



ملخصات مدار



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العمليات الموحدة للدقائق الصلبة

Find sphericity

$$\phi_s = \frac{6 V_p}{\pi D_p^3} \rightarrow \text{volume particle}$$

$$\text{area particle} = \frac{\pi D_p^2}{4} \rightarrow \text{diameter eq}$$

$$\frac{\pi D_p^3}{6} = \text{volume particle} \quad (\text{cylinder, cube, cuboid})$$

specific surface
area = $\frac{\text{Area}}{\text{Volume}}$

$$r = \frac{D}{2}$$

Area

$$\text{cylinder} = \pi D \left(\frac{D}{2} + h \right)$$

$$\text{spher} = \pi D^2$$

$$\text{cuboid} = 2 * (\text{width} * \text{height}) + 2 * (\text{width} * \text{length}) + 2 * (\text{height} * \text{length})$$

$$\text{cube} = (\text{length})^3$$

$$\text{circle} = \pi r^2$$

$$\text{Volume cylinder} = \frac{\pi D^2 h}{4}$$

$$\text{Sphere} = \frac{\pi D^3}{6}$$

$$\text{cuboid} = \text{width} * \text{height} * \text{length}$$

$$\text{cube} = (\text{length})^3$$

* Surface diameter (ds)

$$ds = \sqrt{\frac{6 V_p}{\pi}} \rightarrow \text{area particle}$$

* Volume diameter

$$dv = \sqrt[3]{\frac{6 V_p}{\pi}} \rightarrow \text{volume particle}$$

* Surface Volume diameter

$$ds_v = dv^3 / ds^2$$

degree mixing (quality)

$$s_r^2 = p(1-p) / n$$

initial proportion of on particle
equal to mass fraction
0.5

number of particles of sample

→ Completely random mix

$$b = 1$$

$$s = s_r$$

$$s_0^2 = p(1-p) \rightarrow \text{unmixed } b = 0$$

degree of mixing

$$b = \frac{s_0 - s}{s_0 - s_r} \text{ OR } s_r / s$$

$$b = \frac{s_0^2 - s^2}{s_0^2 - s_r^2}$$

For unmixed
 $I = \frac{1}{\sqrt{n}}$

ball mill $r = \frac{D}{2}$

$$\text{Hz} \times 2\pi = \text{rad/s}$$

$$W_c = \sqrt{\frac{g}{r}} \quad \text{critical velocity}$$

$$r = r_{\text{ball}} - r_{\text{particle}} \approx r_{\text{ball}}$$

radius

$$\text{actual speed} = (0.5 - 0.75) W_c$$

~~W_{ball}~~ $W_{\text{ball}} > W_{\text{critical}}$
 the speed rotation is too high
 and the ball is contact with the
 side of mill

Crushing Roll angle of nip = 2α

$$\cos \alpha = \frac{r_1 + b}{r_1 + r_2}$$

Roll particle

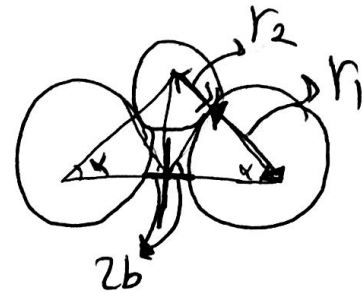
$$\text{Area} = 2b \times \text{roll}$$

$$\text{Volumetric} = \text{Area} \times \text{Velocity}$$

$$\text{actual} = \text{Volumetric} \times \text{actual}$$

$$\text{mass} = \text{density} \times \text{Volume}$$

particle



* power consumption (crushing)

$$\textcircled{1} \text{Rittinger's law (fine)} \quad E = k_R P_c \left(\frac{1}{L_2} - \frac{1}{L_1} \right)$$

$\frac{\text{m}^3}{\text{kg}}$

$L \rightarrow \text{size}$
 M_m

$$\textcircled{2} \text{Hick's law (coarse)} \quad E = k_H P_c \ln \frac{L_1}{L_2}$$

