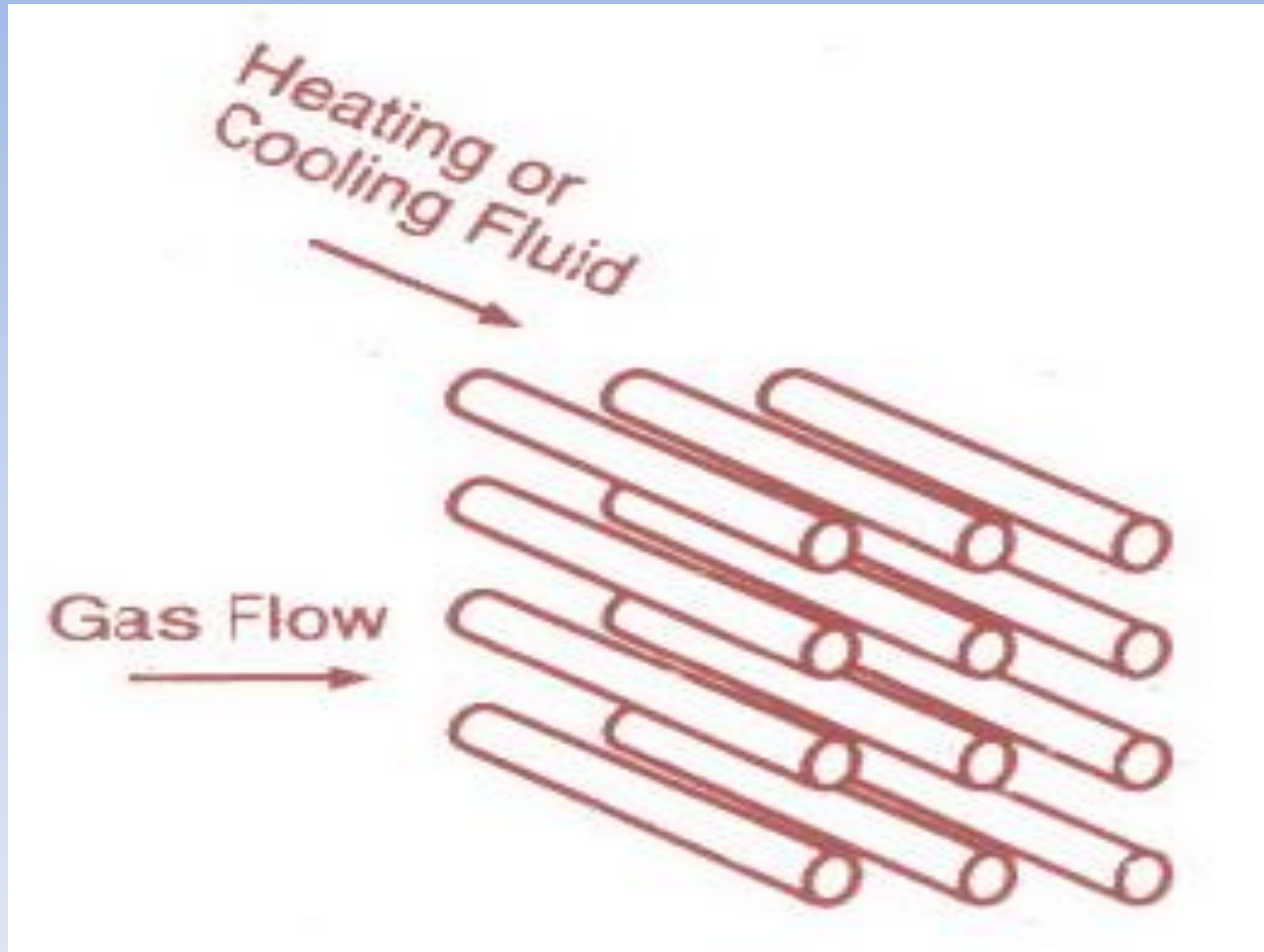
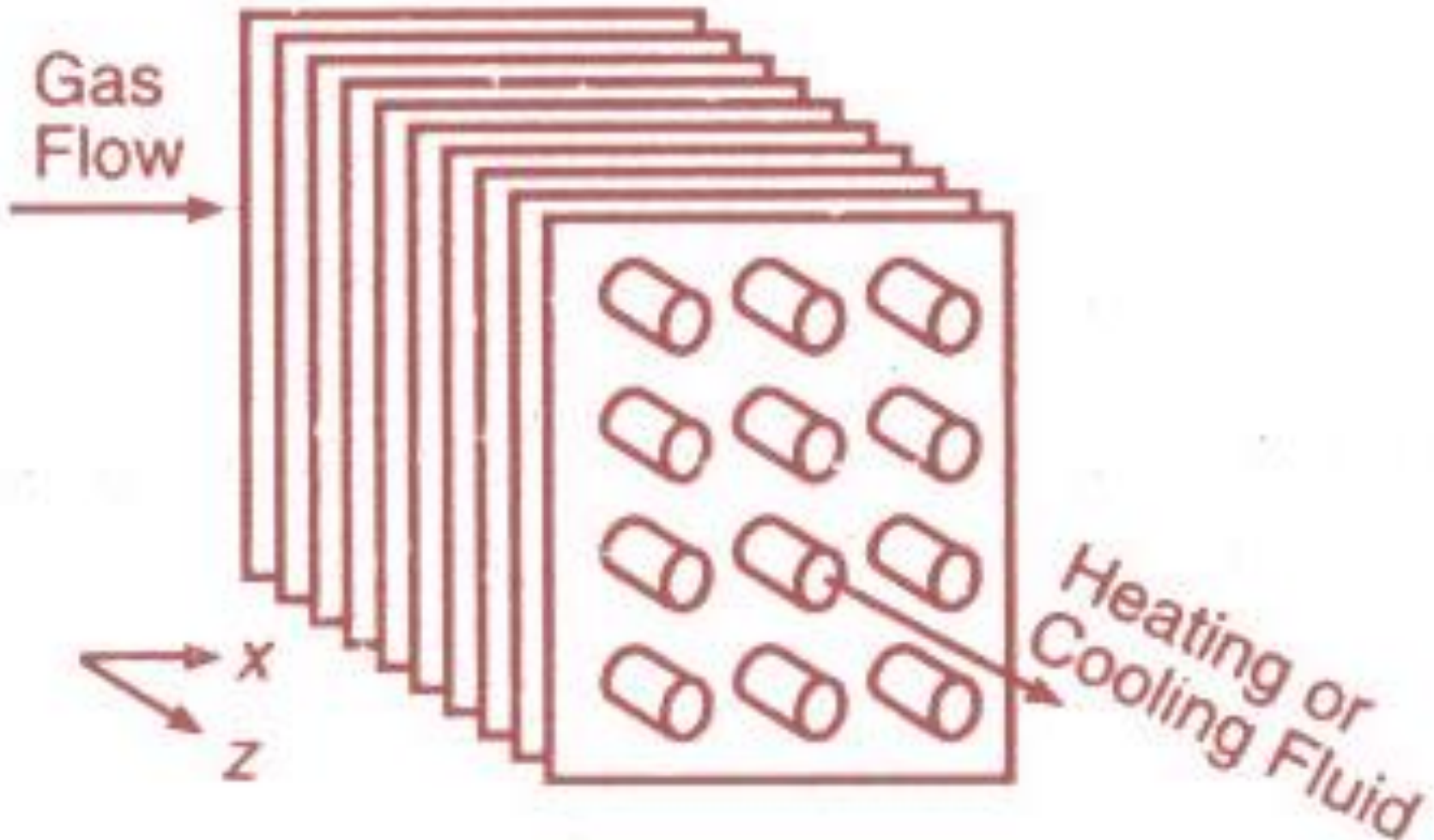


