.

(c) [3 pts] The figure below shows a comparison of PFR under perfect operation (P), bypassing



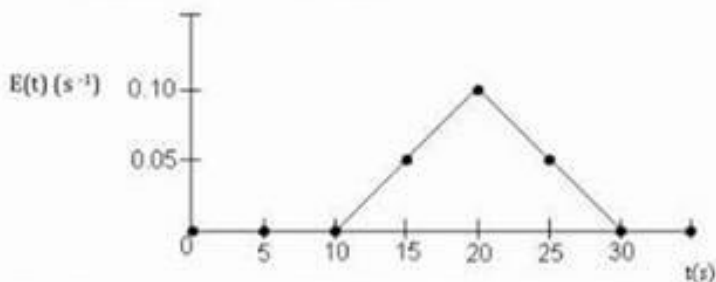
- (c) [3 pts] The figure below shows a comparison of PFR under perfect operation (P), bypassing (BP), and dead volume (DV). The labeling is missing! Label each curve with the correct abbreviation (P, BP, and DV), and show where  $\tau_{50}$ ,  $\tau_r$ , and  $\tau_{10}$  should be on the x-axis.



**Question 2: [9 points]**

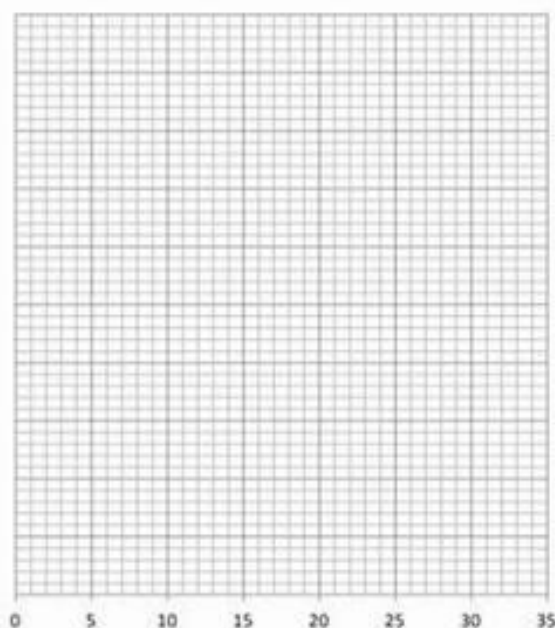
The second order reaction  $2A \rightarrow B + C$  occurs in the liquid phase. The RTD function for the reactor in which it is to be carried out is given by

$$\begin{aligned} E(t) &= 0 & \text{for } 0 < t < 10 \\ E(t) &= 0.01(t-10) & \text{for } 10 < t < 20 \\ E(t) &= 0.01(30-t) & \text{for } 20 < t < 30 \\ E(t) &= 0 & \text{for } t > 30 \end{aligned}$$



The entering concentration is 2 mol/L and the specific reaction rate is 0.06 L/(mol.s).

- What is the mean residence time  $t_m$ ?
- What is the standard deviation  $\sigma$ ?
- What is the conversion after 30 seconds in a batch reactor?
- What is the conversion predicted by the segregation model?



(0905422) Chemical Reaction Engineering II – Midterm Exam – Second Semester 2016/2017 – Dr. Unda Al-Hmoud - Page | 3

**Question 3: [9 points]**

Bakers' yeast oxygen uptake is found to follow Michaelis-Menten mechanism, and inhibited by sulfanilamide. The following data were obtained in a particular medium at 23 °C and various oxygen partial pressures:

