

Data Sheet for Fluid Mechanics Course

One atmosphere = 760 mm Hg = 101.3 kN = 14.7 psia

$\rho_{H_2O} = 1000 \text{ kg m}^{-3} = 62.3 \text{ lb}_m/\text{ft}^3$;

$\rho_{Hg} = 13600 \text{ kg}^{-3} = 845 \text{ lb}_m/\text{ft}^3$

$\mu_{H_2O} = 0.001 \text{ Pa s} = 1 \text{ cP} = 2.09 \times 10^{-3} \text{ lb}_f \text{ s}/\text{ft}^2$

Acceleration due to gravity = $9.81 \text{ ms}^{-2} = 32.2 \text{ ft s}^{-2}$;

$g_c = 32.2 \text{ lbm ft}/\text{lb}_f \text{ s}^2$

$1 \text{ ft}^3 = 28.1 \text{ L} = 7.48 \text{ gal}$

$1 \text{ hp} = 0.746 \text{ kW} = 550 \text{ ft lb}_f/\text{s}$

$1 \text{ ft} = 12 \text{ in}$, $1 \text{ in} = 25.4 \text{ mm}$, $1 \text{ m} = 100 \text{ cm} = 1000 \text{ mm}$

Universal gas constant = $10.73 \frac{(\text{lb}_f/\text{in}^2)\text{ft}^3}{\text{lbmol}\cdot^\circ\text{R}}$; $^\circ\text{R} = ^\circ\text{F} + 460$; $\text{K} = ^\circ\text{C} + 273$

Equations required for problems involving pipe fittings, pipe friction, and entrance and exit losses.

1] Bernoulli's equation:

$$\Delta \left(\frac{p}{\rho} + gz + \frac{V^2}{2} \right) = + \frac{dW_{ao}}{dm} - \mathcal{F}_{tot}$$

$$\mathcal{F}_{tot} = \mathcal{F}_{\text{pipe friction}} + \mathcal{F}_{\text{fittings}} + \mathcal{F}_{\text{enlargement and contraction}}$$

2] Continuity equation:

$$\dot{m} = \rho AV = \rho Q$$

3] Reynolds:

$$\text{Re} = \frac{\rho V D}{\mu} = \frac{4 \rho Q}{\pi \mu D} = \frac{4 \dot{m}}{\pi \mu D}$$

4] Hagen equation:

$$Q = \frac{\pi \Delta P D^4}{128 \mu \Delta x}$$

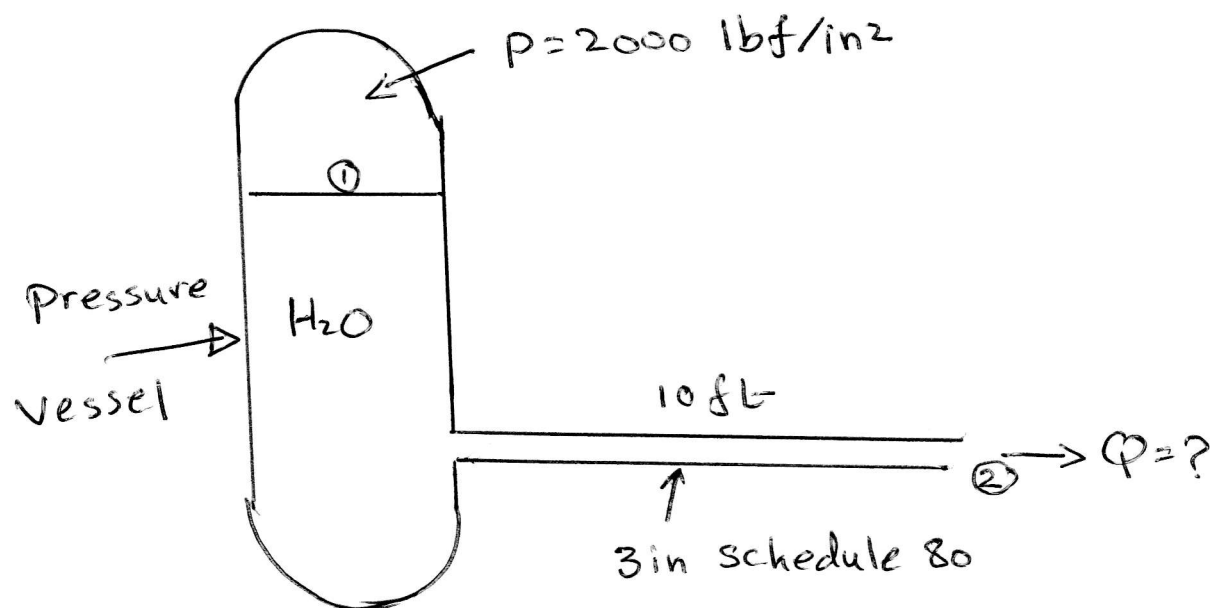
5] Friction Losses

- Pipe friction $\mathcal{F}_{\text{Pipe}} = \frac{4f \Delta x V^2}{2D}$
- Entrance losses (Contraction) $\mathcal{F}_{\text{Contraction}} = K \frac{V^2}{2}$; K from chart
- Exit losses (Expansion) $\mathcal{F}_{\text{Expansion}} = K \frac{V^2}{2}$; $K = \left[1 - \left(\frac{D_1}{D_2} \right)^2 \right]^2$
- Pipe fittings $\mathcal{F}_{\text{Fittings}} = \frac{4f[\sum nD]V^2}{2D} = 4f[\sum n] \frac{V^2}{2}$

6] Friction Factor

- Laminar: $f = \frac{16}{\text{Re}}$
- Turbulent: $f = 0.001375 \left[1 + \left(20000 \frac{\epsilon}{D} + \frac{10^6}{\text{Re}} \right)^{1/3} \right]$ (or any other convenient method)

ex

Given:

pipe size: 3 in schedule 80

Length: 10 ft

 $P_{\text{tank}}: 2000 \text{ psia}$ $P_2: P_{\text{atm}} = 14.6 \text{ psia.}$ Required: Q Solution:

This is a type 2 problem.