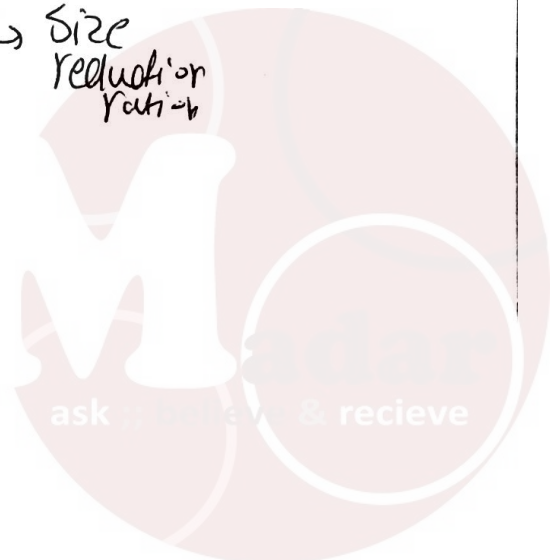
$\frac{\text{m}^3}{\text{kg}}$ size reduction ratio

$\textcircled{3}$ Bond's law (intermediate)

$$E = E_i \sqrt{\frac{100}{L_2}} \left[1 - \frac{1}{q^{1/2}} \right]$$

$$W = 10 W_i \left[\frac{1}{L_2^{1/2}} - \frac{1}{L_1^{1/2}} \right]$$

k_w, k_{ton} size $\rightarrow M_m$



Superficial velocity
↑

CH 7

packed bed
[Voidage, pressure drop]

$$Re = \frac{U \rho}{\mu S (1-e)}$$

Fluid
specific
superficial velocity

$Re < 1$ laminar
 $Re > 100$ turbulent



$$c'_p = \frac{5}{Re} + \frac{0.4}{Re^{0.1}}$$

$Re < 1$ (laminar) $c'_p = \frac{5}{Re}$

$1 < Re < 100$ (transit) $c'_p = \frac{5}{Re} + \frac{0.4}{Re^{0.1}}$

$Re > 100$ (turbulent) $c'_p = \frac{0.4}{Re^{0.1}}$

$c'_p = \checkmark$

$$c'_p = \frac{e^{3*} (-\Delta p)_{dry}}{S(1-e) * \frac{1}{4} * \rho U^2}$$

Fluid
superficial velocity

$$G = \frac{U \rho}{\text{kg/m}^2 \cdot \text{s}}$$

Flow rate flux

$$\rho_{H_2O} = 1000 \text{ kg/m}^3$$

$$S_B = S (1-e)$$

$$S_{\text{spherical}} = 6/d$$

cylinder $d=h$ $S = 6/d$

$e \rightarrow$ percent of voidage
 $(1-e)$ percent of solid

ask & recieve

non spherical particle plates

$$Cp' Re^2 = \frac{4K \rho dp^3 g}{M^2 \pi} (\rho - \rho_f) \quad \text{Free of } U$$

$$\frac{Cp'}{Re} = \frac{4K M g}{\pi \rho_f^2 U_0^3} (\rho - \rho_f) \quad \text{Free of particle size}$$

$$K = ??$$

$$\frac{\pi}{4} d^2 = \text{Area particle}$$

$$\text{Area} \times \rho_f = K dp^3$$

$$K = \checkmark$$

Find terminal Velocity \rightarrow settling

$Cp' / Re^2 \rightarrow \log \rightarrow$ table 3.4 $\rightarrow \log Re \rightarrow$ correction $\neq \log Re$
 $Re = \frac{U d \rho}{\mu}$ \rightarrow particle fluid \rightarrow 3.7 table $\rightarrow Re$

Find particle size

$\frac{Cp'}{Re} \rightarrow \log \rightarrow$ table $\rightarrow \log Re \rightarrow$ table

mm ²	$\rightarrow 10^{-6} m^2$
cm ²	$\rightarrow 10^{-4} m^2$
mm ³	$\rightarrow 10^{-9} m^3$
mN	$\rightarrow 10^{-3} N$

Fluidization

How to ~~calculate~~ calculate U_{mf} ?

