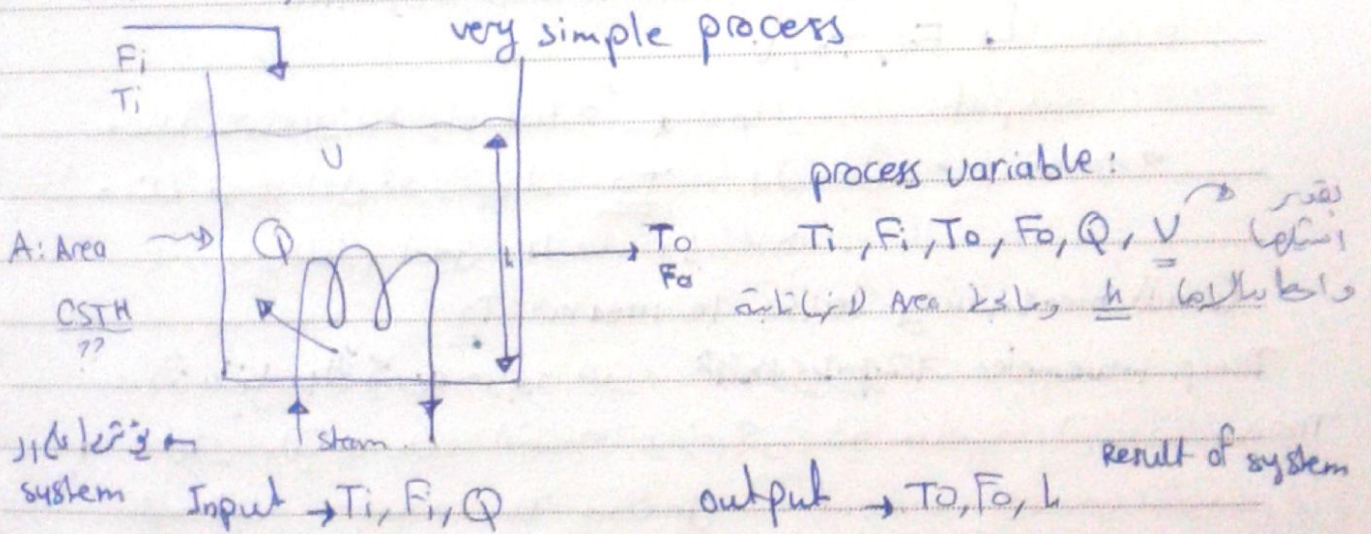
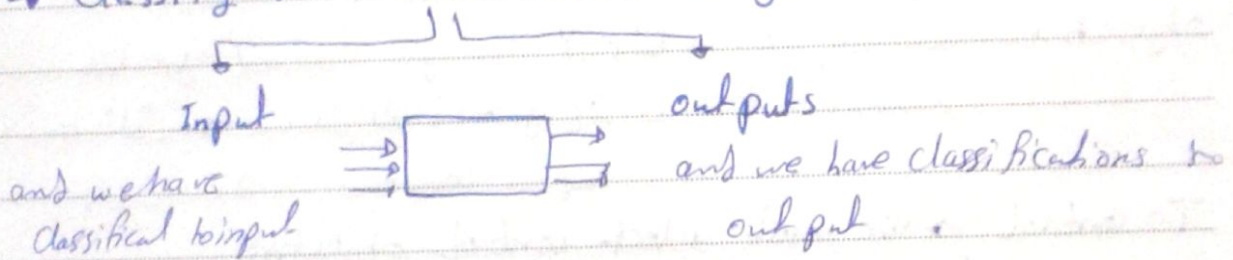


text book : process Dynamics and control 3rd seborg.

Grads → 30% mid 20% project 10% Class participated
40% Final.

process ?

* process variable ... if They control conform with The variable of
The process ... it related with change in variable.
→ classify it to two main categories.



هذا تعريف غير دقيق للعمليات في التحكم
لأنه يجب أن تكون العملية ذات متغيرات
دخول وإخراج متغيرة، داخلية، وإخراجية
في حالة أن F_o هي Input
في حالة أن F_o هي Output
في حالة أن F_o هي Input

Input \rightarrow any variable affect The system
 output \rightarrow any variable represent The affect of The system on The result.

why we are studying The Variable?

وإذا كنت تريد أن تتحكم بالمتغير
 IF you like to control .. what you should control on...?

الهدف من التحكم في المتغير y هو التحكم في
 المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 Levels control

To control \rightarrow we must select control objective

المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 F_o, T_o, V

الهدف من التحكم في المتغير y هو التحكم في
 المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 "control objective" \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 "measurib" \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 control variable \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow

① add measuring devise to measur T_o

Temp. transducer \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow

Transmission \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 indication \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 controller \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 (TC)

reference \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 set point \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 control loop \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow \rightarrow المتغير y في Flow
 set point

Control

[Control loop :-

- ① controlled variable (TO)
- ② measuring device (TT)
- ③ controller (TC)
 - ↳ TC
 - ↳ reference (set point)
 - ↳ desired

④ Input : adjusted → adjustment
 ↳ manipulated variable ↳ manipulation

④ Input : adjusted → adjustment
 ↳ manipulated variable ↳ manipulation

⑤ The final control element

(valve) → line

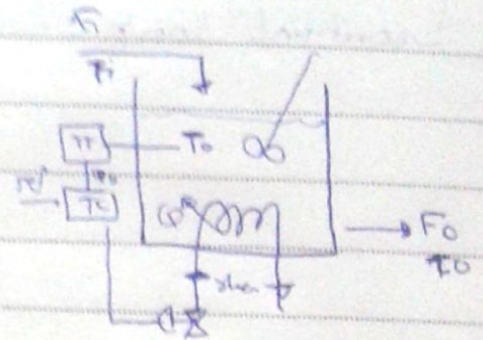
The element use in adjusted The manipulated variable.
 signal لا آخر مكة The final... signal التي خرجت

divice transition" ج. في

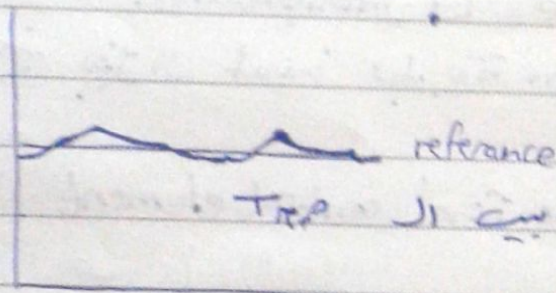
" final → The end of chapter one ! "

To summary The last lecture →
control loop

- 1- controlled variable (control objective)
- 2- measuring device
- 3- controllers
- 4- final control element
- 5- manipulated variable



مراقبة (نظم) ←



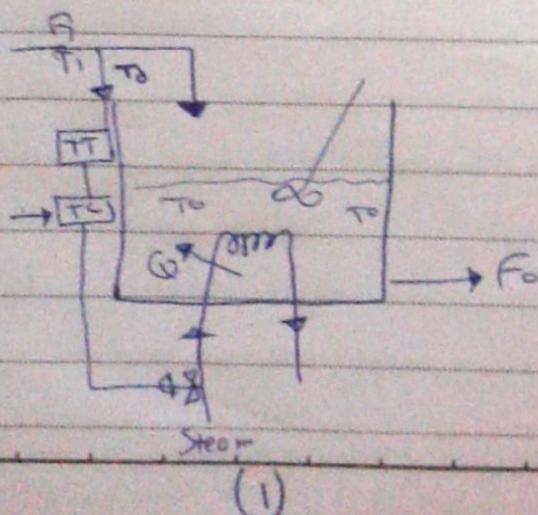
Change action The controller is reached
بعض التغييرات في النظام

المتغيرات في النظام وتكون في حالة التغيير

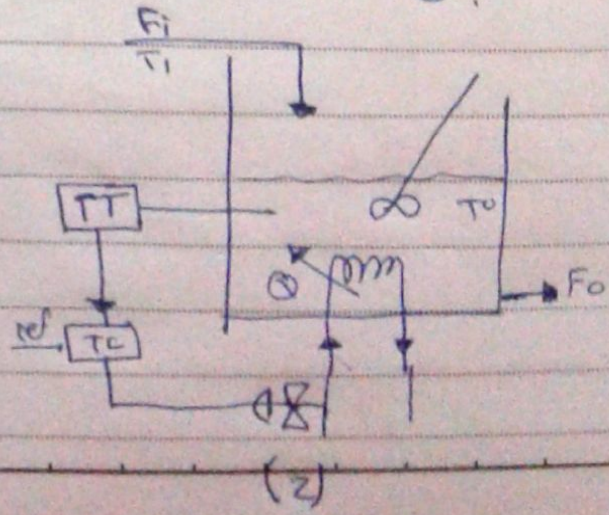
بدرجته التغيير في حاله

input (تغيير في المدخلات) التغيير في المدخلات

بعض التغييرات في النظام وتكون في حالة التغيير

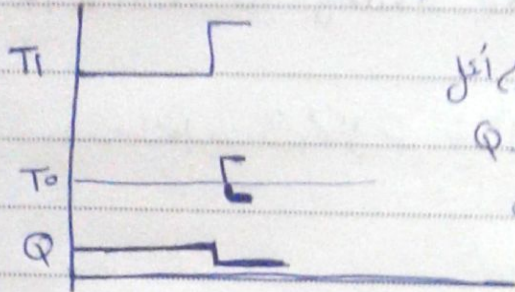


(1)



(2)

في (1) منحنى في وقت التوقع زيادتها ارتفاعها بدون إجراء اختيار
 (2) منحنى في وقت التوقع زيادتها، التوقع



رغم ذلك T توقيت تزايد زمني

إجراء اختيار زمني بأشياء أقل ال Q

لذلك زادت قيمة ال T كما توقيت

بتقصير ال Q حسب الحالة

المسقة هنا لغو "بعض"

ومررت على ال T_0 منحنى ال line الطعني #

وإحتمالها في عتاً

2 control stages → ① advance action

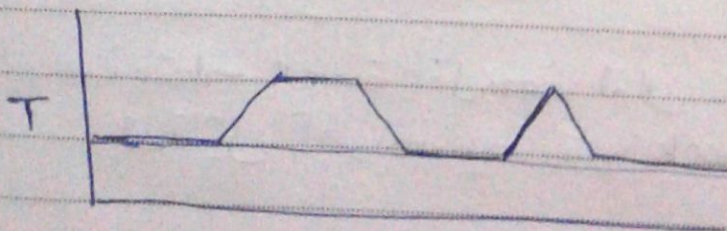
② reaction

Free Feedback control → مخطط في تغير في ال

• Feed back control → رد فعل في، التغير في ال

• Feed Forward control → we take action "advance action"

steady state → measure value equal to The reference



advantage of Feedback control →

→ it take care of The change or correct it occur in The system

dis advantage →

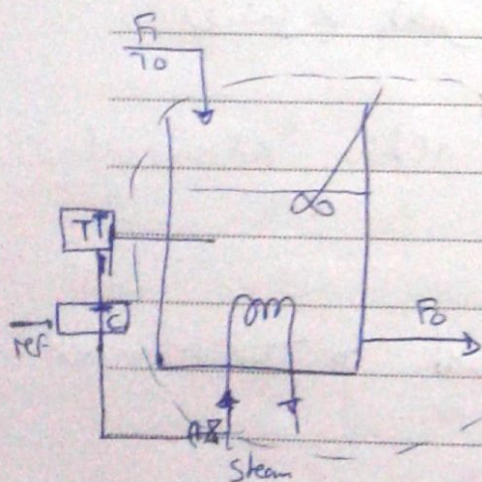
Feed Forward

→ لا يباين هو لا يتنازل قبل حدوث التغيير (التي يتنبأ أن يكون)
هذا هو ما قبل التغيير في input

IF The only change occur in The system occur by certain source by Feed Forward & it's could the perfect control

How To combined The Feed backward & Feed Forward?

الجواب بالحاسبة والاختبار بالحق



diagram,
p & I D
process
instrument
piping

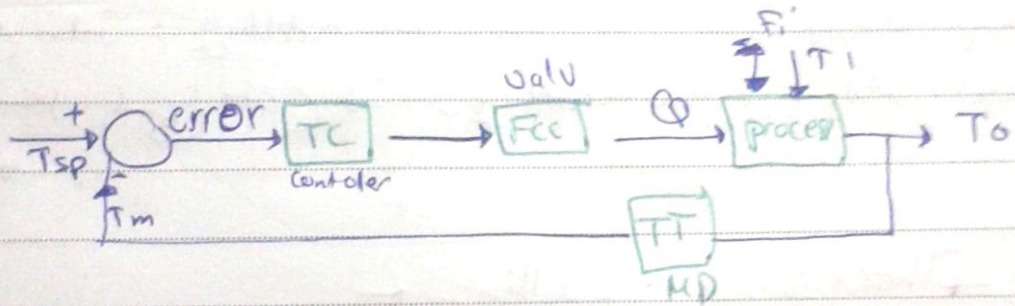
هذا الشكل هو الشكل الذي نستخدمه
black diagram

① خلية لمدى د ال Control Variable ← عبارة عن output و process

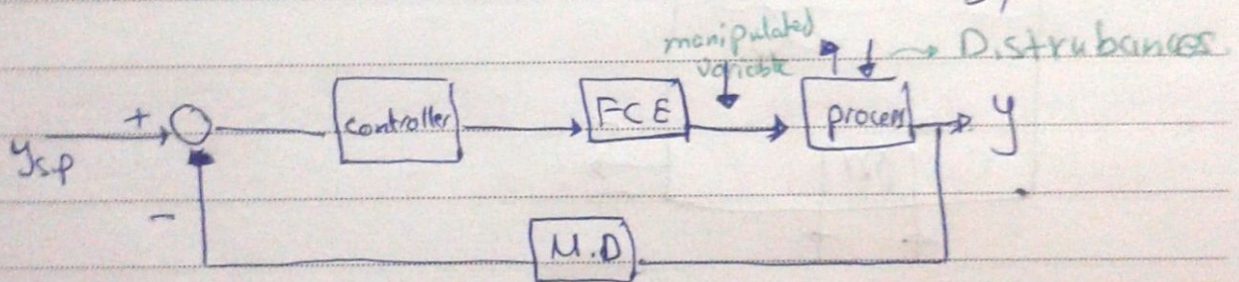
② خلية د ال manipulated variable

③ ارجع الى انشورتيه ل

ولا يتم تغير كل المتغيرات ~~التي~~ بل فقط Input و output
 adapt تغيره في ال process كغيره



28-9-2017 عاينة



process modelling

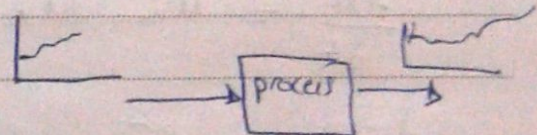
مبنى ال uns

Theoretical modelling

we start with the basic equation describe the process [mass balance/energy balance, ...]