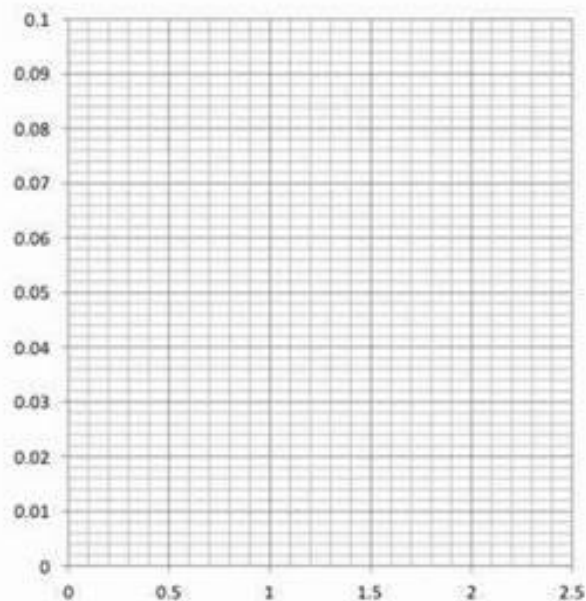
O <sub>2</sub> partial pressure, $P_{O_2}$ (mm Hg)	O <sub>2</sub> uptake rate (no sulfanilamide) $-r_{O_2}$ (μL O <sub>2</sub> /(h.mg cells))	O <sub>2</sub> uptake rate (20 mg sulfanilamide/mL) $-r_{O_2}$ , inhibited (μL O <sub>2</sub> /(h.mg cells))
0.0	0.0	0.0
0.5	23.5	17.4

**Question 3: [9 points]**

Bakers' yeast oxygen uptake is found to follow Michaelis-Menten mechanism, and inhibited by sulfanilamide. The following data were obtained in a particular medium at 23 °C and various oxygen partial pressures:

O <sub>2</sub> partial pressure, $P_{O_2}$ (mm Hg)	O <sub>2</sub> uptake rate (no sulfanilamide) $-r_{O_2}$ ( $\mu\text{L O}_2/(\text{h.mg cells})$ )	O <sub>2</sub> uptake rate (20 mg sulfanilamide/mL) $-r_{O_2}$ , inhibited ( $\mu\text{L O}_2/(\text{h.mg cells})$ )
0.0	0.0	0.0
0.5	23.5	17.4
1.0	33.0	25.6
2.0	39.0	33.4
4.0	42.0	40.0

- (a) Calculate the maximum  $Q_{O_2}$  ( $V_{max}$ ) and the Michaelis-Menten constant  $K_M$ .  
 (b) Using Lineweaver-Burk plot ( $\frac{1}{-r_s}$  vs.  $\frac{1}{S}$ ), determine the type of inhibition sulfanilamide that causes the O<sub>2</sub> uptake to change, then find  $K_i$ .



### Information Sheet

For batch reactor:

$$\frac{dX}{dt} = \frac{-r_A V}{N_{A0}}$$

For moving-bed reactor:

$$-\frac{da}{dW} = \frac{k_d}{U} a^n$$

Midterm Exam

Name: عبدالله النوراني

ID # 0147452

Dear students:

Answer all questions to the best of your ability and knowledge.

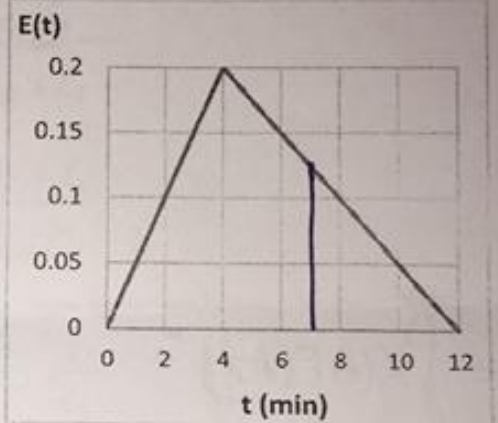
Start with the easiest question first. Use only the available space.

Good Luck!

