

$$5.4 \quad \Delta P = \frac{\rho(V_1^2 - V_2^2)}{2} = \frac{\rho}{2} \left[ \left( 10 \frac{\text{ft}}{\text{s}} \right)^2 - \left( \frac{10}{3} \frac{\text{ft}}{\text{s}} \right)^2 \right] = \rho \frac{\left( 100 \frac{\text{ft}^2}{\text{s}^2} \right)}{9/4}$$

(a) For water

$$\Delta P = 62.3 \frac{\text{lbm}}{\text{ft}^3} \left( \frac{4}{9} \right) \left( 100 \frac{\text{ft}^2}{\text{s}^2} \right) \cdot \frac{\text{lbf s}^2}{32.2 \text{ lbm ft}} \cdot \frac{\text{ft}^2}{144 \text{ in}^2} = 0.60 \text{ psi} = 4.1 \text{ kPa}$$

(b) For air

$$\Delta P = \text{above answer} \cdot \frac{0.075}{62.3} = 7.2 \cdot 10^{-4} \text{ psi} = 0.0050 \text{ kPa}$$

$$5.14 \quad V = \sqrt{2gh}; \quad Q = VA_{\text{outlet}} = V_{\text{tank surface}} A_{\text{tank}} = A_{\text{tank}} \left( -\frac{dh}{dt} \right)_{\text{tank}}$$

$$\left( -\frac{dh}{dt} \right)_{\text{tank}} = \frac{A_{\text{outlet}}}{A_{\text{tank}}} \sqrt{2gh} = 0.01 \sqrt{2 \cdot 9.81 \frac{\text{m}}{\text{s}^2} \cdot 10 \text{ m}} = 0.14 \frac{\text{m}}{\text{s}} = 0.46 \frac{\text{ft}}{\text{s}}$$

Some students will say you should use  $V = \sqrt{\frac{2gh}{1 - (A_2/A_1)^2}}$ . That multiplies the above

answers by 1.00005, which is clearly negligible compared to the uncertainties introduced by the standard Torricelli's assumptions.

$$5.15 \quad V_2 = \sqrt{2 \left( -\frac{\Delta P}{\rho} - g\Delta z \right)}, \text{ but } \Delta P = \rho_{\text{gasoline}} g\Delta z \text{ so that}$$

$$V_2 = \sqrt{2g(-\Delta z) \left( 1 - \frac{\rho_{\text{gas}}}{\rho_w} \right)} = \sqrt{2 \left( 32.2 \frac{\text{ft}}{\text{s}^2} \right) (30 \text{ ft}) (1 - 0.72)} = 23.3 \frac{\text{ft}}{\text{s}} = 7.09 \frac{\text{m}}{\text{s}}$$

This is the same as Ex. 5.5, with different fluids.

$$5.16^* \quad V_2 = \sqrt{-\frac{\Delta P}{\rho_w}} = \sqrt{\frac{P_1 - P_2}{\rho_w}}$$

$$P_1 = 30 \text{ ft} \cdot g\rho_{\text{water}}; \quad P_2 = 10 \text{ ft} \cdot g\rho_{\text{water}} + 20 \text{ ft} \cdot g\rho_{\text{oil}}$$

$$P_1 - P_2 = 20 \text{ ft} \cdot g(\rho_{\text{water}} - \rho_{\text{oil}})$$

$$V = \sqrt{2(20 \text{ ft}) \cdot \left( 32.2 \frac{\text{ft}}{\text{s}^2} \right) \cdot (1 - 0.9)} = 11.3 \frac{\text{ft}}{\text{s}} = 3.46 \frac{\text{m}}{\text{s}}$$

$$\begin{aligned}
 5.17 \quad F &= - \left( \frac{\Delta P}{\rho} + g\Delta z + \frac{\Delta V^2}{2} \right) \quad \text{Assuming the flow is from left to right} \\
 F &= \left( - \frac{8 \frac{\text{lbf}}{\text{in}^2}}{62.3 \frac{\text{lbm}}{\text{ft}^3}} \cdot \frac{32.2 \text{ lbf ft}}{\text{lbf s}^2} \cdot \frac{144 \text{ in}^2}{\text{ft}^2} + 32.2 \frac{\text{ft}}{\text{s}^2} \cdot 20 \text{ ft} + 0 \right) \\
 &= \left( -595 \frac{\text{ft}}{\text{s}^2} + 644 \frac{\text{ft}^2}{\text{s}^2} \right) = -48.6 \frac{\text{ft}^2}{\text{s}^2} = -4.51 \frac{\text{m}^2}{\text{s}^2}
 \end{aligned}$$