Rate equation

experimental modelling



بغير تغير ال input

Theoretical is the best 15 points

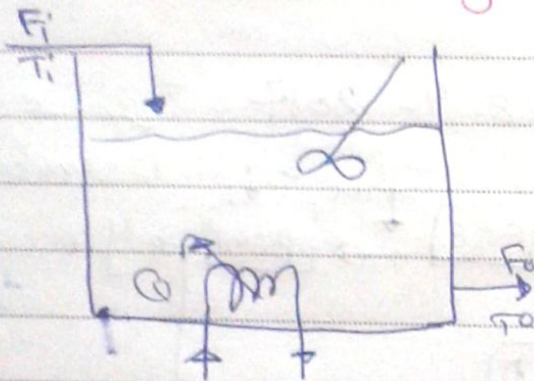
التي ال process energy mass

✖ experimental modeling diff: cells is specific for process for the eqib and condition under the experimental condition which done under it.

→ experimental need to be Generalization - it's not general

الفرق بين النمذجة النظرية والنمذجة التجريبية
النمذجة النظرية: تعتمد على المعادلات الرياضية والنظريات الفيزيائية والكيميائية.
النمذجة التجريبية: تعتمد على البيانات التجريبية والقياسات المباشرة.

→ Theoretical modelling ←



mol / mass balance and energy balance →

$$\frac{dN}{dt} = M_{in} - M_{out} + \begin{matrix} \text{generation} \\ \text{or} \\ \text{consumption} \end{matrix} \rightarrow \text{component balance}$$

$$\frac{dN}{dt} = M_{in} - M_{out} \rightarrow \text{overall mass balance}$$

$$\frac{dPAh}{dt} = \rho F_i - \rho_o F_o$$

F_i = volumetric flow rate

$$A \frac{dh}{dt} = F_i - F_o$$

$\frac{m^3}{min}$

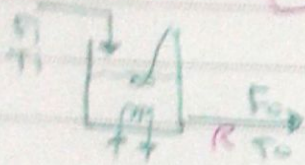
(4)

constant ρ is constant

$$A \rho \frac{dh}{dt} = \rho F_i - \rho F_o$$

$$A \frac{dh}{dt} = F_i - F_o$$

assumption of This ρ is constant
 Let's consider F_o is constant \leftarrow h is variable



$$A \frac{dh}{dt} = F_i - \frac{h}{R}$$

$$h + R A \frac{dh}{dt} = R F_i \rightarrow \boxed{R A \frac{dh}{dt} + h = R F_i}$$

process \leftarrow h is variable
 This equation related change of h due to change in F_i
 F_o is constant

one at put \leftarrow system is affected by only and one input.

- Energy balance

$$\frac{dE}{dt} = E_{in} - E_{out}$$

let it = 0 \rightarrow $\frac{dE}{dt} = 0$

$$\frac{d}{dt} [\rho V c_p (T_o - T_r)] = \rho c_p F_i (T_i - T_{ref}) - \rho c_p F_o (T_o - T_{ref}) + Q$$

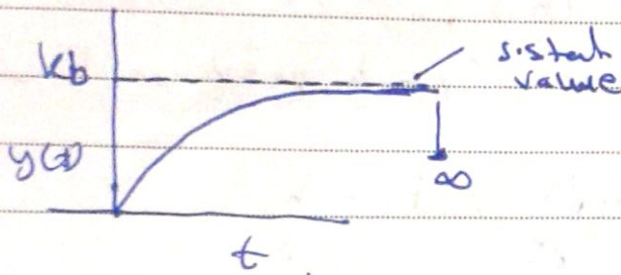
let it = 0 \rightarrow $\frac{dT_o}{dt} = 0$

$$\frac{d(h T_o)}{dt} = \frac{1}{A} F_i T_i - \frac{1}{A} F_o T_o + \frac{Q}{\rho c_p A} \rightarrow \boxed{\frac{dT_o}{dt} + T_o = \frac{1}{A} F_i T_i + \frac{1}{\rho c_p A} Q}$$

10/8 initial value theorem, final value theorem

$$y(s) = \frac{K}{as+1} + \frac{b}{s} \quad , \quad y(t) = \int_0^{-1} \frac{Kb}{(as+1)s}$$

$$y(t) = Kb [1 - e^{-t/a}]$$



or using Final value Theorem

$$y_{\infty}(t) = \lim_{s \rightarrow 0} s y(s)$$

$$y_{\infty}(t) = \lim_{s \rightarrow 0} s \frac{Kb}{(as+1)s} = Kb$$

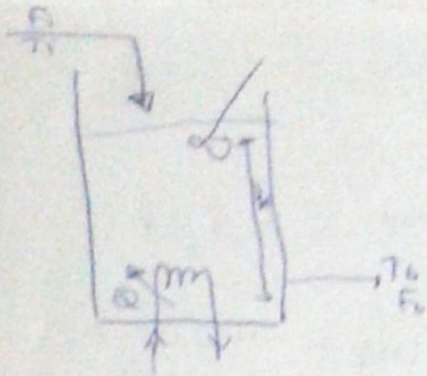
Initial value Theorem

$$y(0) = \lim_{s \rightarrow \infty} s y(s)$$

$$= \lim_{s \rightarrow \infty} s \frac{Kb}{(as+1)s} = 0$$

2017-10-8

④



$$AR \frac{dh}{dt} + h = R F_i$$

Transfer function

variable, (تغير) ~ variable, (تغير) from the state

at steady state.

$$\left(\frac{dh}{dt} \right)_{ss} = 0 \Rightarrow 0 + h_{ss} = R F_{i,ss}$$

$$S.S \rightarrow (0 + h_{ss} = R F_{i,ss})_{ss}$$

$$AR \frac{d(h - h_{ss})}{dt} + (h - h_{ss}) = R(F_i - F_{i,ss})$$

$$AR \frac{dh'}{dt} + h' = R F_i'$$

$$\begin{aligned} h' &= h - h_{ss} \\ F_i' &= F_i - F_{i,ss} \end{aligned}$$

Deviation Form

Why to?

to give up the ~~relation~~ ^{direct} change of the output as a function of input change in

Caplace Transform $\xrightarrow{\text{Laplace}}$ Transfer function

real domain time

Algebraic eq

linear differential eq

$$\mathcal{L} y(t) = y(s)$$

imaginary domain

دالة في المجال الحقيقي
تحويل لابلاس
دالة في المجال التخيلي
معادلات تفاضلية

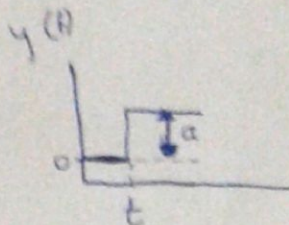
$$\mathcal{L} \frac{dy}{dx} = s y(s) - y(0) \quad \mathcal{L} y dt = \frac{1}{s} y(s)$$

©

changes magnitudes happen in input and response in output.

→ [1] step change

$$y(t) = \begin{cases} 0 & t < 0 \\ a & t \geq 0 \end{cases}$$



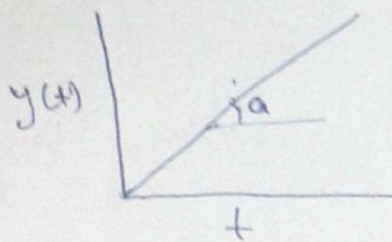
laplace transfer of step function.

$$\mathcal{L} \text{ step f magnitude } a = \underline{\underline{\frac{a}{s}}}$$

why step function is important?
b.c in most cases, (the 'step' happen.)
The change is likely could

دالة كثر استعمالها في
step function

[2] Ramp Function.
 $y(t) = at$



$$\mathcal{L} at = \frac{a}{s^2}$$

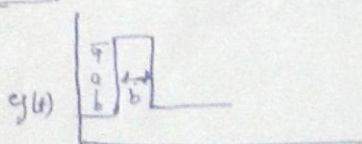
[3] puls function.

دالة نبض

$$\mathcal{L} \text{ puls function} = \frac{(1 - e^{-bs})}{s}$$

دالة نبض عرضها 'b' وارتفاعها 'a'

Ex: step
in
2 step
together.



+ pulse width
= pulse width

4

↓
 $L a \sin \omega t = \left(\frac{1}{\sqrt{2}} \right) \cos$

التقريب 4
200

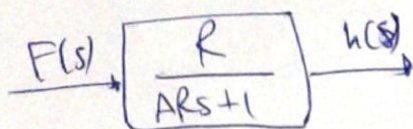
عائشہ راجی کے پرنسپل، لا
لا آئیٹھ
لا سائیٹ
AR

ip. W. 10
فندق
J
الشارع

$$\frac{h(t)}{F_1(t)} \neq$$

$$\frac{L(s)}{F_i(s)} = \frac{R}{ARS + 1}$$

ما اريد، انصحكم



دینا کے لئے ~~میں~~ ^{اپنی} دعا ہے

i) The laplace transfor. of The change in The output TO
The laplace transfn of r , s , input.

Subject Laplace

1. Final Value Theorem : $y(t)_{\infty} = \lim_{s \rightarrow 0} s y(s)$

example

assume $y(s) = \frac{1}{s(s+a)}$, $y(t)_{\infty} \rightarrow y(t)$ and put $t = \infty \rightarrow$ Answer.

$$y(t) = \mathcal{L}^{-1} y(s) = \mathcal{L}^{-1} \frac{1}{s(s+a)} \quad [\text{Partial Fraction}] = \frac{1}{a} (1 - e^{-\frac{1}{a}t})$$

$$y(\infty) = \frac{1}{a} (1 - e^{-\frac{1}{a}\infty}) = 1/a$$

$$\Rightarrow y(t)_{\infty} = \lim_{s \rightarrow 0} \frac{s \cdot 1}{s(s+a)} = \lim_{s \rightarrow 0} \frac{1}{s+a} = \frac{1}{0+a} = \frac{1}{a}$$

Final value of The function That mean
Final Steady State

2. Initial value Theorem

$$y(t)_0 = \lim_{s \rightarrow \infty} s y(s)$$

Initial value of function

للقيمة الأولية

• إذا استخدمنا Initial value Theorem وطبقنا

فإننا نحصل على zero ←

هذا لأن Initial value Theorem لا يمكن استخدامه

في هذه الحالة

10/10/2017

Subject

First order system

It's a system described by a first order "D.E".