Question 1: [10 points]

The elementary liquid phase isomerization reaction  $A \rightarrow B$  ( $k = 0.3 \text{ min}^{-1}$ ) is to be carried out in a continuous flow reactor. Tracer experiments were carried out and found that the reactor has the following RTD

$$E(t) = \begin{cases} \frac{t}{20}, & 0 < t < 4 \text{ min} \\ \frac{12-t}{40}, & 4 < t < 12 \text{ min} \end{cases}$$



- (a) Of what type do you expect this reactor to be? ~~CSTR~~  
 (b) Find the fraction of material that spends at least 7 minutes in the reactor.  
 (c) Calculate the mean residence time  $t_m$ .  
 (d) What is the conversion predicted by the segregation model? (use Simpson's one-third rule)

(a) CSTR because liquid phase

(b)  $\int_0^7 E(t) dt = \frac{1}{3} [0 + 4(0.05) + 2(0.1) + 4(0.15) + 2(0.2) + 4(0.175) + 2(0.15) + 0.125]$   
 $= 0.8416$

	0	1	2	3	4	5	6	7	8	9	10	11	12
E(t)	0	0.05	0.1	0.15	0.2	0.175	0.15	0.125	0.1	0.075	0.05	0.025	0
tE(t)	0	0.05	0.2	0.45	0.8	0.875	0.9	0.875	0.8	0.675	0.5	0.275	0

(c)  $t_m = \int_0^{12} t E(t) dt = \frac{1}{3} [0 + 4(0.05) + 2(0.2) + 4(0.45) + 2(0.8) + 4(0.875) + 2(0.9) + 4(0.875) + 2(0.8) + 4(0.675) + 2(0.5) + 4(0.275) + 0]$   
 $= 6.4 \text{ min}$

Question 2: [9 points]

Beef catalase has been used to accelerate the decomposition of hydrogen peroxide to yield water and oxygen. The concentration of hydrogen peroxide is given as a function of time for a reaction mixture with a pH of 6.76 maintained at 30°C.

t (min)	0	2	5	10
C <sub>H<sub>2</sub>O<sub>2</sub></sub> (mol/L)	0.10	0.079	0.053	0.025

- (a) To what enzyme class does beef catalase belong?  $\alpha$ -amylase
- (b) Determine the Michaelis-Menten parameters  $V_{max}$  and  $K_M$ .
- (c) If the total enzyme concentration is tripled;
- how will the values of the parameters  $V_{max}$  and  $K_M$  change?
  - what CSTR residence time ( $\tau$ ) will be required to reduce  $C_{H_2O_2}$  from 0.10 mol/L to 0.025 mol/L with triple  $E_T$ ?

$$-r_s = \frac{V_{max} [S]}{K_M + [S]}$$

$$\frac{V}{r_s} = \frac{K_M}{V_{max}} + \frac{1}{V_{max}}$$

$$-V_{max} \int_0^t dt = \int_{C_{s0}}^{C_s} \frac{K_M}{C_s} \frac{1}{C_s} dC_s + \int_{C_{s0}}^{C_s} \frac{C_s}{C_s} dC_s$$