Cross Flow Exchanger and Exchanger Effectiveness

Cross flow mixed-unmixed flow



Cross flow exchanger both fluids unmixed



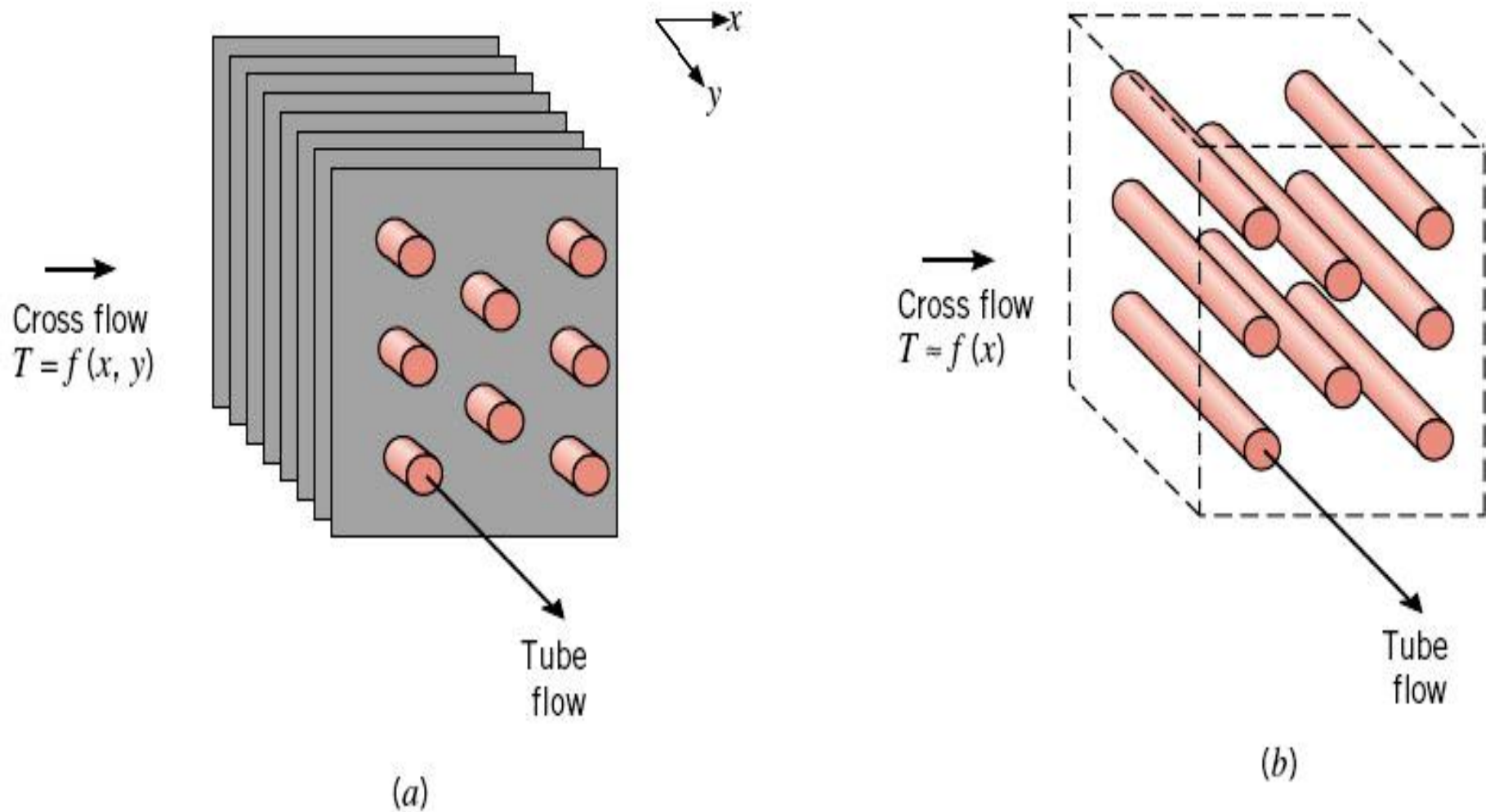
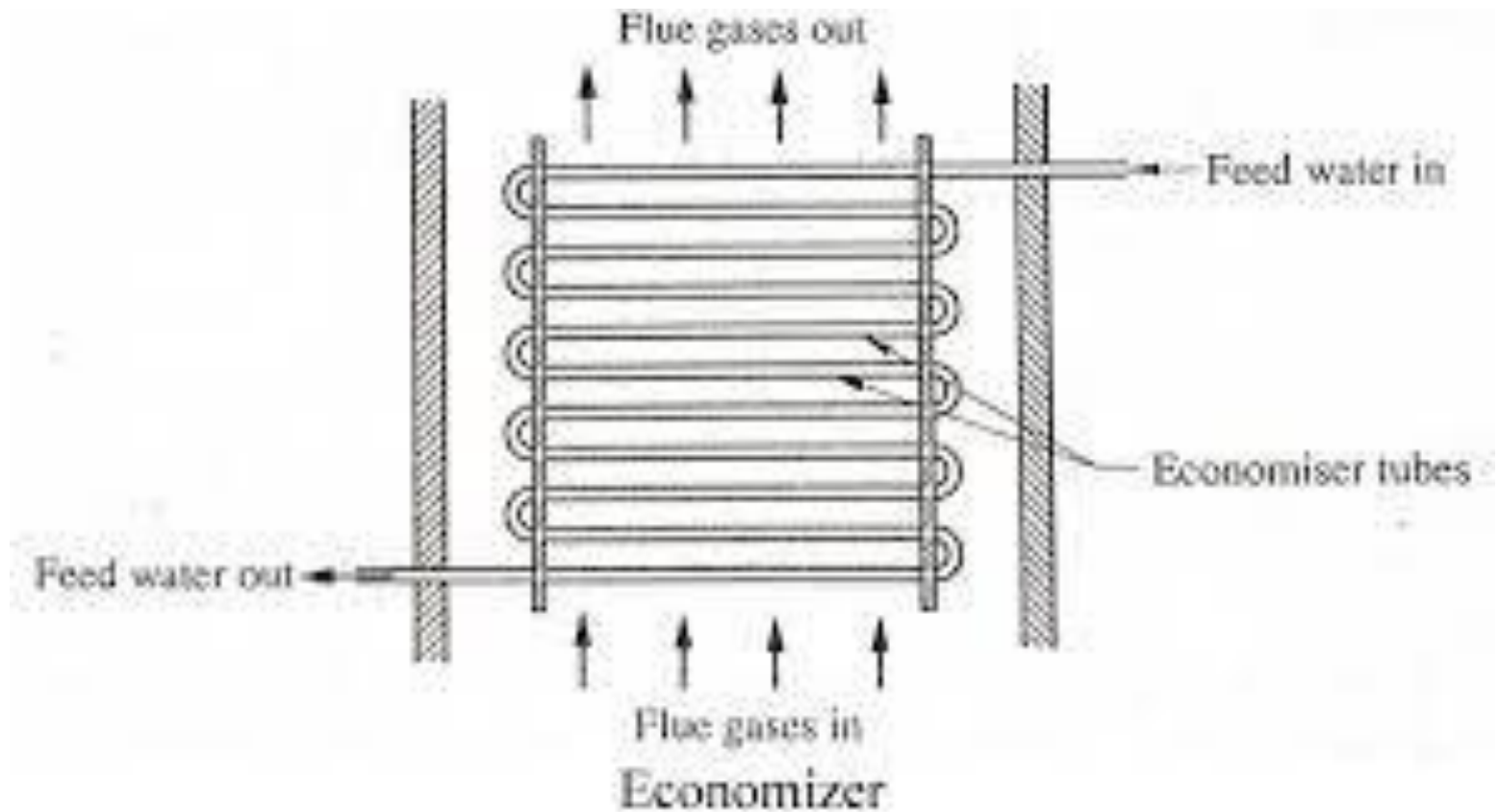
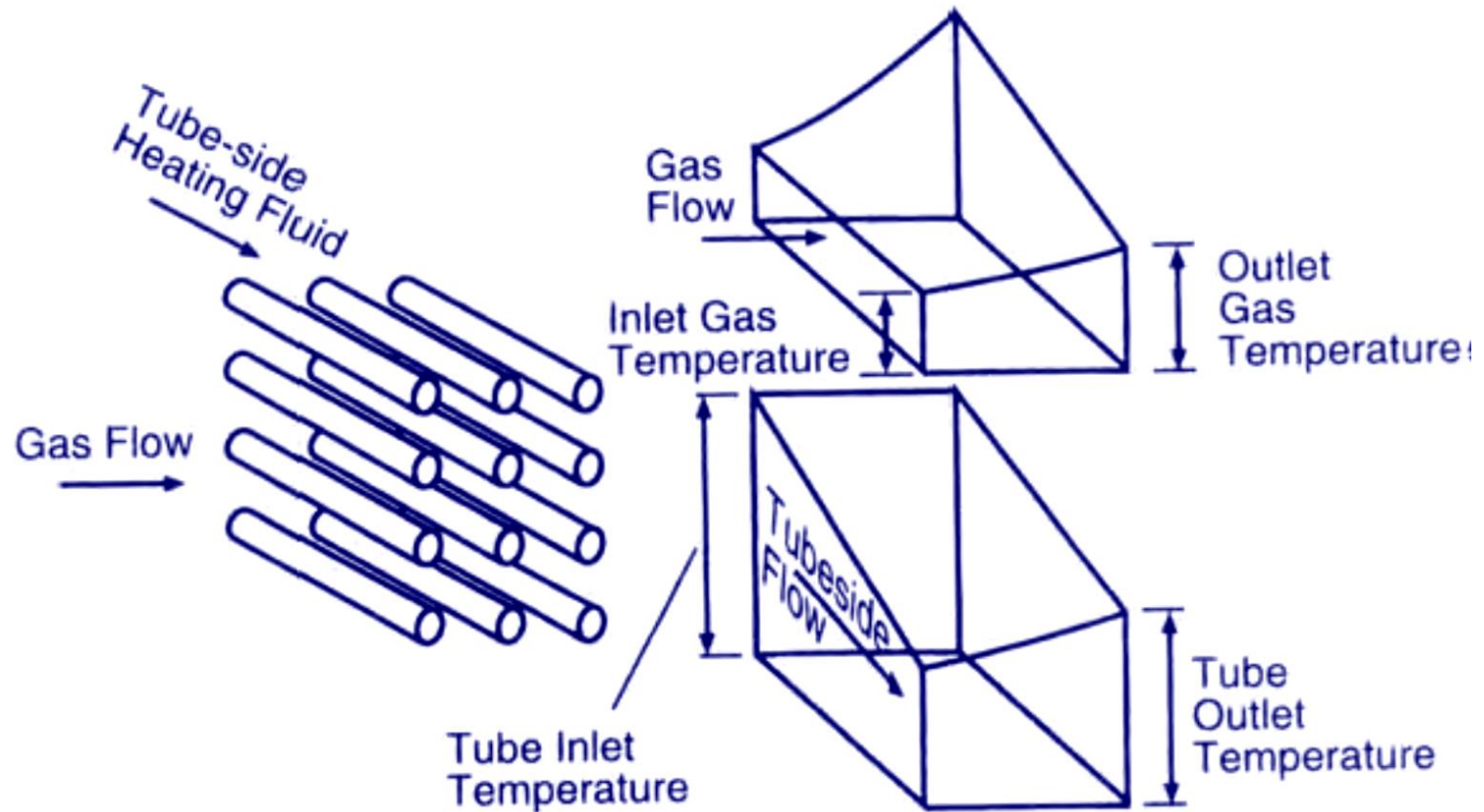