In General $\rightarrow a_0 \frac{dy}{dt} + a_1 y(t) = b x(t)$

• Transfer function \rightarrow الـ $\frac{Y(s)}{X(s)}$ \rightarrow الـ $\frac{b}{a_1 s + a_1}$

$a_0 \frac{dy}{dt} + a_1 y(t) = b x(t)$ system

$0 + a_1 y_{ss}(t) = b x_{ss}(t)$ s.s eq

$a_0 \frac{d(y - y_{ss})}{dt} + a_1 (y - y_{ss}) = b (x - x_{ss})$

$a_0 \frac{dy'}{dt} + a_1 y' = b x'(t)$ deviation from

$a_0 \frac{dy(t)}{dt} + a_1 y(t) = b x(t)$

$\frac{a_0}{a_1} \frac{dy(t)}{dt} + y(t) = \frac{b}{a_1} x(t)$

$\frac{a_0}{a_1} [s y(s) - y(0)] + y(s) = \frac{b}{a_1} x(s)$

$y(s) \left[\frac{a_0}{a_1} s + 1 \right] = \frac{b}{a_1} x(s)$

$\frac{y(s)}{x(s)} = \frac{k}{\tau s + 1}$

$k = b/a_1$ s.s gain

$\tau = a_0/a_1$ time constant

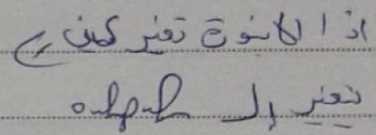
$\tau s + 1$

الـ $\frac{Y(s)}{X(s)}$ \rightarrow الـ $\frac{b}{a_1 s + a_1}$

الـ $\frac{Y(s)}{X(s)}$ \rightarrow الـ $\frac{b}{a_1 s + a_1}$

Change response \rightarrow الـ $\frac{Y(s)}{X(s)}$

الـ $\frac{Y(s)}{X(s)}$ \rightarrow الـ $\frac{b}{a_1 s + a_1}$
الـ $\frac{Y(s)}{X(s)}$ \rightarrow الـ $\frac{b}{a_1 s + a_1}$
الـ $\frac{Y(s)}{X(s)}$ \rightarrow الـ $\frac{b}{a_1 s + a_1}$



$$y(s) = \frac{K}{s+1} + \frac{B}{s}$$

صاف اول الاملا

الزنا - 1st.sg - جف
هنا امر، التوسوس، ليد
مستحب له نظام

K — steady state gain \rightarrow gain or value, value of change

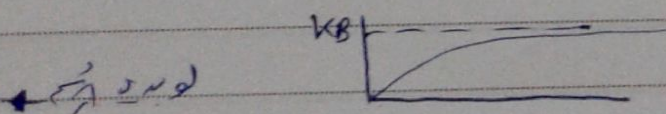
The value of The function of steady state

When you can garanty That your system is ~~affair~~ stable?

at $t = \infty$ $\frac{t = \infty}{y(t) = k_B}$ \hookrightarrow 31 الـ

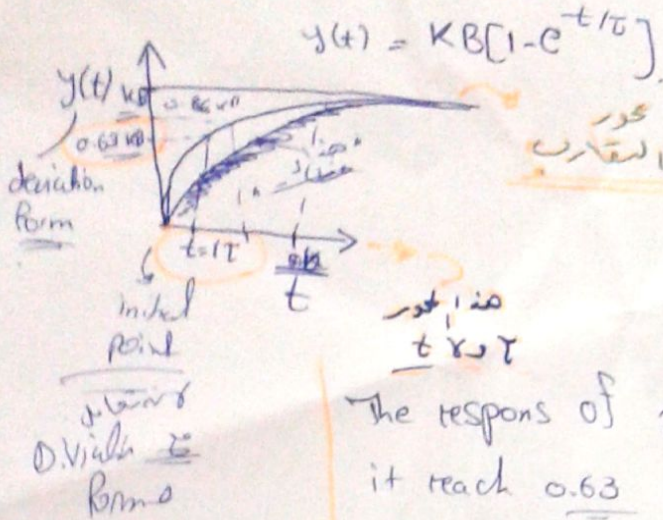
[illegible]

because it defines the value of the function @ 5.5



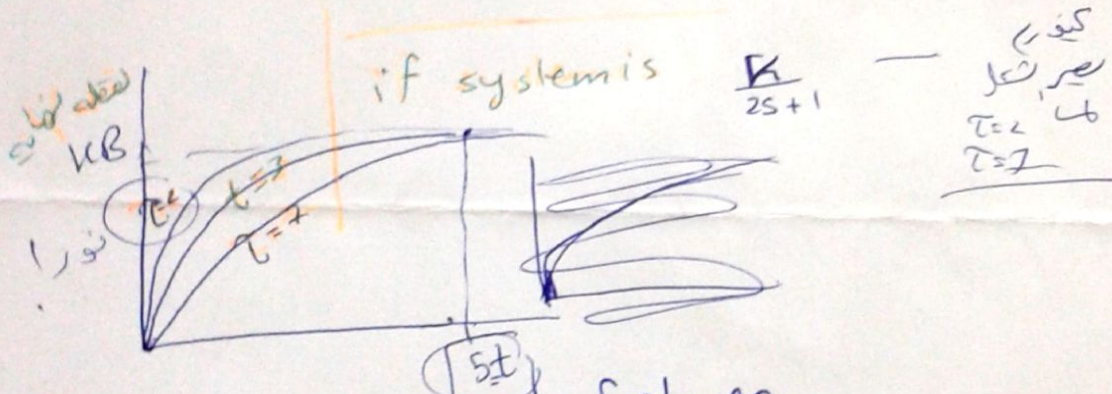
control course

محلقة الخميس [12-oct-2017]



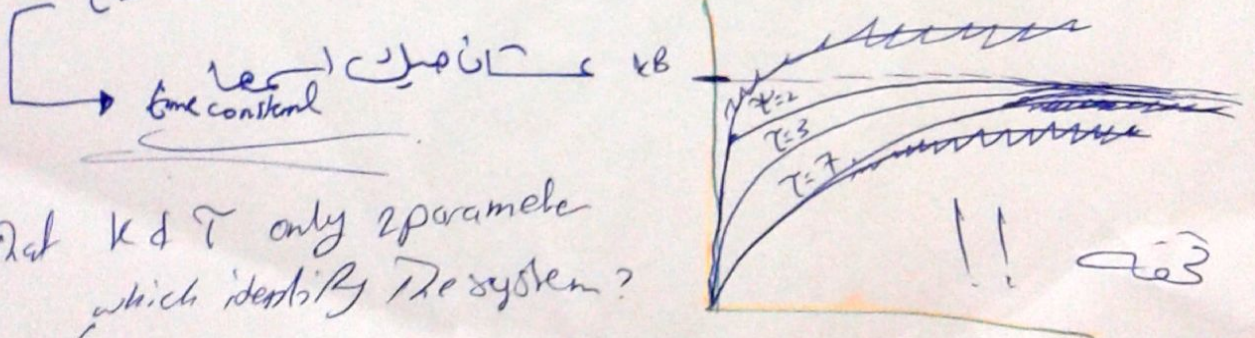
نموذج النظام
لا بد من $\tau \geq 0$
منه لا يوجد $t = \tau$

The response of 1st order function. (system) to a step it reach 0.63 of final steady state.
at $t = 5\tau \rightarrow$ That response to 0.99 of step state
5% error band



نموذج النظام
لا بد من $\tau \geq 0$
منه لا يوجد $t = \tau$

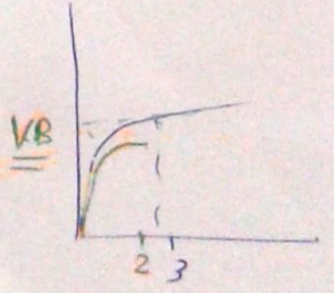
$\tau =$ determine The rate of change.



That K & τ only 2 parameters which identify the system?

نموذج النظام
لا بد من $\tau \geq 0$
منه لا يوجد $t = \tau$

unsteady state



ماذا لنا تربية ك تفرار ح
 مع ناصية بين مات مع ناصية
 كوتبول - 1



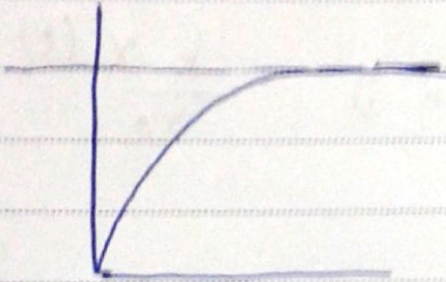
معلمة ال control

15-10-2017

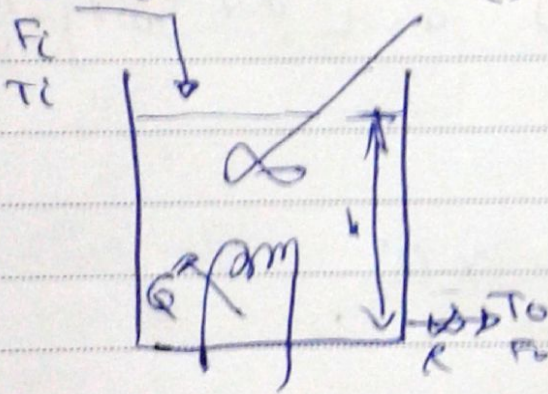
First order system →

$$G(s) = \frac{k}{\tau s + 1}$$

①



كيف نحسب ال k , τ , مع ناصية بين مات مع ناصية
 فية نوصي



$$AR \frac{dh}{dt} + h = R F_i$$

$$\frac{h(s)}{F_i(s)} = \frac{R}{ARs + 1}$$

دعوة لتمام دأف ؟ أدنى شبكة

Function 1, Transfer function

نجد ان ال $k=R$ و ال $AR=\tau$

2nd order system

(2)

System described by 2nd order diff equation

$$a_2 \frac{d^2 y(t)}{dt^2} + a_1 \frac{dy(t)}{dt} + a_0 y(t) = b x(t)$$

$$\frac{a_2}{a_0} \frac{d^2 y(t)}{dt^2} + \frac{a_1}{a_0} \frac{dy(t)}{dt} + y = \frac{b}{a_0} x(t)$$

$$\frac{a_2}{a_0} [s^2 y(s) + s y(0) + y(0)] + \frac{a_1}{a_0} [s y(s) + y(0)] + y(s) = \frac{b}{a_0} x(s)$$

$$y(s) \left[\frac{a_2}{a_0} s^2 + \frac{a_1}{a_0} s + 1 \right] = \frac{b}{a_0} x(s)$$

$$\frac{y(s)}{x(s)} = \frac{b/a_0}{\frac{a_2}{a_0} s^2 + \frac{a_1}{a_0} s + 1}$$

2nd order system
 transfer function

$$G(s) = \frac{y(s)}{x(s)} = \frac{K}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

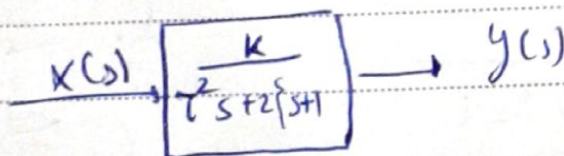
دالة النقل
 # دالة النقل

K = S.S gain

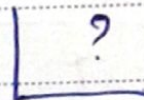
τ = time constant

ζ = Damping factor.

if I am interested final value \rightarrow use final value theorem.



اذا اردت تغير
K و τ
step



هل سي
change?

$$y(t)_{\infty} = \lim_{s \rightarrow 0} s Y(s)$$

$$= \lim_{s \rightarrow 0} s \left[\frac{K}{\tau^2 s^2 + 2\tau\zeta s + 1} \right] \frac{B}{s}$$

$$= KB$$

2nd order diff

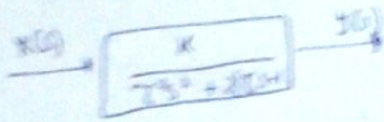
Tuesday 17/10/2012

$\zeta < 1$ oscillation [resonance not damp] \rightarrow underdamp 2nd order system.

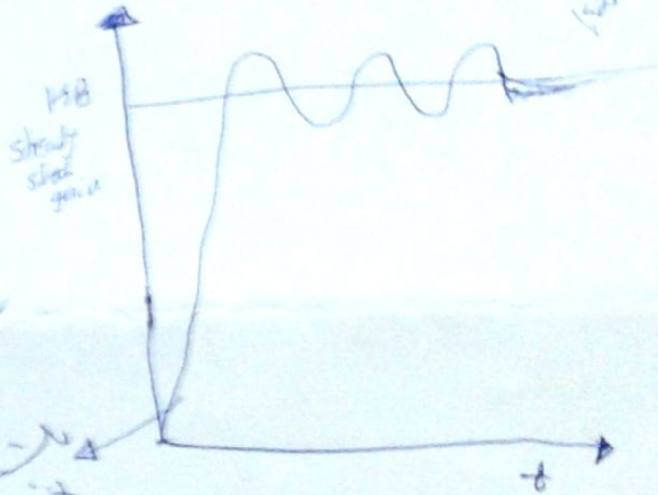
$\zeta = 1$ \rightarrow critically damp 2nd order system.

$\zeta > 1$ \rightarrow over damp 2nd order system.

high gain \rightarrow slow system \rightarrow rise time



step change \rightarrow show the response in 3 cases



Initial value of the change = zero

zero initial condition \rightarrow $y(0) = 0$

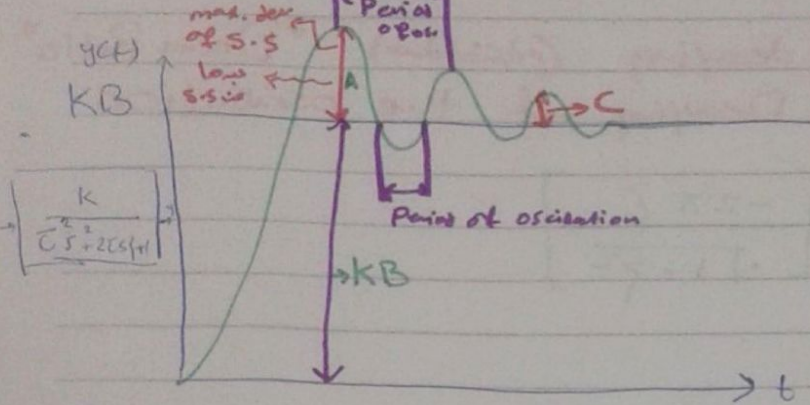
① \rightarrow initial value

\rightarrow final steady state

③ from final value theorem \rightarrow

$$\lim_{s \rightarrow 0} s Y(s) = \lim_{s \rightarrow 0} s \left[\frac{K}{s^2 + 2\zeta\omega_n s + \omega_n^2} \right] \left[\frac{s}{s} \right]$$

No: Thursday Date: 19th/10/2017



characteristic of Oscillatory Response!

1. Period of oscillation (A)
2. A (maximum deviation of steady state)
3. we take incrementation the value of A with respect to S.S value (KB)

$0 < \zeta < 1$ underdamped

* K, τ, ζ , characteristic of the 2nd order system "Response"

4. $\frac{A}{KB}$: overshoot,

* B is not a parameter, it's input change.