$$-V_{max} t = K_M \ln \frac{C_s}{C_{s0}} + C_s - C_{s0}$$

$$-V_{max} = \frac{K_M}{t} \ln \frac{C_s}{C_{s0}} + \frac{C_s - C_{s0}}{t}$$

$$\frac{C_{s0} - C_s}{t} = \frac{K_M}{t} \ln \frac{C_s}{C_{s0}} + V_{max}$$

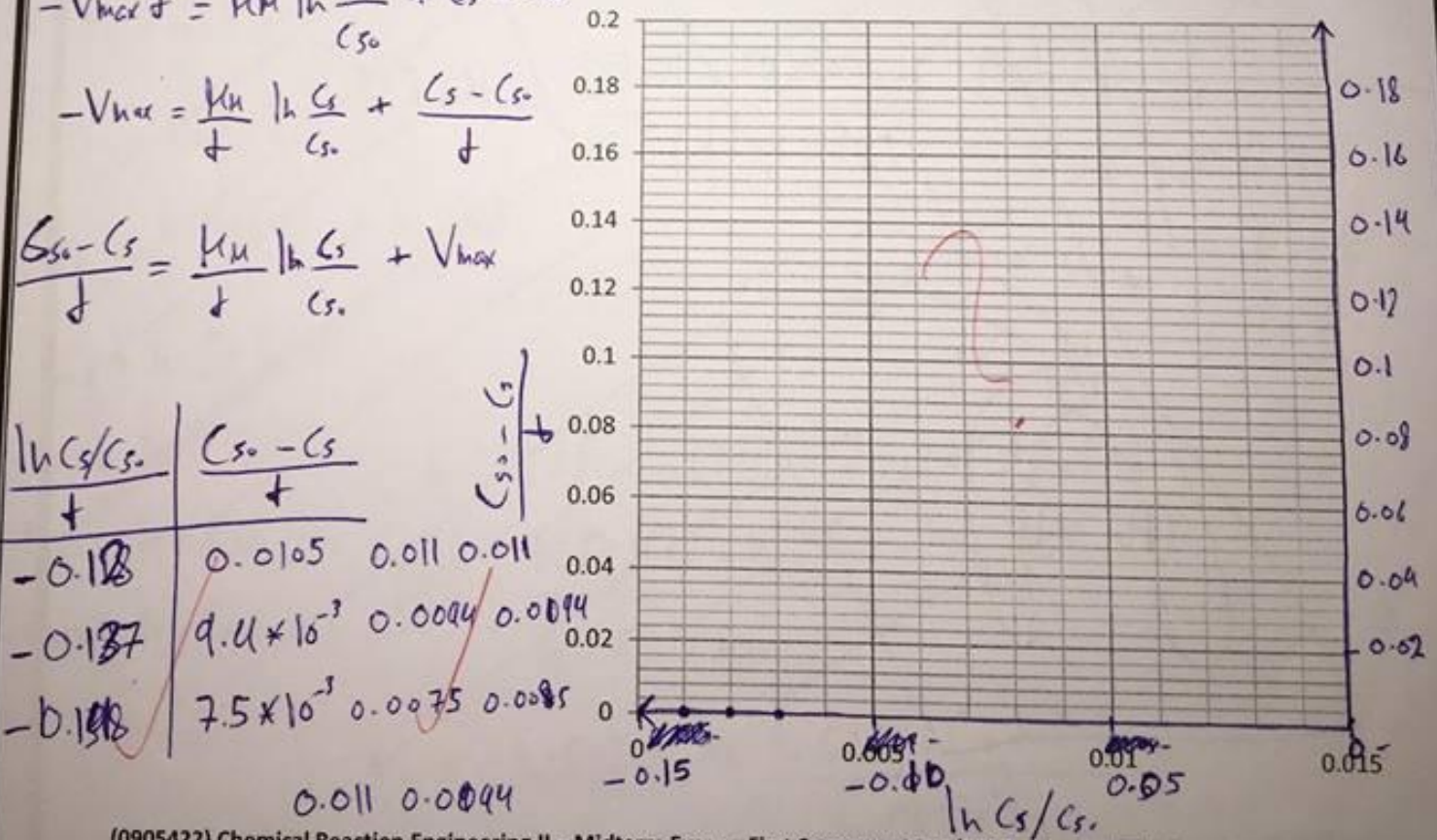
$\ln C_s / C_{s0}$	$\frac{C_{s0} - C_s}{t}$	$\frac{C_s}{C_{s0}}$
-0.18	0.0105	0.011
-0.137	$9.4 \times 10^{-3}$	0.0094
-0.138	$7.5 \times 10^{-3}$	0.0085