FIGURE 11.2 Cross-flow heat exchangers. (a) Finned with both fluids unmixed. (b) Unfinned with one fluid mixed and the other unmixed.

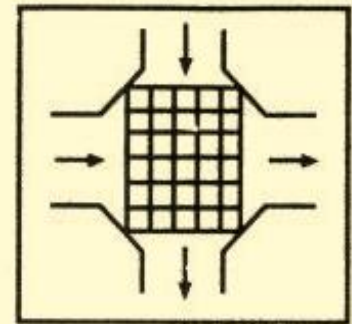
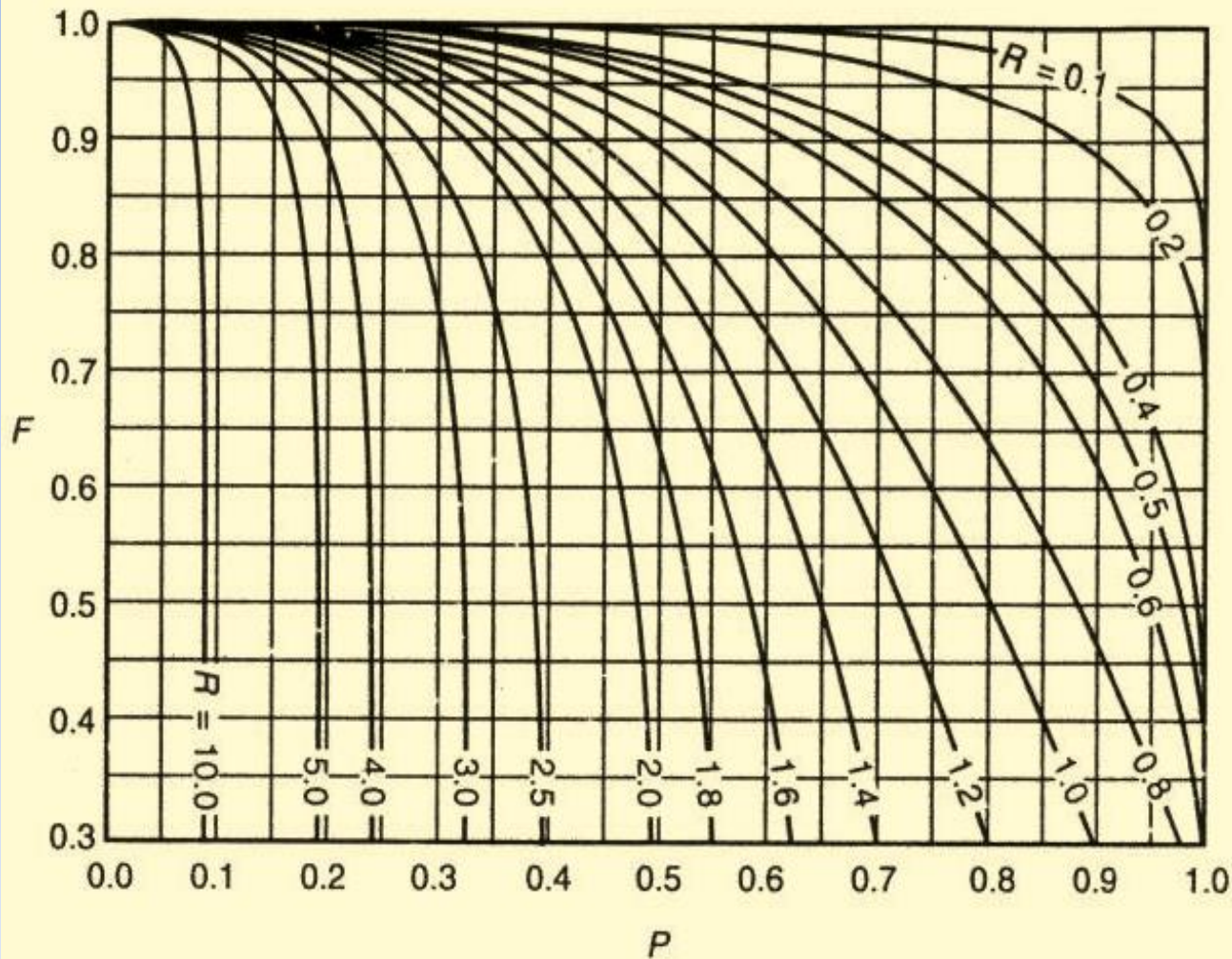
Applications _ Economizer