Apply BE between ① and ②

$$\frac{P_2 - P_1}{\rho} + g\Delta z + \frac{V_2^2 - V_1^2}{2} = -\mathcal{F}_{\text{tot.}}$$

 $V_1 \approx 0$ (Large cross section.) $\Delta z \approx 0$ (negligible compared to other terms)

$$\mathcal{F}_{\text{tot}} = \mathcal{F}_{\text{pipe}} + \mathcal{F}_{\text{entrance}}$$

$$= 4f \frac{\Delta x}{D} \cdot \frac{V_2^2}{2} + K \frac{V_2^2}{2}$$

Substitute in BE and rearrange

$$\frac{P_1 - P_2}{2} = \frac{V_2^2}{2} + \left[\underbrace{K \frac{V_2^2}{2}}_{f_{tot.}} + 4f \frac{\Delta x}{D} \frac{V_2^2}{2} \right]$$

$$= \left[1 + K + 4f \frac{\Delta x}{D} \right] \frac{V_2^2}{2}$$

$$\therefore V_2 = \left[\frac{2(P_1 - P_2) / \rho}{1 + K + 4f \frac{\Delta x}{D}} \right]^{1/2} \quad [1]$$

since $D_{pipe} \ll D_{tank} \therefore K = 0.5$ (from chart)

For 3 in schedule 80, ID = 2.9 in (from table).

Assume commercial steel $\rightarrow \epsilon = 0.0018$ in

$$\therefore (\epsilon/D) = \frac{0.0018}{2.9} = 0.00062$$

To solve the problem we must solve equation [1] and [2] simultaneously, or using the procedure explained earlier.

$$f = 0.001375 \left[1 + \left(20000 \frac{\epsilon}{D} + \frac{106}{Re} \right)^{1/3} \right] \quad [2]$$

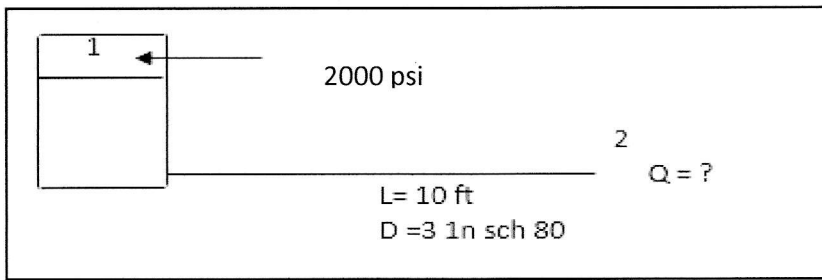
$$Re = \frac{\rho V_2 D}{\mu}$$

$$\rho_{H_2O} = 62.3 \text{ lbm/ft}^3$$

$$\mu_{H_2O} = 2.09 \times 10^{-3} \text{ lbf s/ft}^2$$

solution: similar trial and error as in H/w

$$Q = 16 \text{ ft}^3 \text{ s}^{-1}$$



1) Apply BE Between 1 and 2

$$\frac{P_2 - P_1}{\rho} + g\Delta Z + \frac{V_2^2 - V_1^2}{2} = - \mathcal{F}_{Total} ; \quad g\Delta Z \cong 0 \text{ and } V_1^2 \cong 0 \text{ (large cross section)}$$

$$\mathcal{F}_{Total} = \left[1 + K + 4f \frac{\Delta x}{D} \right] \frac{V_2^2}{2} ;$$

$$V_2 = \left[\frac{2(P_1 - P_2)}{\rho \left(1 + K + 4f \frac{\Delta x}{D} \right)} \right]^{1/2}$$

$$Q = V_2 * \pi \frac{D^2}{4} = \left[\frac{2(P_1 - P_2)}{\rho \left(1 + K + 4f \frac{\Delta x}{D} \right)} \right]^{1/2} * \pi \frac{D^2}{4} = K_1 * \left[\frac{1}{\left(1 + K + 4f \frac{\Delta x}{D} \right)} \right]^{1/2}$$

$$K_1 = \left[\frac{2(P_1 - P_2)}{\rho} \right]^{1/2} * \pi \frac{D^2}{4}$$

$$Re = \frac{4\rho}{\pi \mu D} Q = K_2 Q ; \quad K_2 = \frac{4\rho}{\pi \mu D}$$

(P1-P2). Psi	2000				
Density, lbm/ft3	62.3	K entrance	0.5 K1=	25.02756	
Viscosity,lbf s/ft2	2.09E-03				
g, ft/s ²	32.2	Length, ft	10 K2=	4877.298	
Roughness, in	0.0018	ε/D=	0.000621		
Diameter of pipe,in	2.9				

• Laminar: $f = \frac{16}{Re}$

• Turbulent: $f = 0.001375 \left[1 + \left(20000 \frac{\epsilon}{D} + \frac{10^6}{Re} \right)^{1/3} \right]$

Trial	f	Q=K1*[]	Re = K ₂ · Q	f from eq or Chart	Criteria
1	0.005	16.4046	80010.11737	0.005390813	7.816256904
2	0.005391	16.18129	78920.98075	0.00540006	0.171526421
3	0.0054	16.17612	78895.74757	0.005400276	0.004013712