$$-\frac{dC_s}{dt} = -r_s$$

$$= \frac{V_{max} C_s}{K_M + C_s}$$

$$-\frac{dt}{dC_s} = \frac{K_M + C_s}{V_{max} C_s}$$

$$-\frac{dt}{dC_s} = \frac{K_M}{V_{max}} \frac{1}{C_s} + \frac{1}{V_{max}}$$

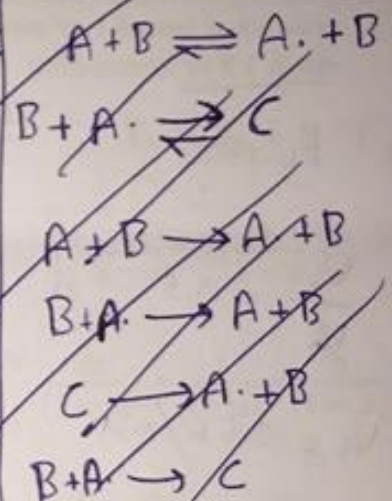
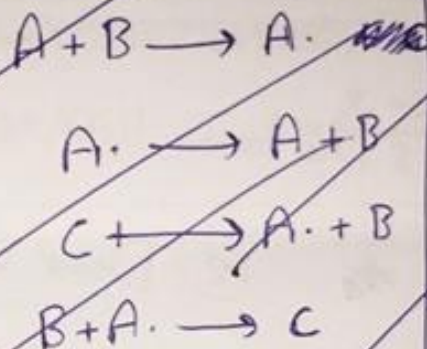
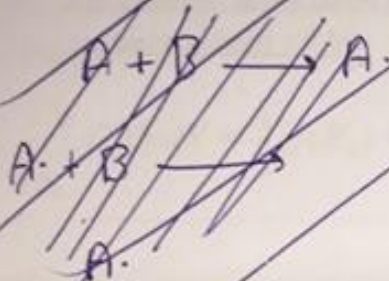
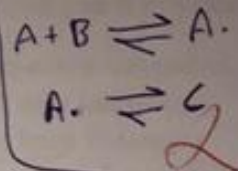
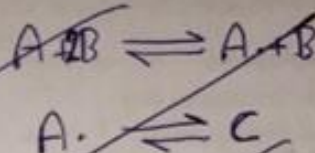
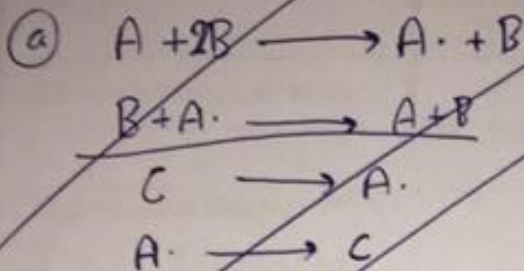
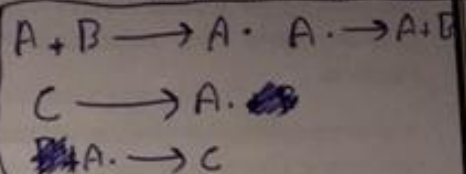


Question 3: [7 points]

The rate of the reversible reaction  $A + B \rightleftharpoons C$  has been studied. Experimental data show that the rate of this reaction is

$$r_c = \frac{k_1 C_A C_B - k_2 C_C}{K + C_B}$$

- (a) Suggest a mechanism consistent with the rate law.  
(b) Sketch the reaction pathways that represent your mechanism.