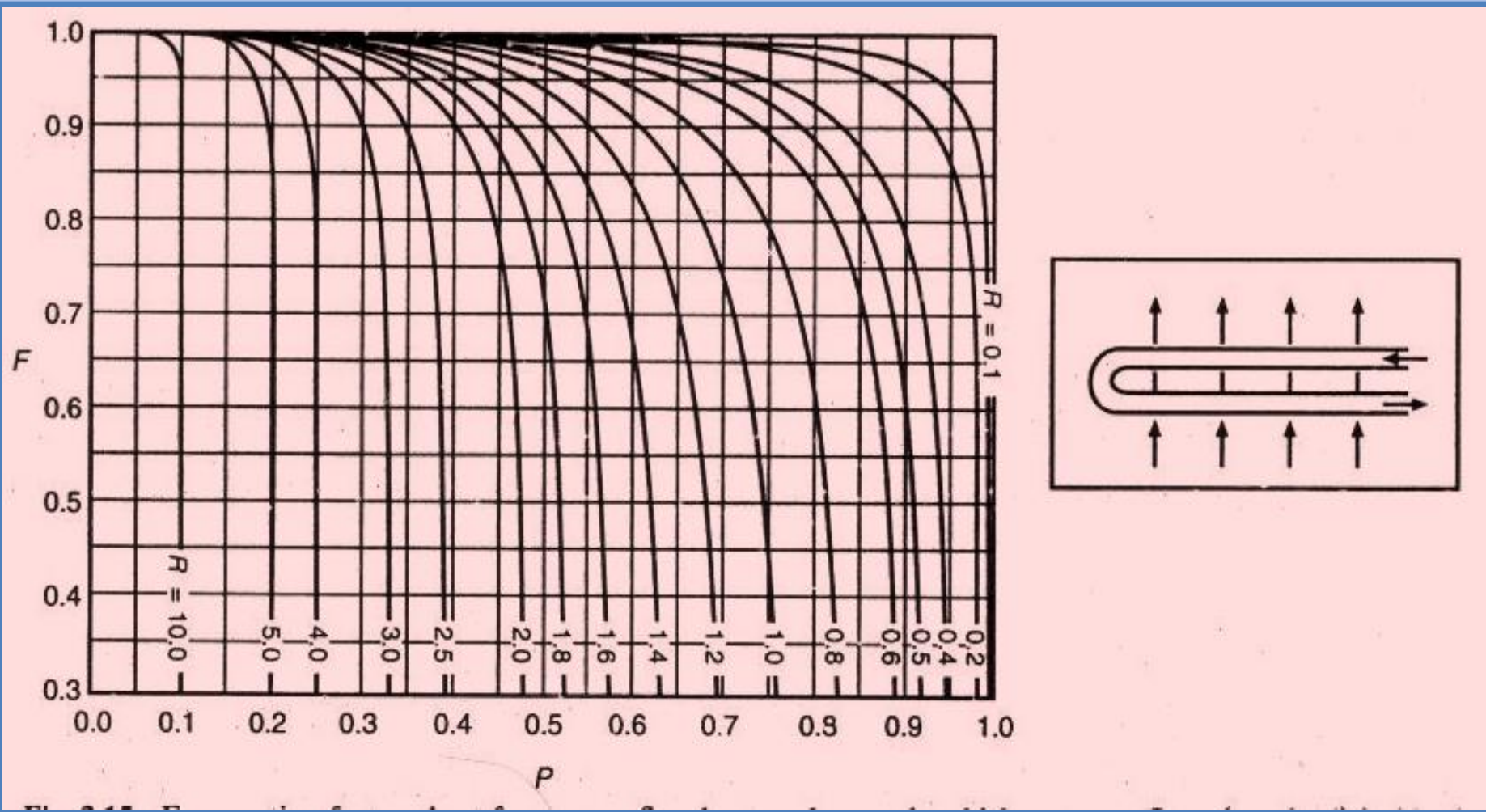
Temperature profiles in a cross-flow heat exchanger



Cross flow exchanger with both streams unmixed



Cross flow 'mixed-unmixed streams'



Heat Exchanger analysis: The effectiveness-NTU Method

- This method is preferable when only inlet temperatures are known.
- Max. Possible heat transfer rate, q_{\max} can be achieved in case of counter current flow exchanger of infinite length. But infinite length is !!!
- If $C_c < C_h$, $C_c \Delta T_c = C_h \Delta T_h \therefore \Delta T_c > \Delta T_h$
- The cold fluid would be heated to inlet temperature of the hot fluid. Hence

$$q_{\max} = C_c (T_{h,i} - T_{c,i})$$

- If $C_h < C_c$, $C_c \Delta T_c = C_h \Delta T_h \therefore \Delta T_h > \Delta T_c$
- The hot fluid would be cooled to the inlet temperature of the cold fluid. Hence

$$q_{\max} = C_h (T_{h,i} - T_{c,i})$$

- In general, $q_{\max} = C_{\min} (T_{h,i} - T_{c,i})$
 where C_{\min} is equal to C_h or C_c whichever is smaller.
- Effectiveness, ε , is defined as the ratio of the actual heat transfer for exchanger to the maximum possible heat transfer rate:

$$\varepsilon = q_{\text{act}} / q_{\max}$$

$$\varepsilon = C_h (T_{h,i} - T_{h,o}) / C_{\min} (T_{h,i} - T_{c,i})$$

or

$$\varepsilon = C_c (T_{c,o} - T_{c,i}) / C_{\min} (T_{h,i} - T_{c,i})$$

- Assume a parallel-flow for which $C_{\min} = C_h$, hence

$$\varepsilon = (T_{h,i} - T_{h,o}) / (T_{h,i} - T_{c,i})$$
- If ε , $T_{h,i}$, and $T_{c,i}$ are known, the actual heat transfer:

$$q_{\text{act}} = \varepsilon q_{\text{max}}$$

$$q_{\text{act}} = \varepsilon C_{\min} (T_{h,i} - T_{c,i})$$

- For any exchanger it can be shown that

$$\varepsilon = f(\text{NTU}, C_{\min}/C_{\max})$$

Where C_{\min}/C_{\max} is equal to C_c/C_h or C_h/C_c , depending on the relative values of heat capacity rates.

- The number of transfer unit, NTU, is defined as

$$\text{NTU} = UA/C_{\min}$$

- ε and NTU can be obtained from equations or charts.