As a fraction or as a percent!
5. overshoot = $\exp\left(\frac{-\pi\zeta}{\sqrt{1-\zeta^2}}\right)$

* $O.S = f_n(K, \tau, \zeta) \Rightarrow$ parameter Represent the Oscillation Response.
 \hookrightarrow have to be known to identify the system

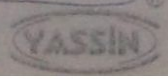
* ~~transient~~ (Transient State) place ζ and τ as transfer 1. 2nd order system
* K is determine the behavior of S.S state behaviour only

* $y(t) = KB \left[1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta t} \sin \frac{\sqrt{1-\zeta^2}}{\zeta} t \right]$ \hookrightarrow plz check it

\hookrightarrow solve this eqn we get \underline{t}
 t_{rise} (time)
i.e. rise time

* How can we cancel τ and K ? \Rightarrow V-I MP

* maximum overshoot when $\zeta = 0 \Rightarrow \frac{A}{B} = 1$



No.

Date.

* $\frac{C}{A}$: The Rate of decaying (oscillation) "Decay Ratio"
 * Rate of Decaying at the oscillation

$$* D.R \Rightarrow \frac{C}{A} = \exp \left[\frac{-2\pi}{\sqrt{1-\zeta^2}} \right]$$

$$* \rho = \frac{2\pi\zeta}{\sqrt{1-\zeta^2}}$$

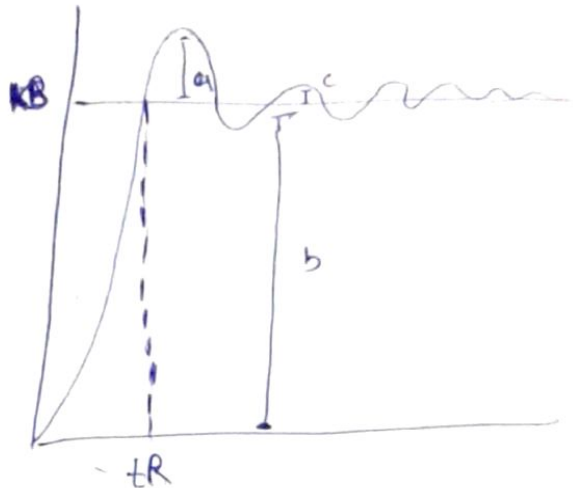
2nd order system →

underdamping

$$O.S = \exp\left(\frac{-\pi \zeta}{\sqrt{1-\zeta^2}}\right)$$

$$D.R = \exp\left(\frac{-2\pi \zeta}{\sqrt{1-\zeta^2}}\right)$$

$$\rho = \frac{2\pi \tau}{\sqrt{1-\zeta^2}}$$



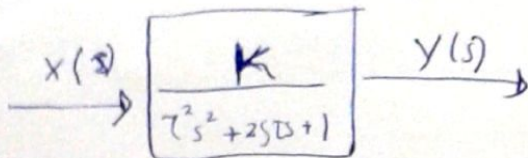
$$\frac{a}{b} = \text{over shoot}$$

Stable time, ζ and ρ
integral of response ①

ماذا نقول في Decay Ratio ؟
فقدان الاختلاف في التذبذب

مهندس في الرياضيات
designer في critical case

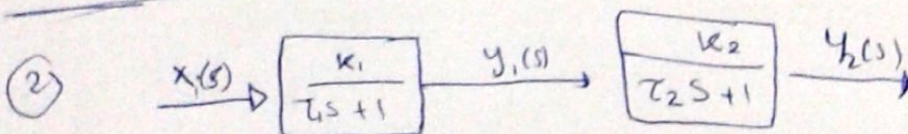
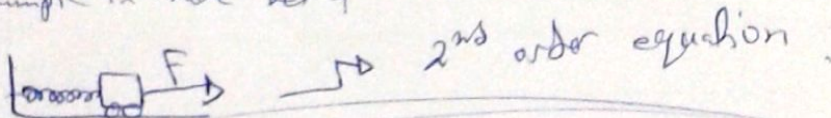
How 2nd order can exist?



physics of a system are description in 2nd order system.

order 2nd في الرياضيات

example in more detail



$$\frac{Y_1(s)}{X_1(s)} = \frac{K_1}{T_1 s + 1}$$

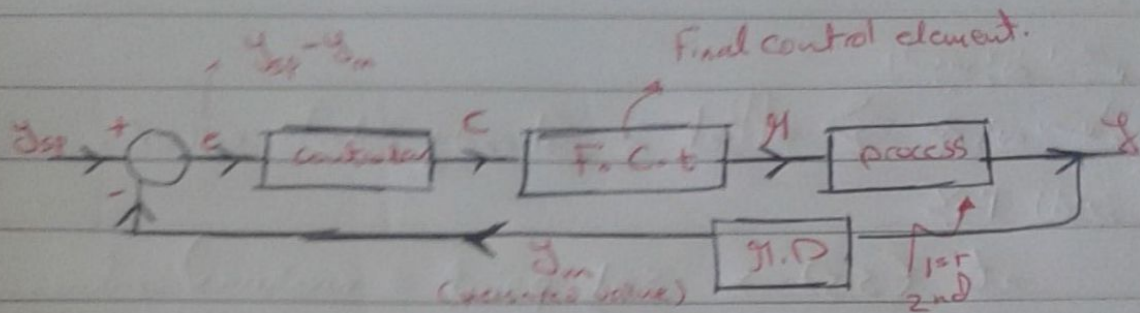
$$\frac{Y_2(s)}{Y_1(s)} = \frac{K_2}{T_2 s + 1}$$

$$\frac{Y_2}{Y_1} = \frac{K_1 K_2}{(T_1 s + 1)(T_2 s + 1)}$$

$$\frac{Y_2(s)}{X_1(s)} = \frac{K_1 K_2}{T_1 T_2 s^2 + (T_1 T_2)s + 1}$$

24/04/2017

Tues.



* Controllers

1- Proportional controller

controller in which the output proportional directly with input.

constant (controller gain) \rightarrow $\bar{e}(s) = \frac{1}{s} \sin \omega t$ controller's input
 $C(t) = K_c e(t) + \bar{e}$ input \rightarrow $\bar{e}(s) = \frac{1}{s} \sin \omega t$ output \rightarrow
 $C(s) = -K_c e - \bar{e}$ controller signal (output) at steady state.

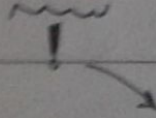
$$\dot{C}(t) = K_c e'(t) \xrightarrow{\text{Laplace}} C(s) = K_c e(s)$$

so $G(ss) = \frac{C(s)}{e(s)} = K_c$ constant #

transfer
function
gain

(input * error = output)

Simple & Fast & Cheap.

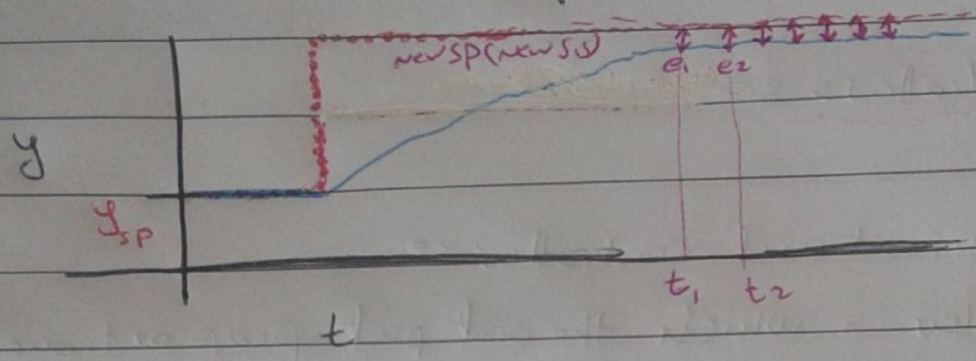


→ البسالة لشيء

مع دالة سطر جديد \Rightarrow offset : Steady State error

كأن لا نصل إليه

at (s.s) \rightarrow set point = measured value (SP)



$$e_1 = e_2$$

$$C_1 = K_c \times e_1$$

$$C_2 = K_c \times e_2$$

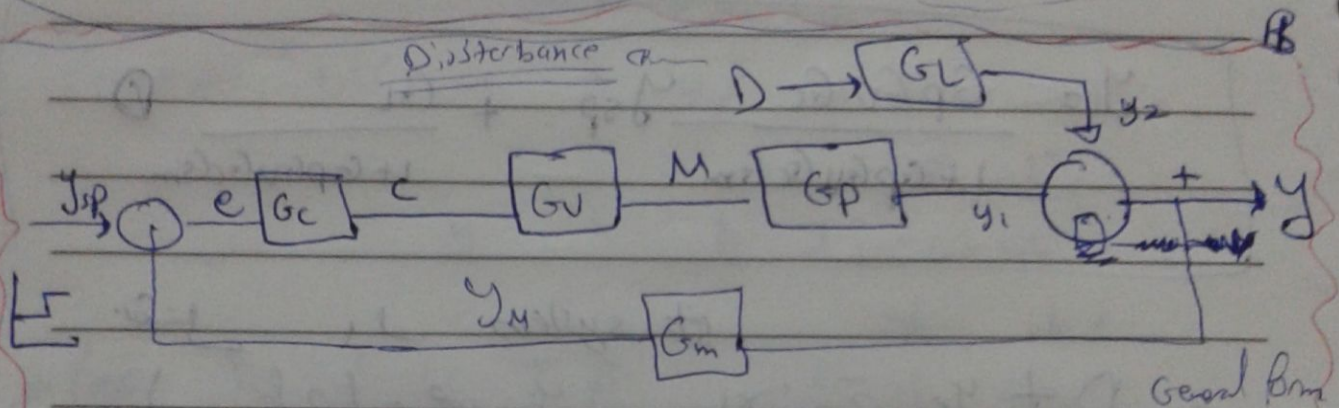
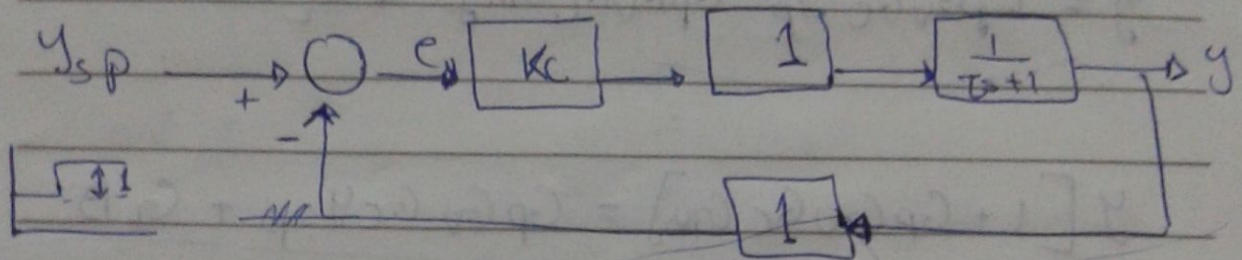
\rightarrow Disadvantage \Rightarrow the controller stuck when $e_1 = e_2$

ملاحظة why?

دالة error \rightarrow البسالة لشيء

→ proportional controller →

$$G_c(s) = K_c$$



* only source for a change to system -
 come from D or y set point →

$$y_{ps} \propto y \text{ if } D \text{ and } y \text{ are constant}$$

for each system we will see external change
 effect it ~ This Disturbance

$$y = y_1 + y_2$$

$$y = G_p M + G_L D$$

$$y = G_p G_v \times C + G_L D$$

$$= G_p G_v G_c e + G_L D$$

$$y = G_p G_v G_c [y_{sp} - y_m] + G_L \times D$$

$$y = G_p G_v G_c y_{sp} - G_p G_v G_c G_m y + G_L \times D$$

$$y [1 + G_p G_v G_c G_m] = G_p G_v G_c y_{sp} + G_L D$$

$$y = \frac{G_p G_v G_c}{1 + G_p G_v G_c G_m} y_{sp} + \frac{G_L}{1 + G_p G_v G_c G_m} D$$

system is a single input

output is a single output

single input single output

Single input single output

SISO ✓

- SINO

- MISO

- MIMO

single input single output

input is a single input

its system characteristic

$$1 + G_p G_v G_c G_m = 0 \quad \text{Characteristic equation}$$

نہیں کہہ سکتے ہیں کہ اس کا نقل (قدار) 1 ہے
 2. براہ راست (transfer function) موجود نہیں ہے، system

not 2

The close loop Transfer function

• اس کے بارے میں یہ کہنا کہ یہ کد کا ہے
 یہ کہہ سکتے ہیں

• اس کے بارے میں یہ کہنا کہ یہ کد کا ہے
 یہ کہہ سکتے ہیں

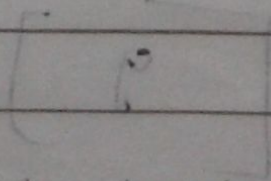
• (مقامی کد) T.F مشترکین ہاں Loop #

• اس کے بارے میں یہ کہنا کہ یہ کد کا ہے (multi class loop) جواب نہیں ہے، Loop

• اس کے بارے میں یہ کہنا کہ یہ کد کا ہے

• سوالیہ علامت

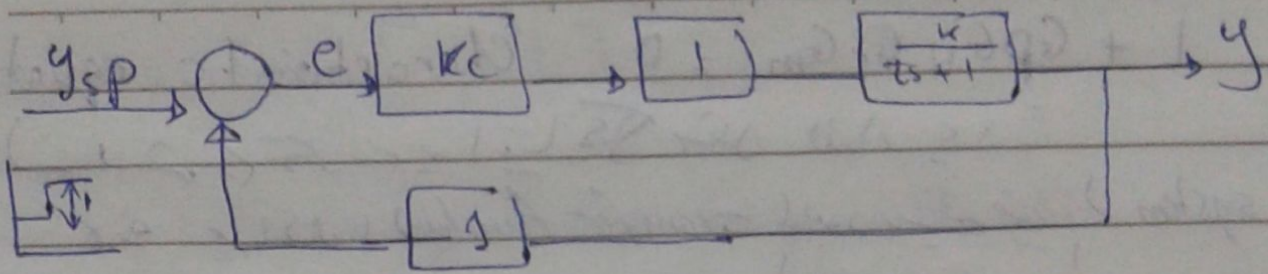
• اس کے بارے میں یہ کہنا کہ یہ کد کا ہے General (معمولی) ہے