$$-r_c = k_3 [C]$$

$$+r_{c4} = k_4 [A \cdot]$$

$$r_c = -k_3 [C] + k_4 [A \cdot]$$

$$r_{p.1} = k_1 [A][B]^2$$

$$-r_{p.2} = k_2 [B][A \cdot]$$

$$r_{p.3} = k_3 [C]$$

$$-r_{p.4} = k_4 [A \cdot]$$

$$k_1 [A][B]^2 - k_2 [B][A \cdot] + k_3 [C] - k_4 [A \cdot]$$

$$[A \cdot] = \frac{k_1 [A][B]^2 + k_3 [C]}{k_2 [B] + k_4}$$

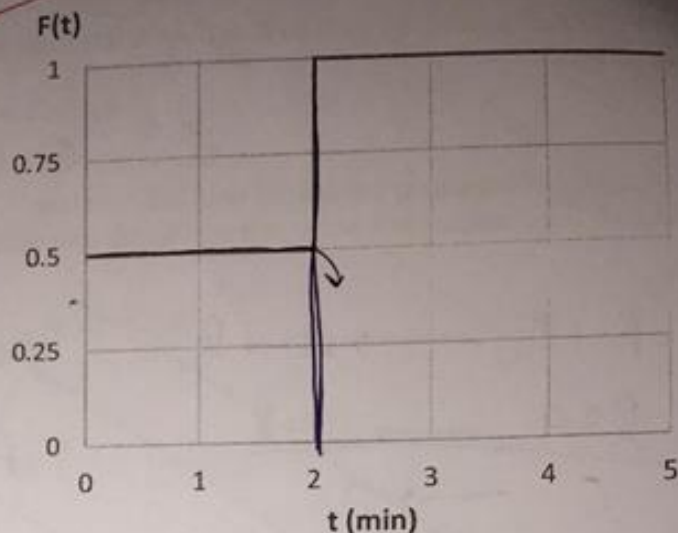
$$r_c = -k_3 [C] + k_4 \frac{k_1 [A][B]^2 + k_3 [C]}{k_2 [B] + k_4}$$

$$k_2 [B] + k_4$$

Question 4: [4 points]

There is a  $2 \text{ m}^3$  tubular reactor in storage that is to be used to carry out some liquid-phase reaction.

A tracer experiment was carried out with volumetric rate of  $1 \text{ m}^3/\text{min}$ , and reported in terms of  $F$  as a function of time in minutes.



(a) Suggest a two-parameter model consistent with the data; the model can consist of ideal reactors, bypass, and dead volume.

(b) Evaluate the model parameters.

(c) **Bonus [3 points]**

Based on your model, evaluate expected conversion if this reactor is used to carry out the liquid-phase second-order reaction  $A + B \rightarrow C$ , where A and B are to be fed in equal molar amounts at a volumetric rate of  $1 \text{ m}^3/\text{min}$ . The entering concentration of A is 2 molar, and the specific reaction rate is  $1.5 \text{ m}^3/(\text{kmol} \cdot \text{min})$ .

① by pass ✗ ideal reactor

②  $\frac{V_b}{V_0} = 0.5$

$V_b = 0.5 \text{ m}^3/\text{min}$  ✓

② Dead Volume

volumetric flowrate inlet  
to reactor =  $0.5 \text{ m}^3/\text{min}$

$$\tau = \frac{V_{SD}}{v}$$

$$2 = \frac{V_{SD}}{v}$$

$$V_{SD} = 1 \text{ m}^3$$

Quiz # 3 (Chapter 10)

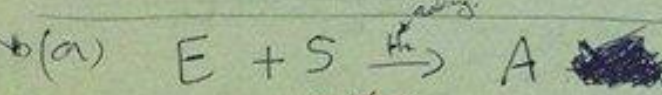
Name: Ali Al-Hmoud

ID # 0136291

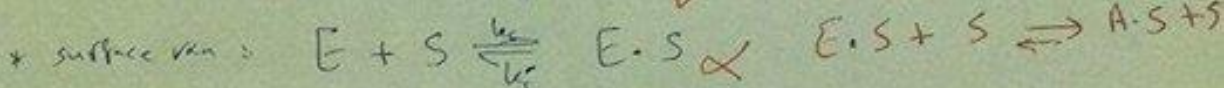
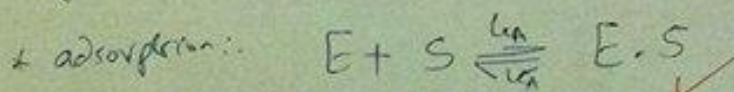
The rate law for the catalytic hydrogenation of ethylene (E) to ethane (A) over a cobalt-molybdenum catalyst is

$$-r_E' = \frac{k P_E P_H}{1 + K_E P_E}$$

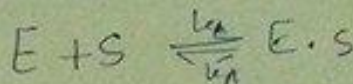
- (a) Write down the reaction stoichiometry.  
(b) Suggest a mechanism and rate-limiting step consistent with the rate law.  
(c) Knowing that  $K_E = 2 \text{ atm}^{-1}$  and  $P_{E0} = 4 \text{ atm}$ , what will be the fraction of vacant sites ( $C_v/C_t$ ) when 40% conversion is achieved?