TABLE 11.3 Heat Exchanger Effectiveness Relations [5]

Flow Arrangement	Relation	
Concentric tube		
Parallel flow	$\varepsilon = \frac{1 - \exp [-NTU(1 + C_r)]}{1 + C_r}$	(11.28a)
Counterflow	$\varepsilon = \frac{1 - \exp [-NTU(1 - C_r)]}{1 - C_r \exp [-NTU(1 - C_r)]} \quad (C_r < 1)$	Where $C_r = C_{\min} / C_{\max}$
	$\varepsilon = \frac{NTU}{1 + NTU} \quad (C_r = 1)$	
Shell-and-tube		
One shell pass (2, 4, . . . tube passes)	$\varepsilon_1 = 2 \left\{ 1 + C_r + (1 + C_r^2)^{1/2} \times \frac{1 + \exp [-(NTU)_1(1 + C_r^2)^{1/2}]}{1 - \exp [-(NTU)_1(1 + C_r^2)^{1/2}]} \right\}^{-1}$	(11.30a)
n Shell passes ($2n, 4n, . . .$ tube passes)	$\varepsilon = \left[\left(\frac{1 - \varepsilon_1 C_r}{1 - \varepsilon_1} \right)^n - 1 \right] \left[\left(\frac{1 - \varepsilon_1 C_r}{1 - \varepsilon_1} \right)^n - C_r \right]^{-1}$	(11.31a)
Cross-flow (single pass)		
Both fluids unmixed	$\varepsilon = 1 - \exp \left[\left(\frac{1}{C_r} \right) (NTU)^{0.22} \{ \exp [-C_r(NTU)^{0.78}] - 1 \} \right]$	(11.32)
C_{\max} (mixed), C_{\min} (unmixed)	$\varepsilon = \left(\frac{1}{C_r} \right) (1 - \exp \{ -C_r[1 - \exp (-NTU)] \})$	(11.33a)
C_{\min} (mixed), C_{\max} (unmixed)	$\varepsilon = 1 - \exp (-C_r^{-1} \{ 1 - \exp [-C_r(NTU)] \})$	(11.34a)
All exchangers ($C_r = 0$)	$\varepsilon = 1 - \exp (-NTU)$	(11.35a)

TABLE 11.4 Heat Exchanger NTU Relations

Flow Arrangement	Relation
Concentric tube	
Parallel flow	$NTU = -\frac{\ln [1 - \varepsilon(1 + C_r)]}{1 + C_r} \quad (11.28b)$
Counterflow	$NTU = \frac{1}{C_r - 1} \ln \left(\frac{\varepsilon - 1}{\varepsilon C_r - 1} \right) \quad (C_r < 1)$
	$NTU = \frac{\varepsilon}{1 - \varepsilon} \quad (C_r = 1) \quad (11.29b)$
Shell-and-tube	
One shell pass (2, 4, . . . tube passes)	$(NTU)_1 = - (1 + C_r^2)^{-1/2} \ln \left(\frac{E - 1}{E + 1} \right) \quad (11.30b)$
	$E = \frac{2/\varepsilon_1 - (1 + C_r)}{(1 + C_r^2)^{1/2}} \quad (11.30c)$
n Shell passes ($2n, 4n, . . .$ tube passes)	Use Equations 11.30b and 11.30c with
	$\varepsilon_1 = \frac{F - 1}{F - C_r} \quad F = \left(\frac{\varepsilon C_r - 1}{\varepsilon - 1} \right)^{1/n} \quad NTU = n(NTU)_1 \quad (11.31b, c, d)$
Cross-flow (single pass)	
C_{\max} (mixed), C_{\min} (unmixed)	$NTU = -\ln \left[1 + \left(\frac{1}{C_r} \right) \ln(1 - \varepsilon C_r) \right] \quad (11.33b)$
C_{\min} (mixed), C_{\max} (unmixed)	$NTU = -\left(\frac{1}{C_r} \right) \ln [C_r \ln(1 - \varepsilon) + 1] \quad (11.34b)$
All exchangers ($C_r = 0$)	$NTU = -\ln(1 - \varepsilon) \quad (11.35b)$

Where $C_r = C_{\min} / C_{\max}$

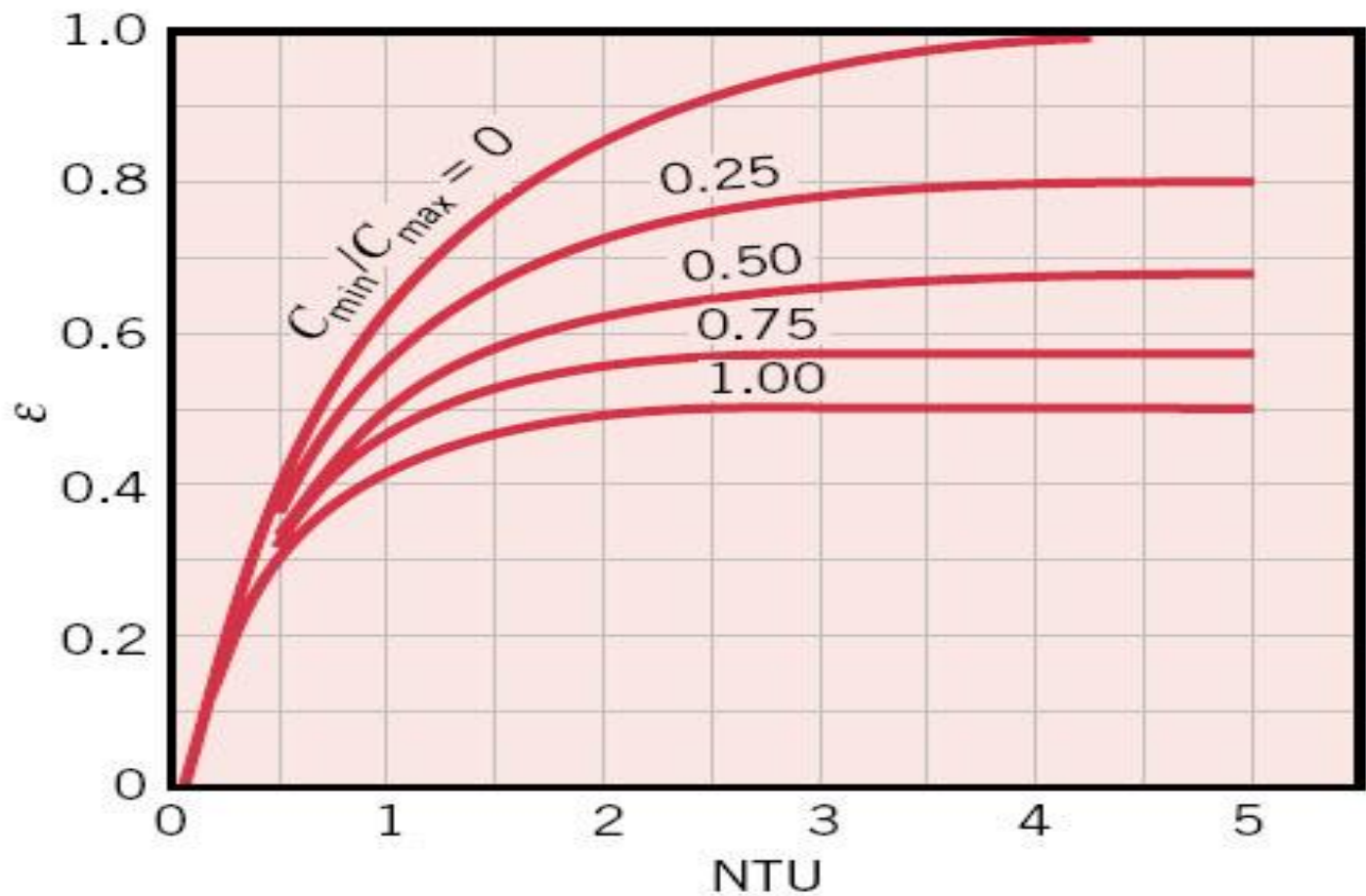


FIGURE 11.10 Effectiveness of a parallel-flow heat exchanger (Equation 11.28).