The negative value of the friction heating makes clear that the assumed direction of the flow is incorrect, and that the flow is from right to left.

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$$\begin{aligned}
 5.18^* \quad V_2 &= \sqrt{2 \left( - \frac{\Delta P}{\rho} - g\Delta z \right)} \\
 V_2 &= \sqrt{2 \left( \frac{20 \frac{\text{lbf}}{\text{in}^2}}{62.3 \frac{\text{lbm}}{\text{ft}^3}} \cdot \frac{32.2 \text{ lbf ft}}{\text{lbf s}^2} \cdot \frac{144 \text{ in}^2}{\text{ft}^2} + 5 \text{ ft} \cdot 32.2 \frac{\text{ft}}{\text{s}^2} \right)} = 57.4 \frac{\text{ft}}{\text{s}} = 17.5 \frac{\text{m}}{\text{s}}
 \end{aligned}$$

$$\begin{aligned}
 5.34^* \quad V_2 &= \sqrt{\frac{\frac{2(P_1 - P_2)}{\rho} + 2g(z_1 - z_2)}{1 - (A_1 / A_2)^2}} \\
 &= \sqrt{\frac{\frac{2(7 - 5) \frac{\text{lbf}}{\text{in}^2}}{0.72(62.3) \frac{\text{lbm}}{\text{ft}^3}} \cdot \frac{32.2 \text{ lbf ft}}{\text{lbf s}^2} \cdot \frac{144 \text{ in}^2}{\text{ft}^2} + 2 \cdot 32.2 \frac{\text{ft}}{\text{s}^2} \cdot 2 \text{ ft}}{1 - (0.5)^4}} = 24.0 \frac{\text{ft}}{\text{s}} = 7.33 \frac{\text{m}}{\text{s}} \\
 Q &= VA = 24.0 \frac{\text{ft}}{\text{s}} \cdot \frac{\pi}{4} (0.5 \text{ ft})^2 = 4.72 \frac{\text{ft}^3}{\text{s}} = 0.13 \frac{\text{m}^3}{\text{s}}
 \end{aligned}$$

$$\begin{aligned}
5.36^* \quad V &= C_v \sqrt{\frac{2(P_1 - P_2)}{\rho(1 - (A_2/A_1)^2)}}; \quad P_{\text{water-mercury interface}} = P_2 + \rho_{\text{water}} g \cdot 2 \text{ in} \\
P_{\text{mercury-air interface}} &= P_1 = P_{\text{mercury-water interface}} + \rho_{\text{Hg}} g \cdot 0.1 \text{ in} \\
P_1 - P_2 &= 2 \text{ in } \rho_{\text{wg}} + 0.1 \text{ in } \rho_{\text{Hg}} g = \rho_{\text{wg}} \cdot (2 + 1.36) \text{ in} \\
V &= 1.0 \sqrt{\frac{2 \cdot 32.2 \frac{\text{ft}}{\text{s}^2} \cdot 62.3 \frac{\text{lbm}}{\text{ft}^3} \cdot \left(\frac{3.36}{12} \text{ ft}\right)}{\left(0.075 \frac{\text{lbm}}{\text{ft}^3}\right)(1 - 0.1^2)}} = 123 \frac{\text{ft}}{\text{s}} = 37.5 \frac{\text{m}}{\text{s}} \\
Q &= VA = 123 \frac{\text{ft}}{\text{s}} \cdot 1 \text{ ft}^2 = 123 \frac{\text{ft}^3}{\text{s}} = 3.48 \frac{\text{m}^3}{\text{s}}
\end{aligned}$$