(b) mechanism:



if adsorption rate limiting



$$-r_E = k_1 P_E C_v - k_{-1} C_{ES}$$

$$-r_E = k_1 (P_E C_v - \frac{C_{ES}}{K_E})$$

$$\delta \frac{r_E}{k_1} = 0 \quad \delta \frac{r_D}{k_{-1}} = 0$$

if surface rxn is rate limiting

$$-r_E = k_2 P_E C_v - k_{-2} C_{ES}$$

$$-r_E = k_2 (P_E C_v - \frac{C_{ES}}{K_E})$$

rate of desorption

$$-r_D = k_3 C_{ES} - k_{-3} P_A C_v$$

$$-r_D = k_3 (C_{ES} - \frac{P_A C_v}{K_D})$$

#### Question 4 [8 points]

The elementary isothermal gas-phase reaction  $A \rightarrow B + C$  is carried out in a moving-bed reactor. The catalyst decays by sintering (i.e. 2<sup>nd</sup> order decay). The moving bed contains 100 kg of catalyst and the catalyst flow rate ( $U_s$ ) through the bed is adjusted so that the exiting catalytic activity is one-fourth of the entering activity.  $\frac{1}{4} \times 0.1$

The specific reaction rate for fresh catalyst is  $0.10 \text{ dm}^3 / (\text{kg-cat} \cdot \text{s})$ . Pure A enters the reactor at a concentration of  $0.005 \text{ mol/dm}^3$  and a constant volumetric flow rate of  $3.75 \text{ dm}^3 / \text{s}$ .

(a) Find the catalyst activity as a function of catalyst weight.  $a(w)$

(b) What will be the exit conversion?

$$\textcircled{a} \quad \frac{-da}{dw} = \frac{k_d}{U_s} a^n$$

$$\frac{-da}{a^n} = \frac{k_d}{U_s} dw$$

$$\int_0^a \frac{-da}{a^2} = \int_0^w \frac{k_d}{U_s} dw$$

$$\frac{1}{a} \Big|_0^a = \frac{k_d}{U_s} w \Big|_0^w$$

$$\boxed{a = \frac{U_s}{k_d w}}$$

$$-r_A = k C_A$$

$$C_A = C_{A0}(1-x)$$

$$-r_A = k C_{A0}(1-x)$$

$$\frac{dx}{dw} = \frac{U_s}{F_{A0}} \times \frac{k C_{A0}(1-x)}{k_d w}$$

$$\int_0^x \frac{dx}{(1-x)} = \int_0^w \frac{U_s \times k C_{A0}}{k_d F_{A0}} \times \frac{1}{w} dw$$

$$\ln \frac{1}{1-x} = \int_0^w \frac{0.25 \times 0.1 \times 0.005}{0.01875} \times \frac{1}{w} dw$$

$$\ln \frac{1}{1-x} = 6.67 \times 10^{-3} \int_0^w \frac{1}{w} dw$$

$$\ln \frac{1}{1-x} = 6.67 \times 10^{-3} \ln w \Big|_0^w$$

$$F_{A0} = C_A U = \frac{0.005 \text{ mol}}{\text{dm}^3} \times \frac{3.75 \text{ dm}^3}{\text{s}} = 0.01875 \frac{\text{mol}}{\text{s}}$$

$$U_s = \frac{1}{4} \times 0.1 = 0.025$$

(0905422) Chem

Name: \_\_\_\_\_

ID # \_\_\_\_\_

P10-  
V9

The University of Jordan  
Faculty of Engineering & Technology  
Chemical Engineering Department  
Section \_\_\_\_\_  
Experiment # 8 (Chapter 10)  
Partner Name: \_\_\_\_\_  
Partner ID # \_\_\_\_\_

Calculations, owing to the  
effect of temperature,  
used to grow  
chem. Soc. -  
for two

The University of Jordan  
School of Engineering  
Chemical Engineering Department