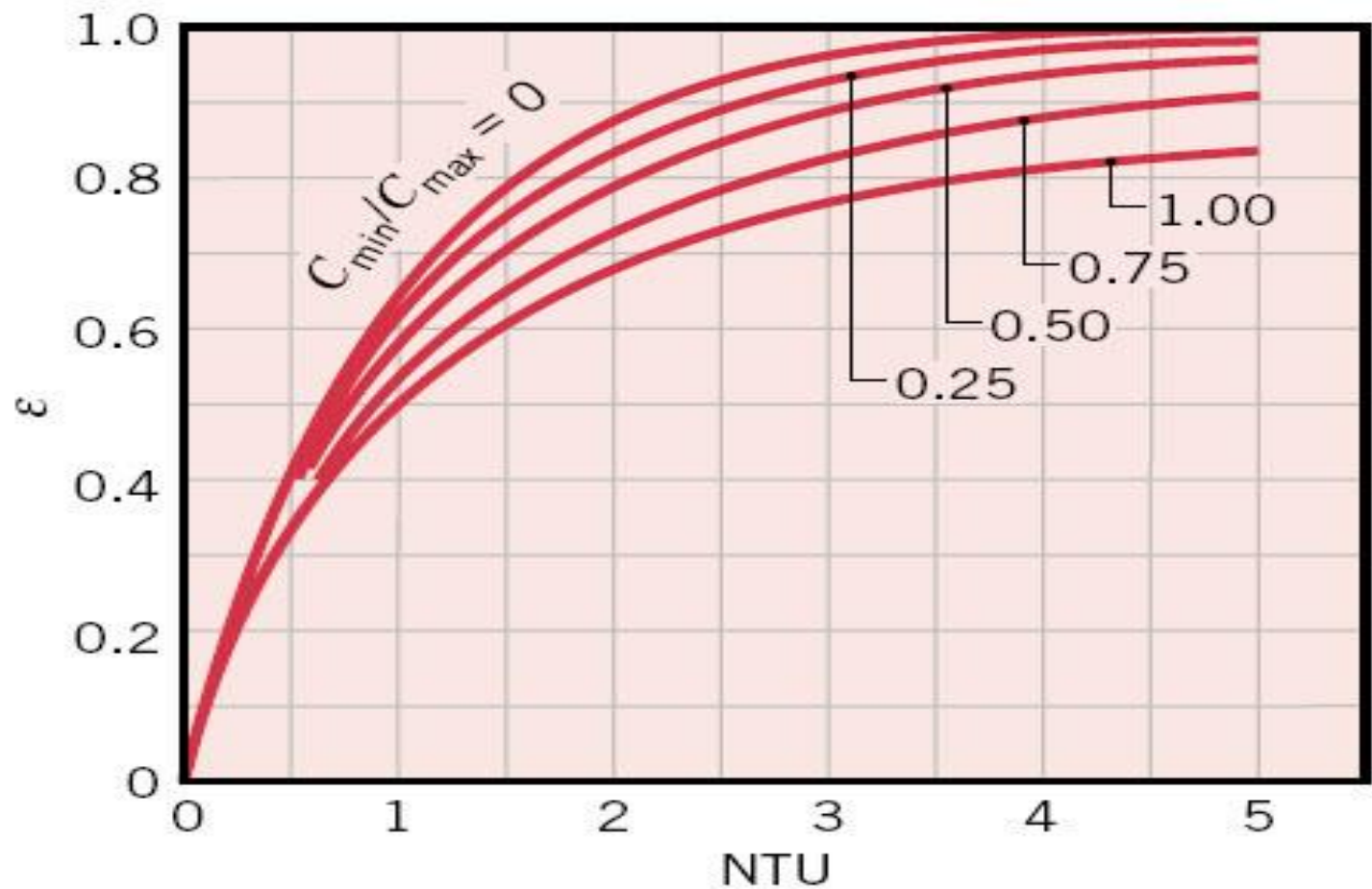


FIGURE 11.11 Effectiveness of a counterflow heat exchanger (Equation 11.29).

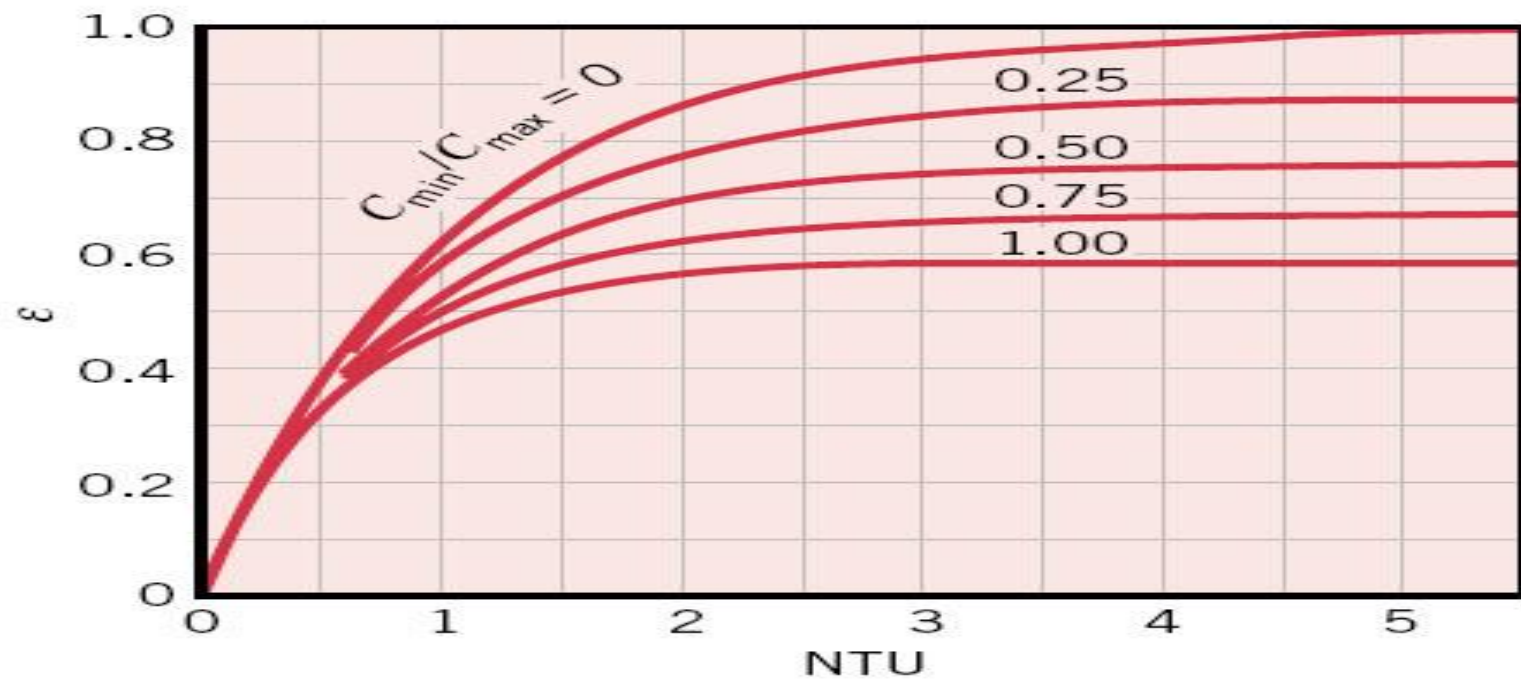
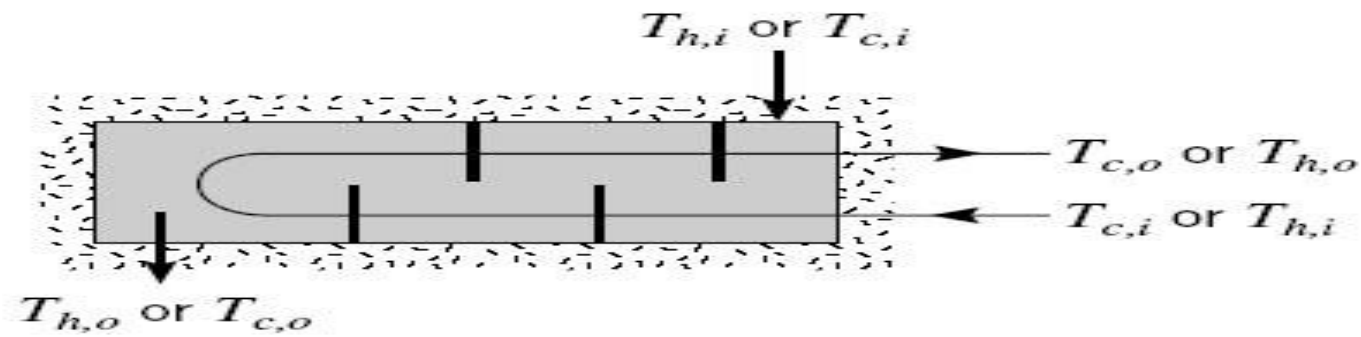