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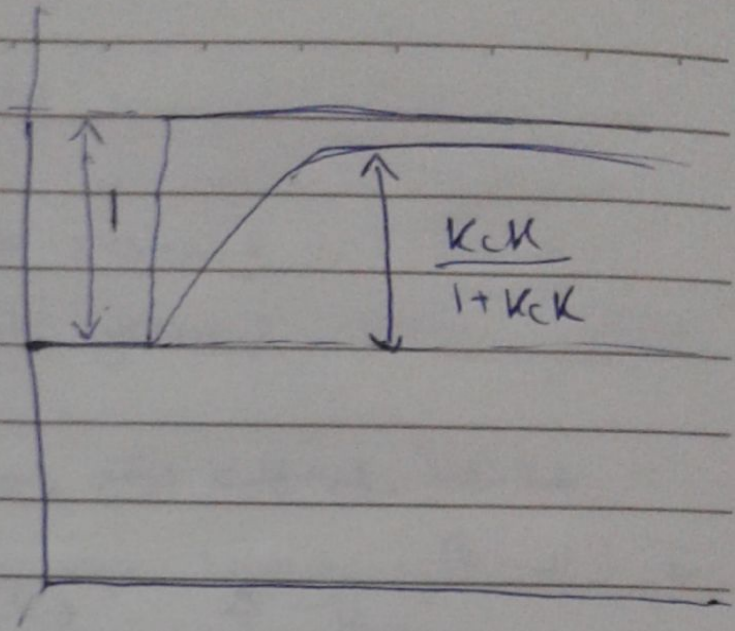
$$y = \frac{Kc \left[\frac{K}{Ts+1} \right] \left(\frac{1}{s} \right)}{1 + Kc \cdot 1 \cdot \frac{K}{Ts+1}}$$

$$y = \frac{Kc K}{Ts+1} \cdot \frac{1}{s} \cdot \frac{1}{1 + Kc K \frac{1}{Ts+1}}$$

$$y = \frac{Kc K}{Ts+1} \cdot \frac{1}{s} \cdot \frac{Ts+1}{Ts+1 + Kc K}$$

$$y = \frac{Kc K}{1 + Kc K} \cdot \frac{1}{s}$$

$$y(t) = \lim_{s \rightarrow 0} s \left[y \right] = \frac{Kc K}{1 + Kc K}$$



و رافع این

$$\frac{K_c K}{1 + K_c K} < 1$$

یعنی هر چه تا به حد
بیشتر شود

$$\text{offset} = \text{New setpoint} - y(t)_{\infty}$$

$$\text{offset} = 1 - \frac{K_c K}{1 + K_c K}$$

$$= \frac{1}{1 + K_c K}$$

* increasing prop to the controller $\frac{K_c}{\text{gain}}$ یعنی K_c را زیاد کنیم

offset را کمتر می‌کند

و این باعث می‌شود که سیستم دقیق‌تر باشد

اما اگر K_c خیلی بزرگ شود، سیستم ناپایدار می‌شود

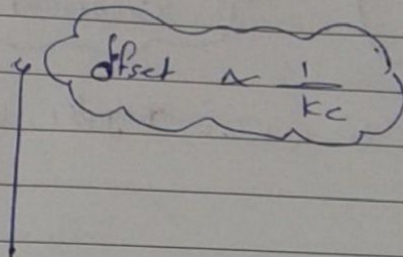
instability system

Controller.

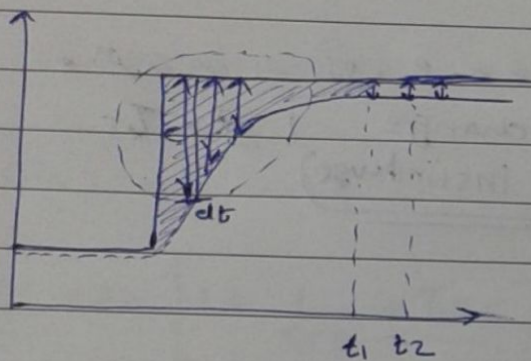
$$G_c(s) = K_c$$

→ Fast
Simp.
Cheap

→ offset



* We can't eliminate offset by $\uparrow K_c$ because $\uparrow K_c$ cause to unstable system.



error is the area under (history) of error

get it like this

integrate the error signal (Integration) is used to get rid of offset

$$C(t) = K_c e(t) + \frac{K_c}{T_I} \int_0^t e(t) dt$$

output of controller is the sum of proportional and integral action

output of controller remain constant

laplace transform is used to get rid of offset (transform)

$$C(s) = K_c e(s) + \frac{K_c}{T_I} \left[\frac{1}{s} e(s) \right]$$

$$C(s) = K_c \left[1 + \frac{1}{T_I s} \right] e(s)$$

$$G(s) = \frac{C(s)}{E(s)} = K_c \left[1 + \frac{1}{T_i s} \right]$$

$$G(s) = K_c \left[\frac{T_i s + 1}{T_i s} \right]$$

Proportional Integral Controller (PI)

error \rightarrow Integrals \rightarrow offset \rightarrow error \rightarrow offset

T_i, K_c Two parameters

PI is dynamic, \rightarrow P, PI, \rightarrow dynamic

Dynamic

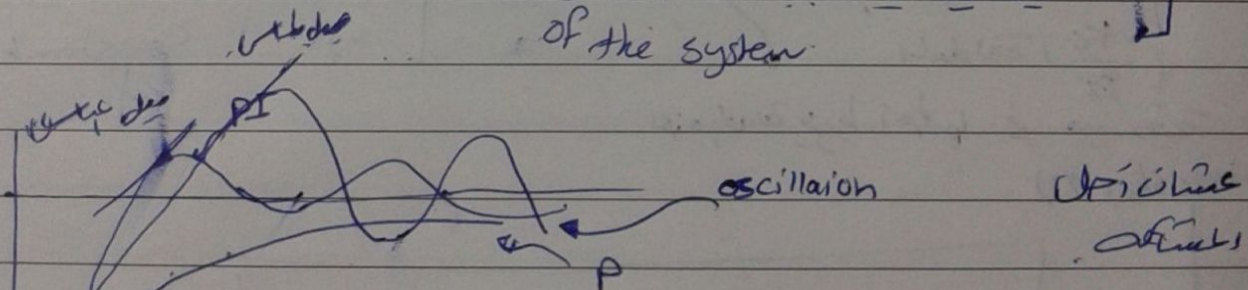
(the change is instantaneous)

change \rightarrow input \rightarrow output

(Slower) \rightarrow system \rightarrow slower

2nd order \rightarrow 1st order \rightarrow 2nd order \rightarrow 1st order

Oscillation of the system



Oscillation in the system

Rate of change of the error

$$C(t) = K_c e(t) + \frac{K_c}{T_I} \int_0^t e(t) dt + K_c T_D \frac{d e(t)}{dt}$$

PID

[Proportional integral Derivative Controller] → increase in time (oscillation)
 (Three Parameter)

$$K_c, T_D, \frac{K_c}{T_I}$$

Laplace transform.

$$C(s) = K_c e(s) + K_c \left[1 + \frac{1}{T_I s} \right] + K_c T_D s e(s)$$

$$\frac{C(s)}{e(s)} = K_c \left[1 + \frac{1}{T_I s} + T_D s \right]$$

↑
 3 parameter modification

$$\frac{C(s)}{e(s)} = K_c \left[\frac{T_I T_D s^2 + T_I s + 1}{T_I s} \right] * \left[\frac{1}{s+1} \right]$$

3 Parameter.
 slower

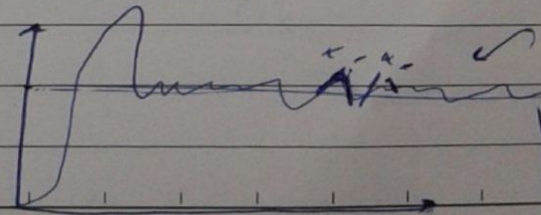
(Ideal PID) is not physically realizable.

physically un-realizable.
 [Ideal PID]

why the system is physically un-realizable?

Dynamic out is input

$$\frac{Y(s)}{X(s)} = \frac{Q(s)}{P(s)}$$



all high oscillation
 sensitive of high

Practical

sensitive for high frequency noise

Subject

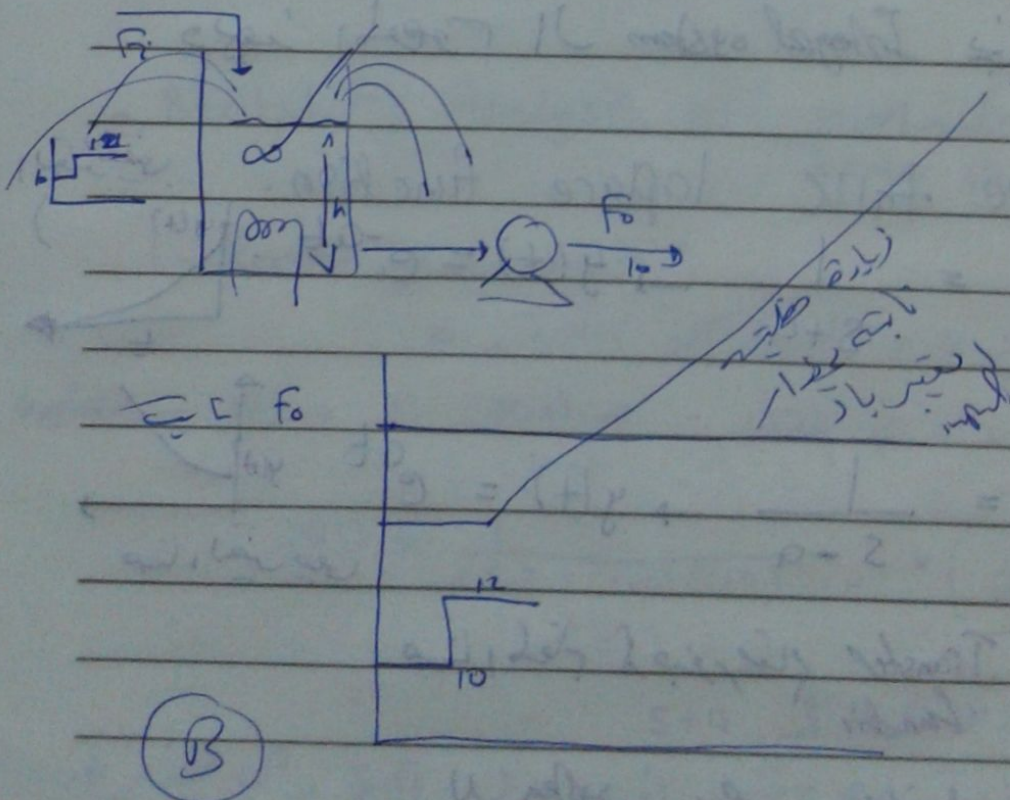
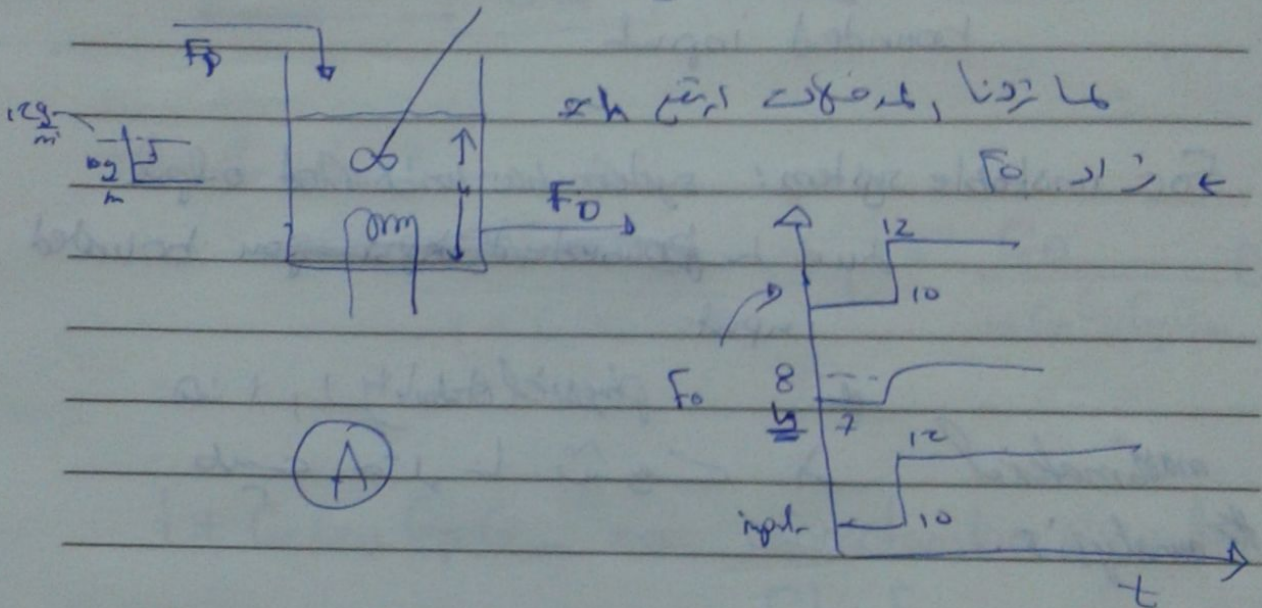
Day Thursday

Date 2-11-2017

process stability :-

what is a stable system?

what is unstable system?