$e = 0.4$ [spherical particle] glass

1- Stokes' law

$$U_{mf} = \frac{0.00059 d^2 (\rho_s - \rho) g}{\mu}$$

$$Re_{mf} = \frac{U_{mf} d \rho}{\mu}$$

$$Re_1 < 1 \Rightarrow \text{done}$$

$$Re_1 > 1$$

$$Ga = \frac{d^3 \rho (\overset{\text{solid, particle}}{\rho_s} - \underset{\text{fluid}}{\rho}) g}{\mu^2}$$

$$Re_{mf} = 25.7 (\sqrt{1 + 5.53 \times 10^{-5} Ga} - 1)$$

$$Re_{mf} = \frac{U d \rho}{\mu}$$

$$U = \checkmark$$

at min. ρ

$$\Delta p = L(1-e)(\rho_s - \rho)g$$

$$U_{mf} = \frac{0.0055 e^3 d^2 (\rho_s - \rho) g}{(1-e) \mu}$$

$$m_s = (1-e) A L \rho_s$$

non spherical particle (plates)

$$U = \frac{1}{K''} \frac{e^3}{S^2 (1-e)^2} \frac{1}{\mu} \frac{-\Delta p}{L} \quad (\text{Carmen})$$

$$U_{mf} = \frac{1}{5} \frac{e^3 (\rho_s - \rho) g}{S^2 (1-e) \mu}$$

$$Re_{mf} = \frac{U_{mf} d \rho}{\mu} \begin{matrix} > 1 \times \\ < 1 \checkmark \end{matrix}$$

$$Re_1 > 1$$

$$Ga = \frac{d^3 \rho g (\rho_s - \rho)}{\mu^2}$$

$$dp = \sqrt[3]{\frac{6 \mu U}{\pi}}$$

$$Re_{mf} = 33.65 (\sqrt{1 + 6.18 \times 10^{-5} Ga} - 1)$$

$$U_{mf} = \frac{\mu}{dp \rho} Re_{mf}$$

$$\frac{Re_o}{Re_{mf}} = \frac{U_o}{U_{mf}}$$

$U_o \Rightarrow$ spherical particle

$$Re_o = (2.33 Ga^{0.018} - 1.53 Ga^{-0.016})^{13.3}$$

$$Re_o = \frac{U_o d \rho}{\mu}$$

What is the voidage (extent of expansion) (e)

$$\frac{1}{Ga} = \frac{d^3 \rho (\rho_s - \rho) g}{\mu^2}$$

$$Re_o \checkmark$$

$$U_o \checkmark$$

$$U_{mf}$$

ignore the wall effect

$$\frac{U_o - U_{mf}}{U_o} = 0.043 Ga^{0.57} [1 - 1.24 d/d_t]$$

$$n = \checkmark$$

$$\frac{U_{mf}}{U_o} = e^n \Rightarrow e = \checkmark$$

$$= 2.51 \log \left(\frac{(1.83 Ga^{0.018} - 1.2 Ga^{-0.016})^{13.3}}{\sqrt{1 + 5.53 \times 10^{-5} Ga} - 1} \right)$$



gas cyclone

$$U_0 = \frac{d^2 g \rho_s}{18 M} \dots \rightarrow \text{diameter particle}$$

\Downarrow sub in previous

$$U_0 = \frac{U_r}{U_t^2} r g \dots \text{(gravitational field)} \\ \text{cyclon}$$

$$U_0 = \frac{U_r}{U_t^2} 0.2 d_0 g$$

$$U_r = \frac{G}{\underbrace{2\pi r Z \rho}_{\text{surface area}}} \rightarrow \text{mass velocity}$$

$$U_t = U_{t0} \sqrt{\frac{dt}{2r}}$$

maximum
at the well (velocity of the gas enter)