(0905422) Chemical Reaction Engineering II

In-Class Assessment # 10-6

Partner (1) Name: Murad Barham

ID # 0144455

Partner (2) Name: Hamzah bani abdo

ID # 0110553

The elementary gas phase irreversible reaction  $2A \rightarrow 2B$  is carried out isothermally in a moving bed reactor in which there is significant pressure drop. Pure A enters the reactor at a concentration of  $0.1 \text{ mol/dm}^3$  and a flow rate of  $2 \text{ mol/min}$ . The entering pressure is  $10 \text{ atm}$  and the pressure at the exit is  $4.472 \text{ atm}$ . The catalyst decay is by poisoning and of zero order. The catalyst loading rate is  $10 \text{ kg/min}$  and the catalyst bed contains  $40 \text{ kg}$  of catalyst.

Additional information: Specific reaction rate  $k = 20.0 \text{ dm}^6/(\text{mol} \cdot \text{kg cat} \cdot \text{min})$   
Catalyst decay constant  $k_d = 0.25/\text{min}$

For catalyst decay by poisoning:

$$-\frac{da}{dt} = k_d a^n$$

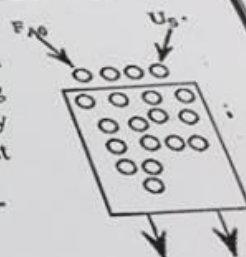
For isothermal gas-phase reaction with  $\varepsilon = 0$ ,

$$y = \frac{P}{P_0} = (1 - \alpha W)^{1/2}$$

For moving-bed reactor:

$$t = \frac{W}{U_s} \quad \frac{dX}{dW} = \frac{a[-r'_A(t=0)]}{F_{A0}}$$

- (a) Show that the pressure drop parameter  $\alpha = 0.02 \text{ kg}^{-1}$ .  
(b) What is the conversion at the exit of the reactor?



1/2

40 / 0.25

(0905422) Chemical Reaction Engineering II

First Semester – 2017/2018

Quiz # 3 (Chapter 10)

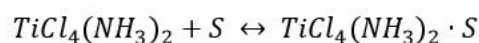
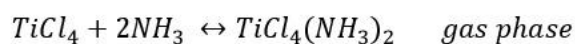
Name: \_\_\_\_\_

ID # \_\_\_\_\_

Titanium nitride (TiN) films are used in decorative coatings as well as in wear-resistant tools. There is increasing interest in TiN because of its thermal stability, good diffusion barrier properties, and its low electrical resistivity. Titanium nitride films were formed by chemical vapor deposition (CVD) from a mixture of  $\text{TiCl}_4$ ,  $\text{NH}_3$ ,  $\text{H}_2$  and Ar. The following observations can be made:

- The rate of deposition is independent of Ar and  $\text{H}_2$
- At low partial pressures of both  $\text{TiCl}_4$  and  $\text{NH}_3$ , the deposition rate appears to be first-order in  $\text{TiCl}_4$  and second-order in  $\text{NH}_3$
- At high partial pressures of  $\text{NH}_3$  the rate varies inversely with  $\text{TiCl}_4$

The following mechanism has been suggested for the reaction:



It is believed that the gas-phase reaction to form the complex  $\text{TiCl}_4(\text{NH}_3)_2$  is in equilibrium.

(a) Determine the rate expression for the suggested mechanism.

(b) Does the rate expression agree with experimental observations? Explain.

(c) What is the observed adsorption method called? \_\_\_\_\_

(d) What type of surface reaction mechanism is suggested? \_\_\_\_\_

(e) What linearization will you do to determine the reaction rate parameters?

(f) Use the data below to determine the reaction rate parameters:

$r_{Dep}(\text{mol TiN}/\text{cm}^2 \cdot \text{min}) \times 10^8$	15	10	6	8.5	16
$P_{NH_3}(\text{mT})$	79	79	79	60	10
$P_{TiCl_4}(\text{mT})$	1	3	10	2.3	2.3