FIGURE 11.12 Effectiveness of a shell-and-tube heat exchanger with one shell and any multiple of two tube passes (two, four, etc. tube passes) (Equation 11.30).

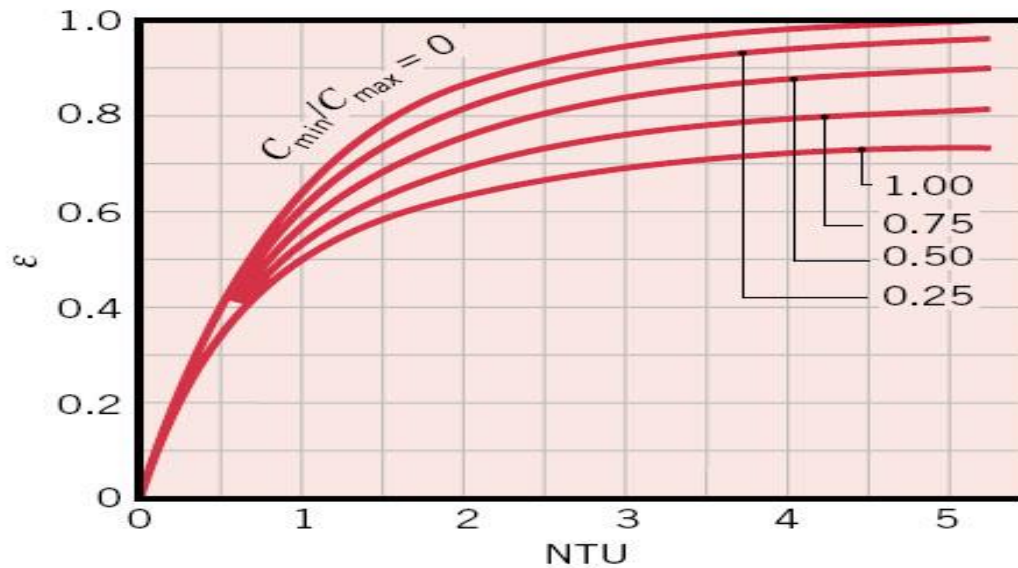
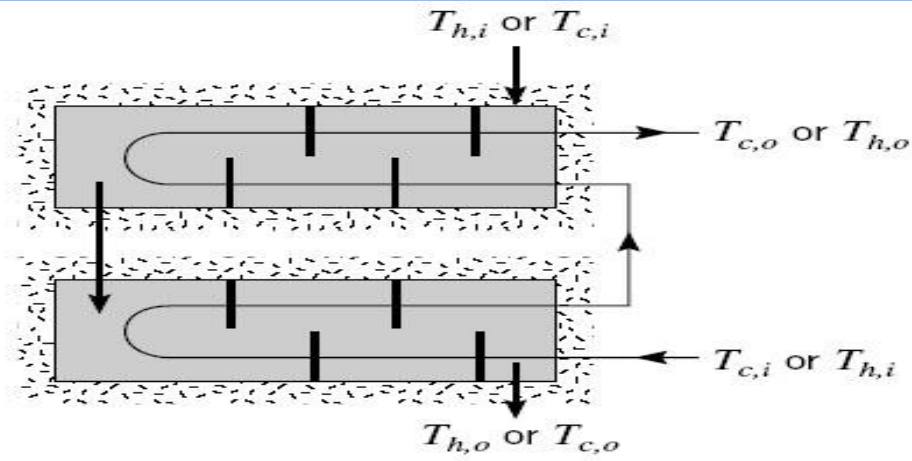
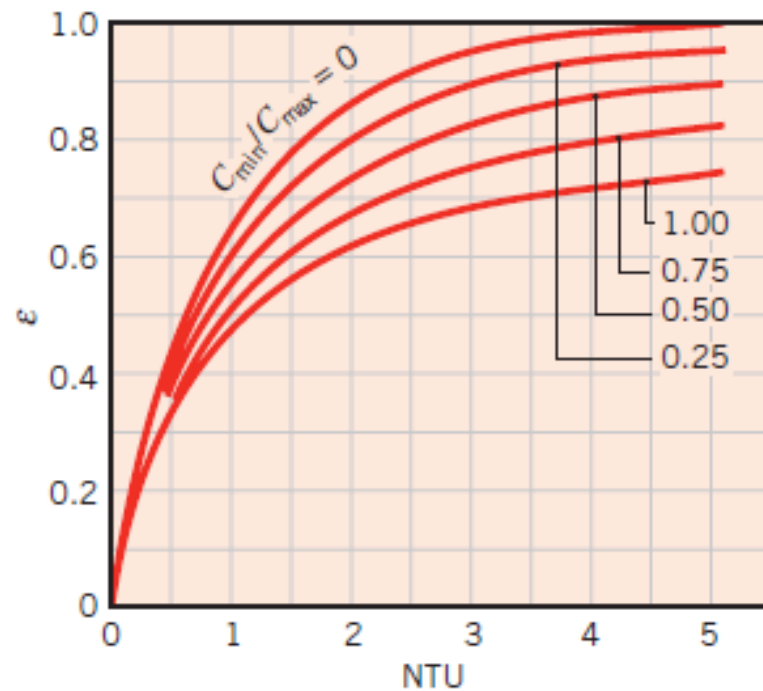
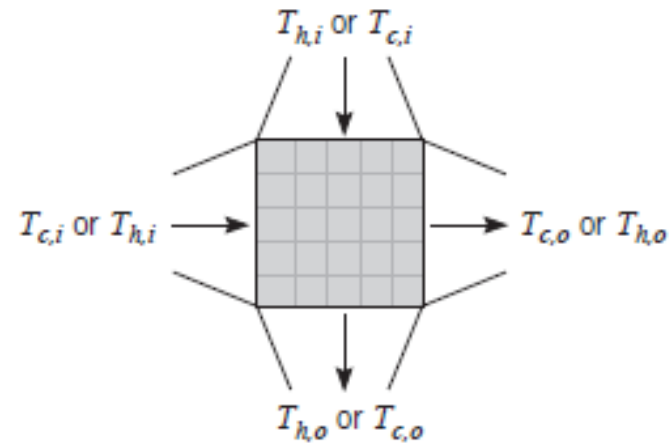
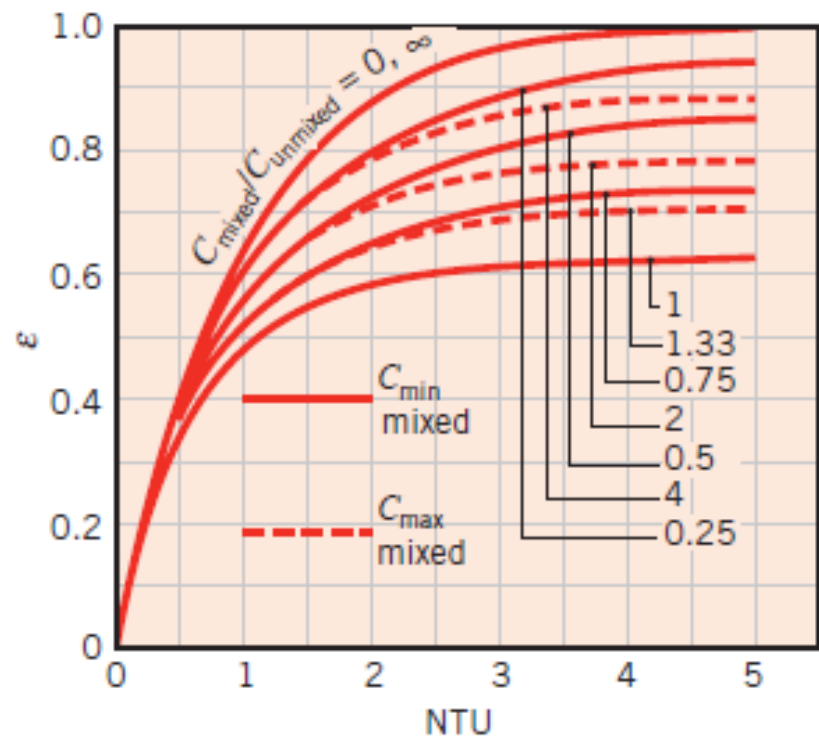
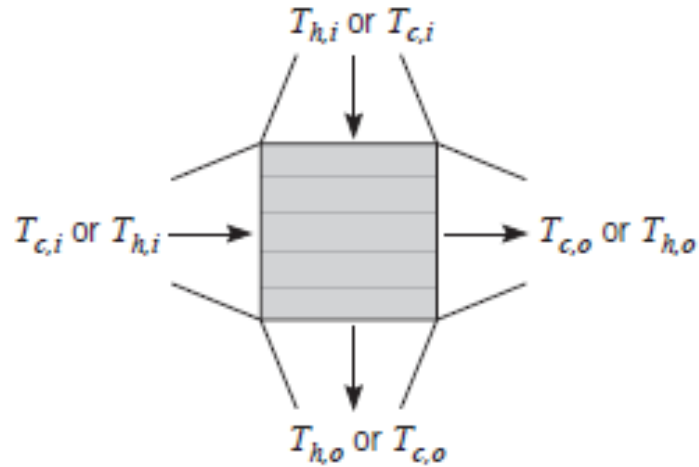