$$U_0 = \frac{0.2 G d_0 g}{\pi Z dt U_{t0}^2}$$

$$U_0 = \frac{0.2 A_i^2 d_0 \rho_g}{\pi Z dt G} \rightarrow \text{gas inlet}$$

find d cyclon

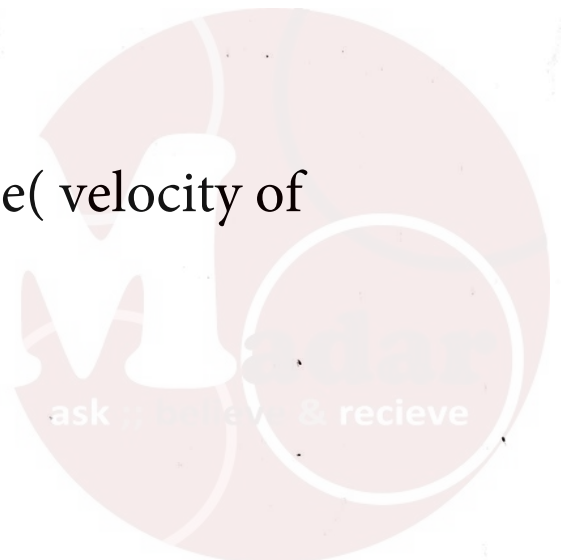
$\rho(\text{gas})$

$$G = A_i \rho U_{t0} \quad (\text{kg/m.s}^2) \\ \downarrow \\ \text{area gas inlet}$$

uto: tangential velocity at circumference(velocity of the gas which enters the cyclone)

ut: tangential velocity at radius r

dt: diameter of cyclone



Flooding rates
in packed column

packed column

$$F = \frac{SB}{e^3}$$

① dry Towers

$DP_{\text{air Bed}}$

② wet towers $L=0$

$$- DP_w = (1 + k/dn) DP_d$$

broken 5.5
Rashig ring 3.3
size solid

③ irrigated

$$DP = (1 + kL/dn) DP_d$$

Flooding rate (velocity) (in packed column)

$$\frac{L}{G} \sqrt{\frac{\rho_g}{\rho_L}}$$

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$\rho_g \rightarrow$ estimate
ideal gas
law

$$\sqrt{\frac{U_G^2 SB}{ge^3} \left(\frac{\rho_g}{\rho_L}\right) \left(\frac{M_L}{M_w}\right)^{0.2}} = \text{correction factor}$$

$\rightarrow 1 \rightarrow$ water

$SB \rightarrow$ (Table \rightarrow design)

$e \rightarrow$ Rashig rings \rightarrow

$$U_G = \checkmark$$

$$\text{mass velocity} = U_G * \rho_g$$

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$$\frac{dv}{dt} = \frac{(-\Delta P) A^2}{r_M v}$$

[Filtration]

Constant rate

$$\frac{V}{t} = \frac{A^2 (-\Delta P)}{r_M v}$$

Constant pressure

$$\frac{V^2}{2} = \frac{-\Delta P A^2 t}{r_M v} \rightarrow \text{constant pressure}$$

ΔP increases at certain limits $t_1 \rightarrow$ Filtrate V_1

$$\frac{1}{2} (V^2 - V_1^2) = \frac{-\Delta P A^2}{r_M v} (t - t_1)$$

Volume of Filtrate of const. P (under V)
 Volume of Filtrate (i) (under V_1)
 Total (under t)
 Time of const p (under $t - t_1$)

Flow through Cloth

Constant rate

$$V_1^2 + \frac{L A}{v} V_1 = \frac{A^2 (-\Delta P) t_1}{r_M v}$$

Constant pressure

$$\frac{1}{2} (V^2 - V_1^2) + \frac{L A}{v} (V - V_1) = \frac{A^2 (-\Delta P) (t - t_1)}{r_M v}$$

washing rate = $\frac{1}{u}$ rate Filtration

$A = 12 \times 2 \times (A^2)$
 ↑ Fram
 ↓ Fram

Time of washing
OR Volume of washing
 $\left(\frac{dV}{dt}\right)_{\text{filtrate}}$

constant pressure $\left(\frac{1}{t}\right)s$
 $(t-t_1)$