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stable (A) $\bar{a} < 0$, $a < 0$ #
unstable B.

The stable system has a bounded output due to bounded input

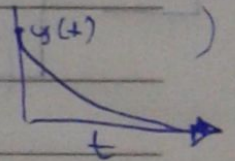
For unstable system: system has unbounded output due to ~~bounded input~~ bounded input

physical stability, in mathematically analysis.

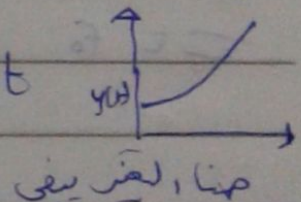
unstable $\bar{a} > 0$ Integral system

if we talk Laplace function.

$$y(s) = \frac{1}{s+a} \rightarrow y(t) = e^{-at}$$



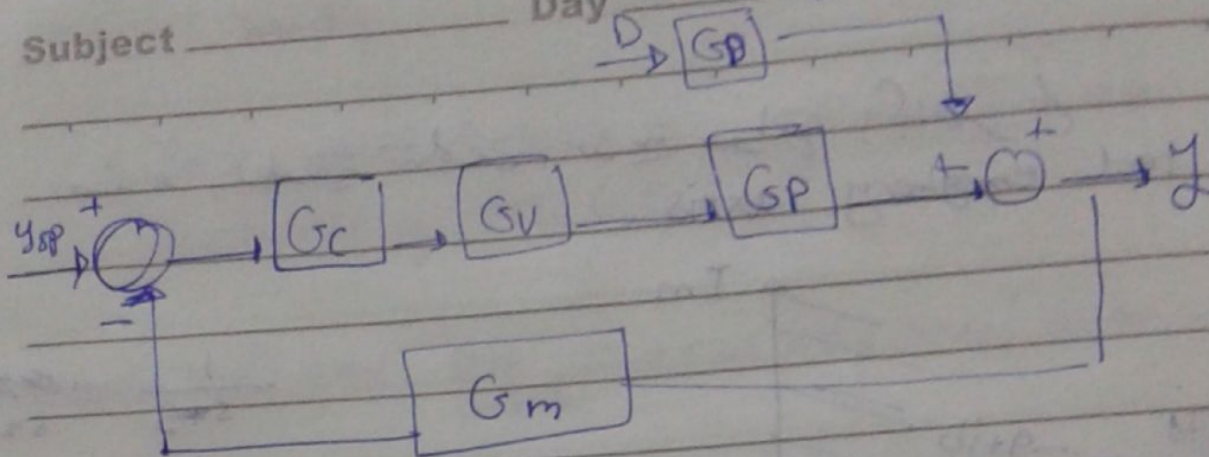
$$y(s) = \frac{1}{s-a} \rightarrow y(t) = e^{at}$$



behavior, Transfer function

characteristic eq, system equation

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Transfer function →

$$y(s) = \frac{G_c G_v G_p}{1 + G_c G_v G_p G_m} y_{s.p} + \frac{G_D}{1 + G_c G_v G_p G_m} D$$

$1 + G_c G_v G_p G_m = 0$ characteristic equation.
Ch. E.

• Stability Analysis is mathematical analysis to describe stability.

1- Root locus method

unstable system if positive root

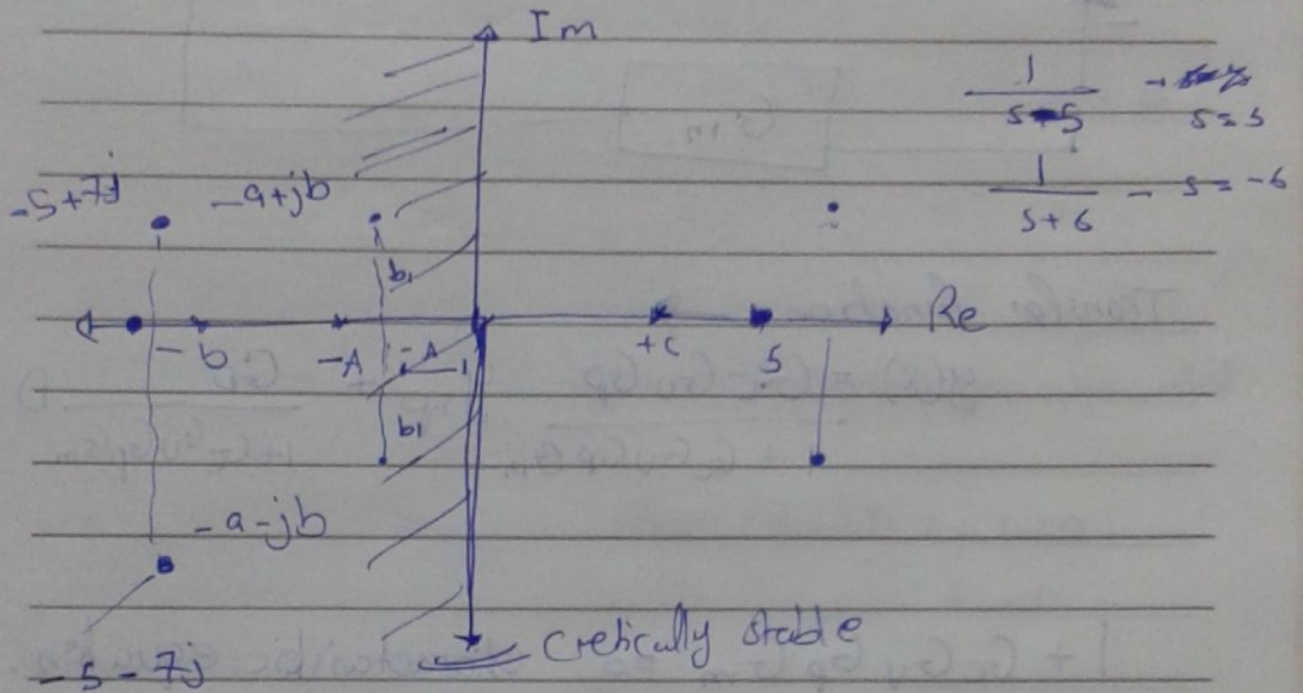
$$y(s) = \frac{1}{(s-a)(s+a)(s+a)} = \left(\frac{1}{s-a} + \frac{1}{s+a} + \frac{1}{s+a} \right)$$

$s+a$ is LBP (Left Half Plane)

$s-a$ is RHP (Right Half Plane)

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to real (imaginary axis), s is real emergency axis.



if it $-5 \pm 7j$

• if all the roots ^{are} to the left of the emergency axis the system is stable.

if one root to the right.

The system is unstable

according to root locus method #

if at emergency \rightarrow critically stable

#

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Test II :- From The R-H Array :-

Column 1	2	3
a_0	a_2	a_4
a_1	a_3	a_5
$A_1 =$	A_2	A_3
B_1	B_2	B_3
$a_0 s^n + a_1 s^{n-1} + a_2 s^{n-2} + \dots + a_n s^0$		
C_1	C_2	C_3
\emptyset	\emptyset	0
	0	
0		

$$A_1 = \frac{a_0 a_2 - a_1 a_1}{a_1}$$

$$A_2 = \frac{a_1 a_4 - a_0 a_5}{a_1}$$

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For stable system all elements in column 1 should be positive. (+ve)

example

$$10s^3 + 17s^2 + 8s + 1 + K_c = 0$$

لپ سے بڑھانے کے لیے

10	8	0
17	$1 + K_c$	0
$\frac{17+8-10(1+K_c)}{17}$	0	0
$\frac{17+8-10(1+K_c)}{17} \div (1+K_c)$		
$\frac{17+8-10(1+K_c)}{17}$		

* For stable system $\frac{17+8-10(K_c+1)}{17} > 0$

div

$$(1 + K_c) > 0$$

$$10(1 + K_c) < 17 + 8$$

$$1 + K_c < \frac{17+8}{10} \rightarrow K_c < \frac{17+8-1}{10}$$

$$K_c > -1$$

$$K_c < 12.6$$

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Range of

K_c

Range of K_c for stability

$$-1 < K_c < 12.4$$

system have not

instability

steady state

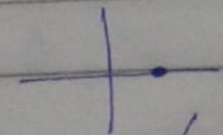
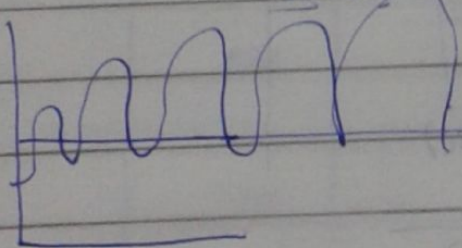
response

oscillation

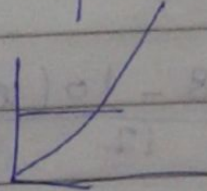
oscillation response

complex response

instability



instability



response

$$1 - G + F > 0$$

$$1 - G + F > 0$$

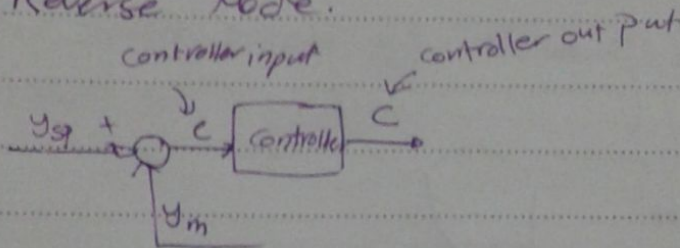
* Controllers :-

Types : P, PI, PID.

Controller Mode

1) Direct Mode

2) Reverse Mode.



Direct mode :

If The output of controller (C) increases when the measured value of controlled variable (ym) increases, then the controller is in Direct Mode.

Reverse mode :

if the output decreases when the measured value increases, then the controller is in

Reverse mode

(Direct)

$$C = k_c \times e$$

$$C = k_c \times [y_{sp} - y_m]$$

هنا y_m زيادة e سوف C تزداد
وهذا هو $Direct$

k_c هو $Gain$ من C الى e

Reverse

$$C = K_c [y_{sp} - y_m]$$

$K_c > 0$

عند زيادة C تقل y_m وبتالي

$K_c > 0$ عكس

**** why Direct & Reverse ??**

To have synchronization between the controller & the valve.

Types of Valves:

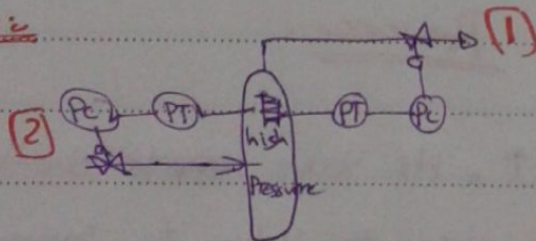
→ Response of valve to the signal of the Controller

→ Air-to-open [Fail close]

→ Air-to-close [Fail open]

هذا النوع من الصمامات يتجه signal إلى الصمام

Ex:



(1) if the pressure increase \Rightarrow so the valve must close. $[C \downarrow] \Rightarrow$ so the type is [Fail open]

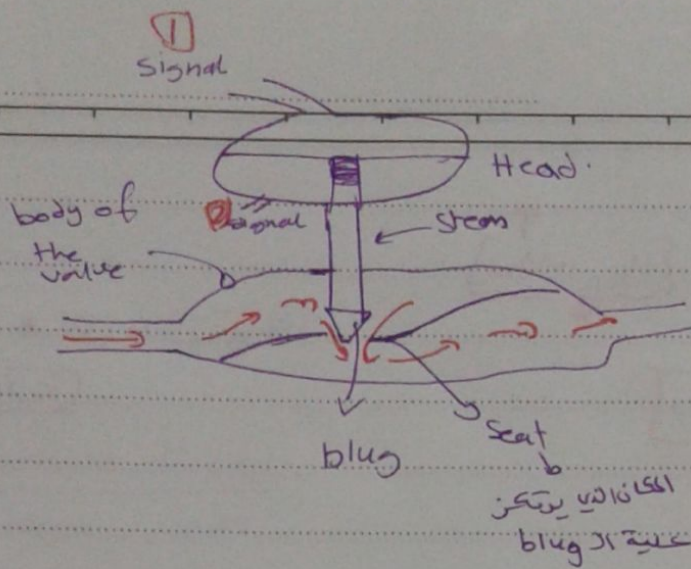
عند زيادة الضغط يجب أن يغلق الصمام

(2) if the pressure increase \Rightarrow so the flow must decrease.

so the valve must close $[- \Rightarrow$ Fail close]

عند زيادة الضغط يجب أن يغلق الصمام

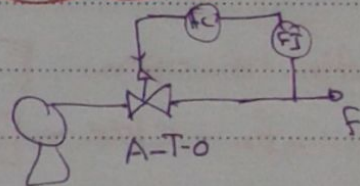
Subject :



(1) signal \uparrow , the valve will closed.
[Fail open]

(2) signal \uparrow , the valve will open
[Fail close]

أولاً أنا اختار ال Valve
ثم اكتب ال Controller
الذي يتوافق معه



→ the type of controller is
Reverse

⇒ $F \uparrow$, the Valve should close

→ to close the Valve to signal must

decrease. ($C \downarrow$)

Reverse.