FIGURE 11.13 Effectiveness of a shell-and-tube heat exchanger with two shell passes and any multiple of four tube passes (four, eight, etc. tube passes) (Equation 11.31 with $n = 2$).

Effectiveness of a single pass, cross-flow heat exchanger with both fluids unmixed (Equation 11.32).



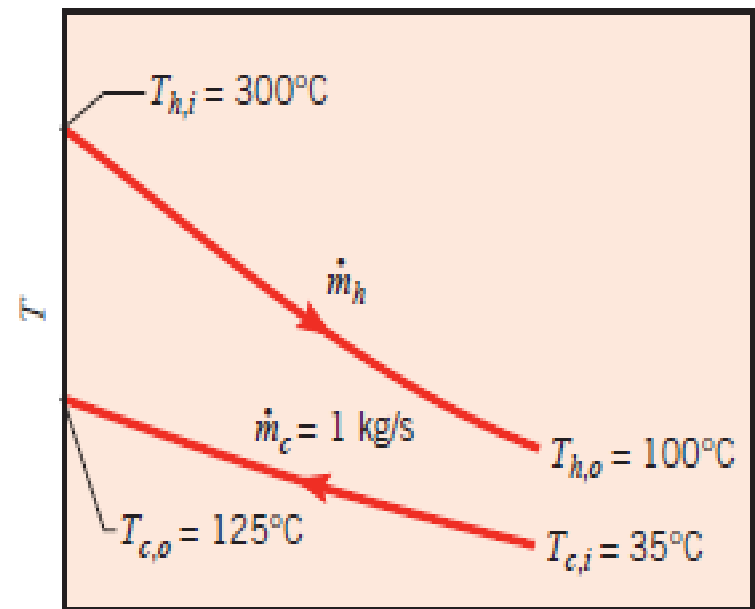
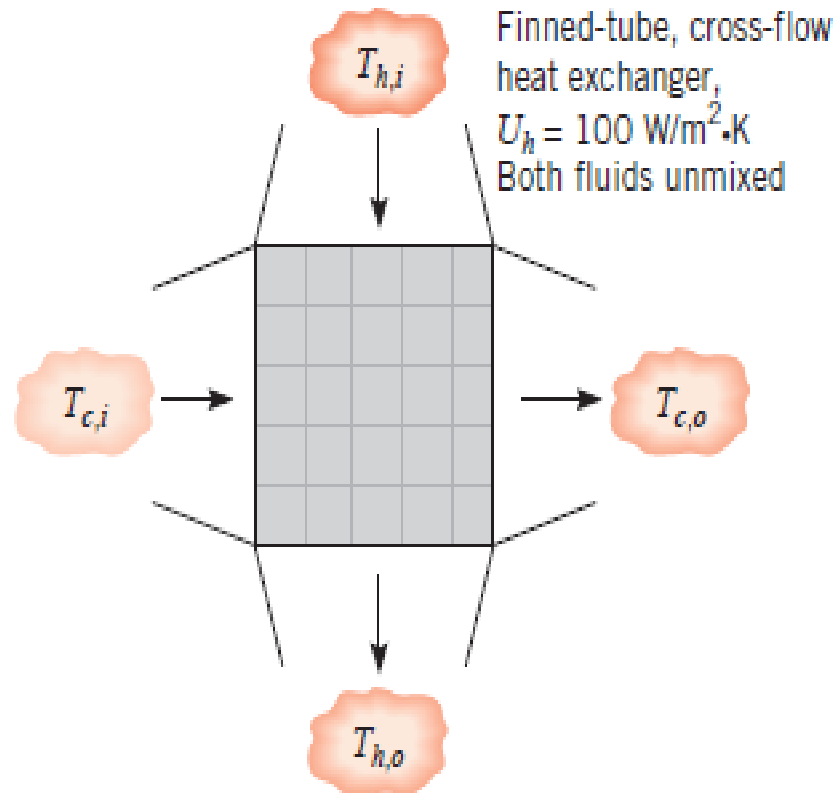
Effectiveness of a single pass, cross-flow heat exchanger with one fluid mixed and the other unmixed (Equations 11.33, 11.34).



problem

Hot exhaust gases, which enter a finned-tube, cross-flow heat exchanger at 300°C and leave at 100°C , are used to heat pressurized water at a flow rate of 1 kg/s from 35 to 125°C . The overall heat transfer coefficient based on the gas-side surface area is $U_h = 100 \text{ W/m}^2 \cdot \text{K}$. Determine the required gas-side surface area A_h using the NTU method.

Schematic



Try to solve the problem