$$\begin{aligned}
5.39 \quad V_2 &= C_v \sqrt{\frac{2(-\Delta P)}{\rho \left(1 - \left(\frac{D}{D_0}\right)^4\right)}}; \quad -\Delta P = \frac{\rho V_2^2}{2 C_v^2} \left(1 - \left(\frac{D}{D_0}\right)^4\right) \\
V_2 &= \frac{1 \text{ ft}}{\text{s}} \sqrt{\frac{\frac{\pi}{4} (1 \text{ in})^2}{\frac{\pi}{4} (0.2 \text{ in})^2}} = 25 \frac{\text{ft}}{\text{s}} \\
-\Delta P &= \frac{\left(55 \frac{\text{lbm}}{\text{ft}^3}\right) \left(25 \frac{\text{ft}}{\text{s}}\right)^2 (1 - (0.2)^4)}{(2)(0.6)^2} \cdot \frac{\text{lbf s}^2}{32.2 \text{ lbm ft}} \cdot \frac{\text{ft}^2}{144 \text{ in}^2} = 10.3 \frac{\text{lbf}}{\text{in}^2} = 70.9 \text{ kPa}
\end{aligned}$$

5.41 This is simplest by trial and error. First we guess that  $D_2/D_1 = 0.5$ . Then

$$\begin{aligned}
V_2 &= V_1 \cdot \left(\frac{D_1}{D_2}\right)^2 = 1 \frac{\text{ft}}{\text{s}} \cdot \left(\frac{1}{0.5}\right)^2 = 4 \frac{\text{ft}}{\text{s}} \text{ and} \\
-\Delta P &= \left(1 - \left(\frac{D_2}{D_1}\right)^4\right) \frac{\rho}{2} \cdot \left(\frac{V}{C_v}\right)^2 \\
&= (1 - 0.5^4) \frac{13.6 \cdot 62.3 \frac{\text{lbm}}{\text{ft}^3}}{2} \cdot \left(\frac{4 \frac{\text{ft}}{\text{s}}}{0.62}\right)^2 \cdot \frac{\text{lbf s}^2}{32.2 \text{ lbm ft}} \cdot \frac{\text{ft}^2}{144 \text{ in}^2} = 3.57 \frac{\text{lbf}}{\text{in}^2}
\end{aligned}$$

This done by Excel as explained in the Excel file given in e learning

$$5.51 \quad V_{\text{out}} = \sqrt{2gh}; \quad Q_{\text{out}} = A_{\text{exit}} V_{\text{out}} = -A_{\text{tank}} \frac{dh}{dt}$$

$$A_{\text{tank}} = 50 \text{ ft}^2 + 50 \text{ ft}^2 \left( \frac{h}{20 \text{ ft}} \right) = 50 \text{ ft}^2 + 2.5 \text{ ft} \cdot h = a + bh$$

where  $a$  and  $b$  are constants.

$$\frac{dh}{dt} = \frac{-A_{\text{out}} \sqrt{2gh}}{a + bh}; \quad -A_{\text{out}} \sqrt{2g} \int_0^{\Delta t} dt = \int_{h_0}^h \frac{adh}{\sqrt{h}} + b \int_{h_0}^h \sqrt{h} dh$$

$$\Delta t = \frac{1}{A_{\text{out}} \sqrt{2g}} \left[ \frac{a}{\frac{1}{2}} \sqrt{h} + \frac{b}{\frac{3}{2}} h^{\frac{3}{2}} \right]_{h=0}^{h=h_{\text{top}}}$$

$$= \frac{1}{1 \text{ ft}^2 \sqrt{2 \cdot 32.2 \frac{\text{ft}}{\text{s}^2}}} \left[ \frac{50 \text{ ft}^2}{\frac{1}{2}} \sqrt{20 \text{ ft}} + \frac{2.5 \text{ ft}}{\frac{3}{2}} (20 \text{ ft})^{\frac{3}{2}} \right] = 74.3 \text{ s}$$