► Subject :

Controllers:-

P, PI, PID

Controller mode

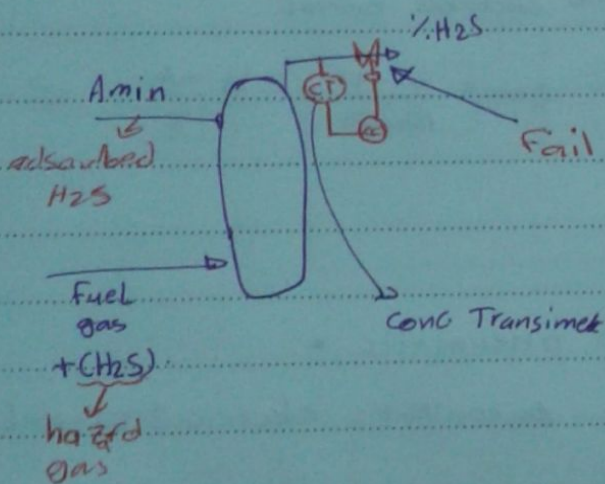
Direct ($K_c < 0$)

Reverse ($K_c > 0$)

Controller valves

A-T-O (Fail ^{close} ~~open~~)

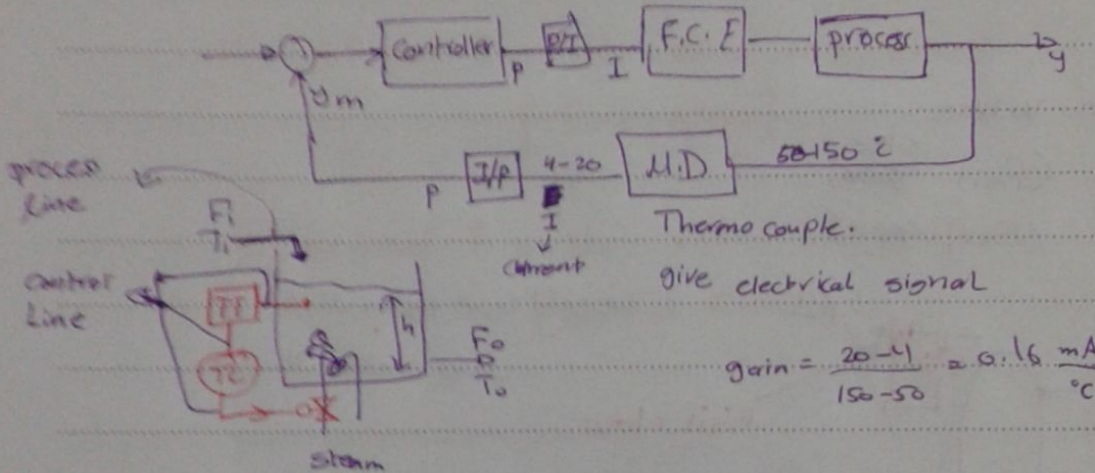
AT-C (Fail open)



Control signal

Types of control signal :-

- 1) Electric 4-20 mA no standard
- 2) pneumatic [work with compressed air] 3-15 psi
or Compressed Fluid



$$\text{gain} = \frac{20-4}{150-50} = 0.16 \frac{\text{mA}}{^\circ\text{C}}$$

* If my controller is pneumatic.

I must buy a device to convert electrical signal to pneumatic.

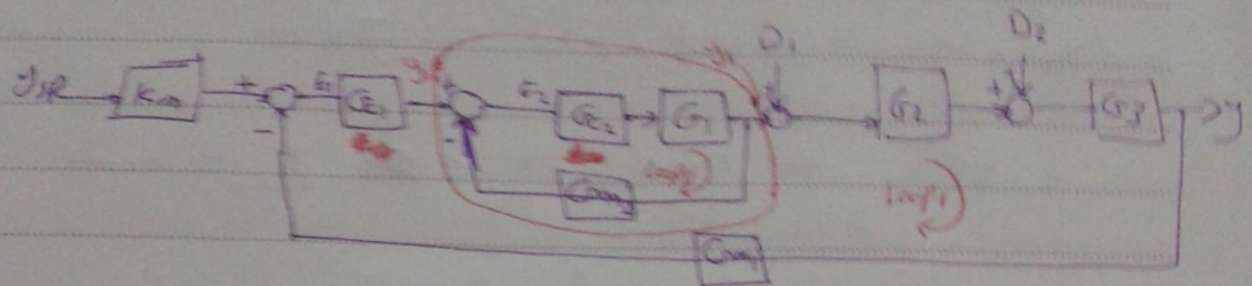
* what is the gain of I/P converter.

$$\text{Gain}_{I/P} = \frac{\Delta \text{out Put}}{\Delta \text{input}} = \frac{15-3}{20-4} = \frac{12}{16}$$

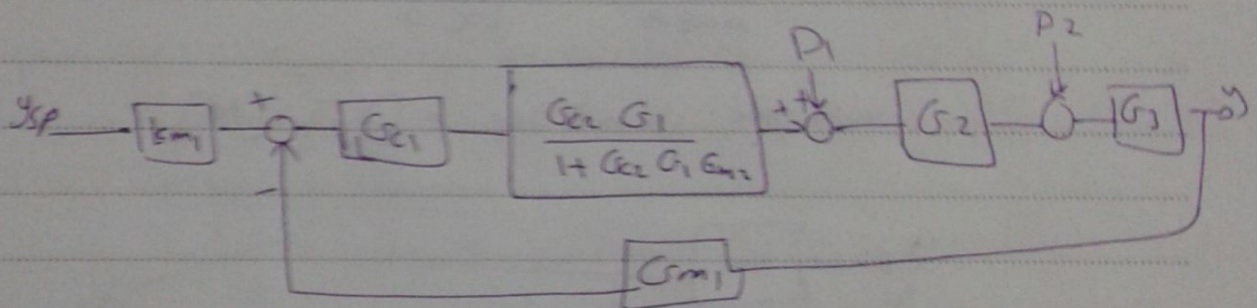
$$\text{Gain}_{P/I} = \frac{16}{12}$$

Subject:

Ex:



$$y_1 = \frac{G_{c2} G_1}{1 + G_{c2} G_1 G_{m2}} y_{sp1} \quad \leftarrow \text{Loop 2}$$



$$y = \frac{K_{m1} G_{c1} \left[\frac{G_{c2} G_1}{1 + G_{c2} G_1 G_{m2}} \right] G_2 G_3}{1 + G_{c1} \left[\frac{G_{c2} G_1}{1 + G_{c2} G_1 G_{m2}} \right] G_2 G_3 G_{m1}} y_{sp}$$

$$\text{Ch.E} = 1 + G_{c1} \left[\frac{G_{c2} G_1}{1 + G_{c2} G_1 G_{m2}} \right] G_2 G_3 G_{m1} = 0$$

S T A R S N O T E B O O K

why k_m ??

ما يصير عند توافق الحرارة بين y و y_{sp}

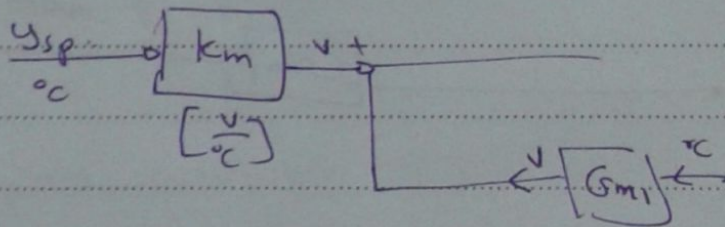
if $y \equiv T$ the thermo couple \Rightarrow ~~the~~ \neq voltage

\Rightarrow the signal out from $G_m \equiv V$

and y_{sp} in $^{\circ}C$

$$k_m \equiv \frac{\Delta \text{out put}}{\Delta \text{input}} \equiv \left[\frac{V}{^{\circ}C} \right]$$

when multiple $k_m \cdot y_{sp} \equiv \left[\frac{V}{^{\circ}C} \right] [^{\circ}C]$



* Design of control systems-

- Control configuration [feed ~~back~~ ^{forward}, feed forward]

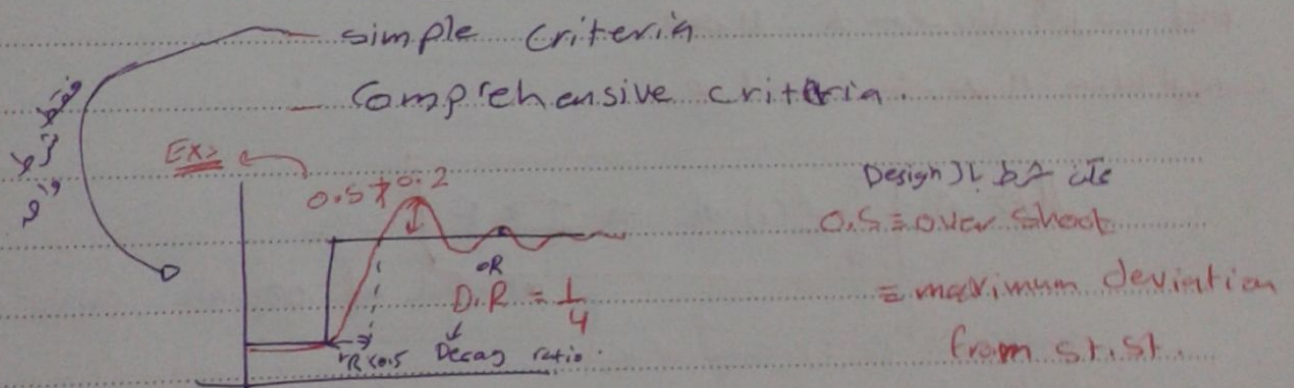
- controller types [P, PI, PID]

- stability

- Direct & Reverse \rightarrow A-T-O, A-T-C

\Rightarrow Controller Tuning - specify the values of control parameters [K_c , T_f , T_D]

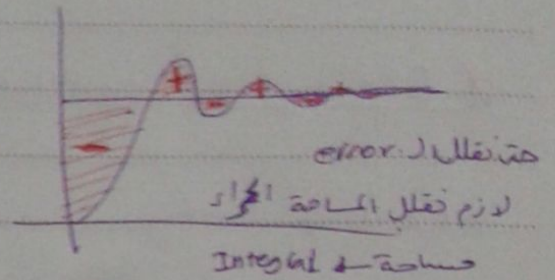
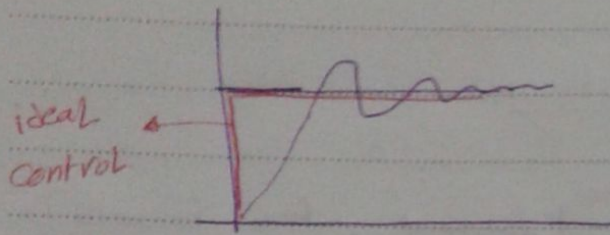
Tuning Criteria



if \Rightarrow controller \Rightarrow with minimum O.S. & min. t_r

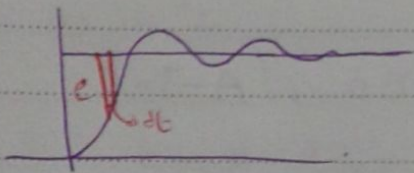
\Rightarrow no why since O.S. & t_r \Rightarrow ~~are~~ ^{are} ~~very~~ ^{very}

\rightarrow Go to comprehensive.



Comprehensive \Rightarrow look at the response of a hole.

1) Integral Method.



$$A = \int_0^{\infty} e(t) dt$$

هنا A سوف نطبع أقل من

هذا سوف يؤثر على action التحكم

$$A = \int_0^{\infty} e^2(t) dt = ISE$$

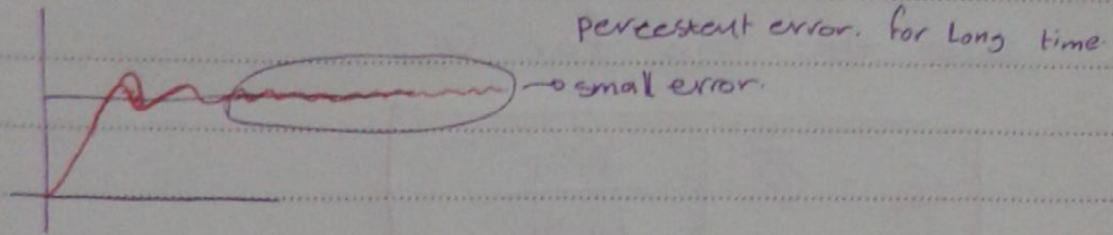
integral of square error.

لا يستخدم في طالع 1) fraction

\hookrightarrow there is a problem here if $e(t) < 1$

$$IAE = \int_0^{\infty} |e(t)| dt$$

Subject :

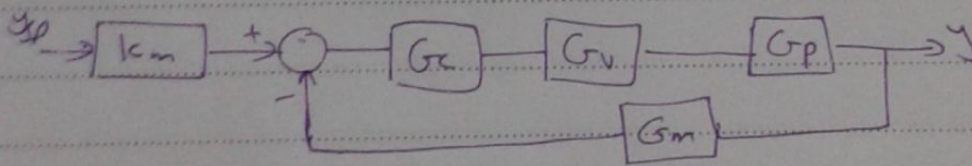


الطريقتان السابقتان لا يستطيعان حلها

$$ITAE = \int_0^{\infty} t |e(t)| dt$$

عندما كان t كبيراً كان e صغيراً
عندما كان e صغيراً كان t كبيراً
حتى يطغى عندئذٍ الـ Area الكبيرة
الـ Controller المستقلة

2) Direct synthesis method:



$$\frac{y}{y_{sp}} = \frac{k_m G_c G_v G_p}{1 + G_c G_v G_p G_m} = \frac{G_c G}{1 + G_c G}$$

Assume $G_m = k_m$

let $G = G_m G_v G_p$

► Subject :

Solve the eqn. for G_c .

$$G_c = \frac{1}{G} \left[\frac{y y_{sp}}{1 - y/y_{sp}} \right]$$

عند معرفة $\frac{y}{y_{sp}}$ قلنا نجد G_c

if $\frac{y}{y_{sp}} = 1$ perfect control ————

$$\rightarrow G_c = \infty$$

no feasible
to do perfect
control.

is there another
definition of
perfect controller.

Direct synthesis method (DSM)

$$G_c = \frac{1}{G} \left[\frac{y/ds.p}{1 - y/ds.p} \right], \quad (y/ds.p) \text{ is } (y/ds.p)$$

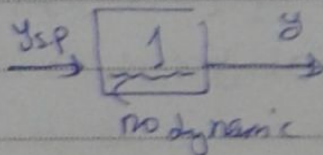
performance criteria $\frac{y}{y_{sp}}$

perfect control $\frac{y}{y_{sp}} = 1$, G_c is not feasible.

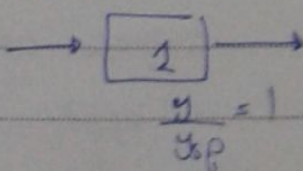
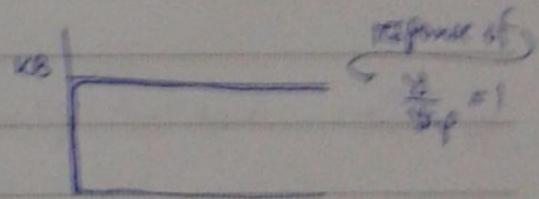
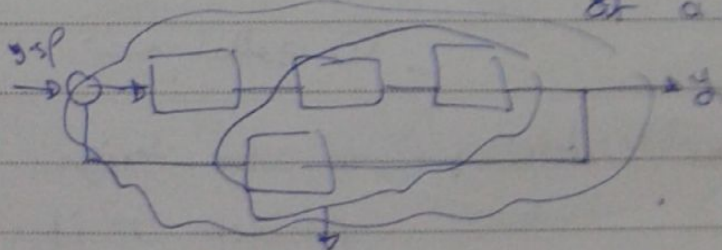
1. $\frac{y}{y_{sp}} = 1$ is the first order system.

* what does $\frac{y}{y_{sp}} = 1$ meaning?

system is zero order. Over all dynamics of a system



We are considering this system at a zero order.



system is have instantaneous response.

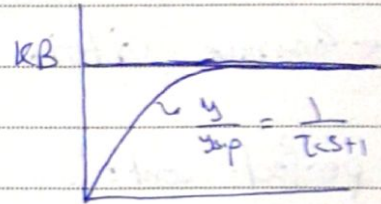
if response of zero order is not response \rightarrow The next step \rightarrow possible is a 1st order system.

$$\frac{y}{y_{s.p}} = \frac{1}{\tau_s s + 1}$$

این سیستم یک سیستم یکپارچه اول است.
یعنی (یک پله) و (یک زمان تاخیر) $\tau_s + 1$

لا اکتفا به این فرم کلی
لا میسر می آید زیرا به ترتیب

response of $\frac{1}{\tau_s s + 1}$



$$G_c = \frac{1}{G} \left[\frac{\frac{1}{\tau_s s + 1}}{1 - \frac{1}{\tau_s s + 1}} \right] = \frac{1}{G} \left[\frac{\frac{1}{\tau_s s + 1}}{\frac{\tau_s s + 1 - 1}{\tau_s s + 1}} \right]$$

$$G_c = \frac{1}{G} * \frac{1}{\tau_s s}$$

این یک کنترلر انتگرال است.
Controller.

فرض ما طراحی PI یا PID Controller است. اما طبقه بندی اینها
در صورت نیاز کنترل performance و انتخاب
Criteria.

① به کمک این

The choice of performance criteria → ② to solve design problem if it appear after apply eq.

example about design problem →

$$\text{assume } G = \frac{1.6 (s - 0.5)}{s + 2}$$

$$G = G_p G_o G_m$$

use The DSM To design a ^[PI] controller using
a performance criteria $\frac{y}{y_{sp}} = \frac{1}{T_s + 1}$

$$G_c = \frac{s + 2}{1.6 (s - 0.5)} \times \frac{1}{T_s + 1}$$

$$G_c = \frac{s + 2}{1.6 T_{cs} (s - 0.5)}$$

معاملات PI controller
(مثلاً $\frac{1}{T_s + 1}$ مع
المعاملات $\frac{1}{T_s + 1}$)
المعاملات $\frac{1}{T_s + 1}$

$$G_c = K_c \left[1 + \frac{1}{T_{cs}} \right]$$

المعاملات $\frac{1}{T_s + 1}$
positive root
unstable controller

controller is not stable

!! unstable controller

process is not stable

→ The performance criteria you required can not give stable controller for this process.

الآن بتغير الـ criteria

$$\frac{y}{y_{sp}} = \frac{(s - 0.5)}{T_s + 1}$$

معاملات PI controller

* End chapter 11

Controller Design.

[simple criteria

comprehensive

[integral methods.

DSM.

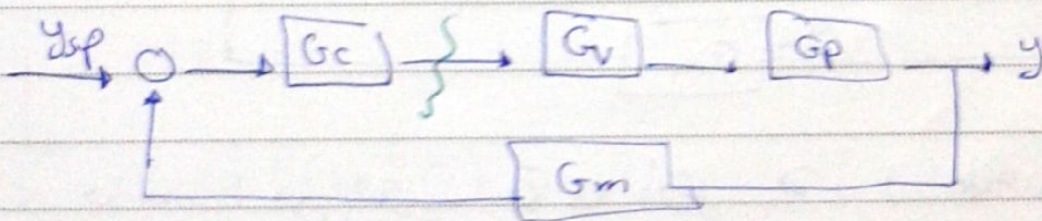
Empirical method :

+ equation or formula from alot of experiment + Analysis.

→ at the end give the formula to calculate control parameter.

1- Cohen coon method.

* open loop based method.



Open loop tell us that →

1. introduce a step change input to the process.

2. approximate the response as a first order plus time delay.

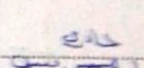
3. Find the K, τ, θ of the process

↑ loop ال step 1 ال input daye ال كيف ال response ال
 ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال
 ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال
 ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال
 ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال ال

TC

at Via gele 6002 Newswing Corp Inc
Jewia

10



بقدره ما في ركنه من اهل البيت (عليه السلام) في ركنه من اهل البيت (عليه السلام)

ian the

5

10

—

—

• sk2

5

100
50
Change

equation of 1st order with time delay

$$G = \frac{K e^{-\theta s}}{\tau s + 1}$$

time delay

time domain —————
 very small step change —————
 small

time domain —————
 K, τ

صاف امین، بجزد، اعلا —————
 رابط العقل وحی و صفا و صفا

after find K, τ, θ

تاریخ
تاریخ
تاریخ

PID

$$K_c = f(K, \tau, \theta)$$

$$\tau_I = f_i(K, \tau, \theta)$$

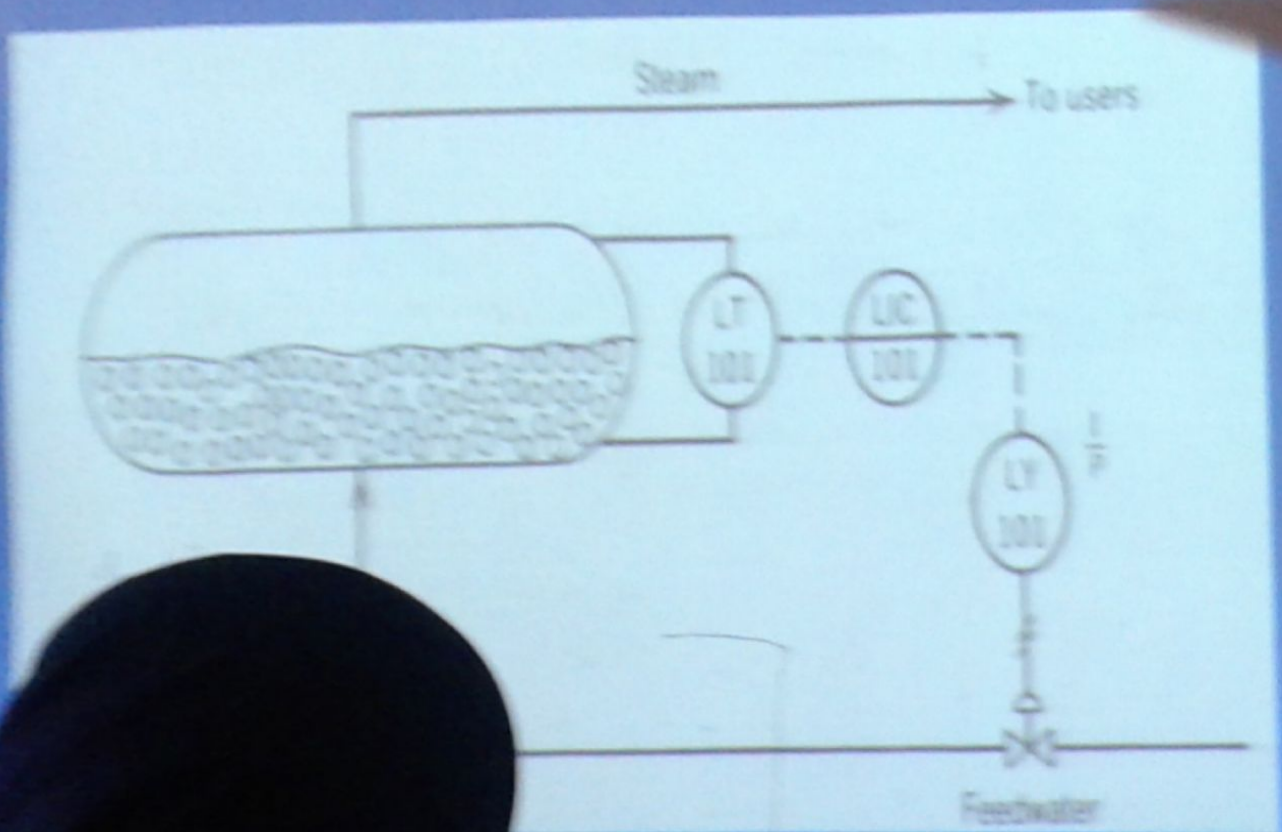
$$\tau_D = f_D(K, \tau, \theta)$$

K_c, τ_I, τ_D —————
 معینه

تا زار از راد سے لازم (تاریخ) نقل

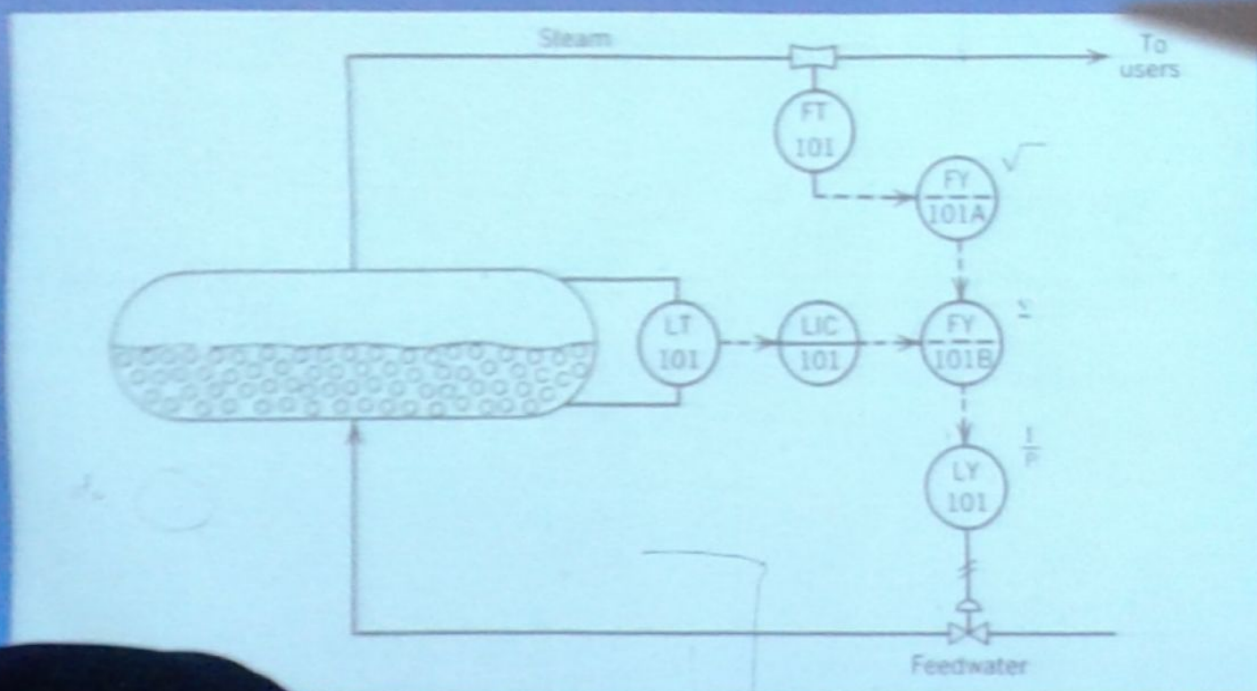
Boiler Drum Control

"Single-element control" scheme

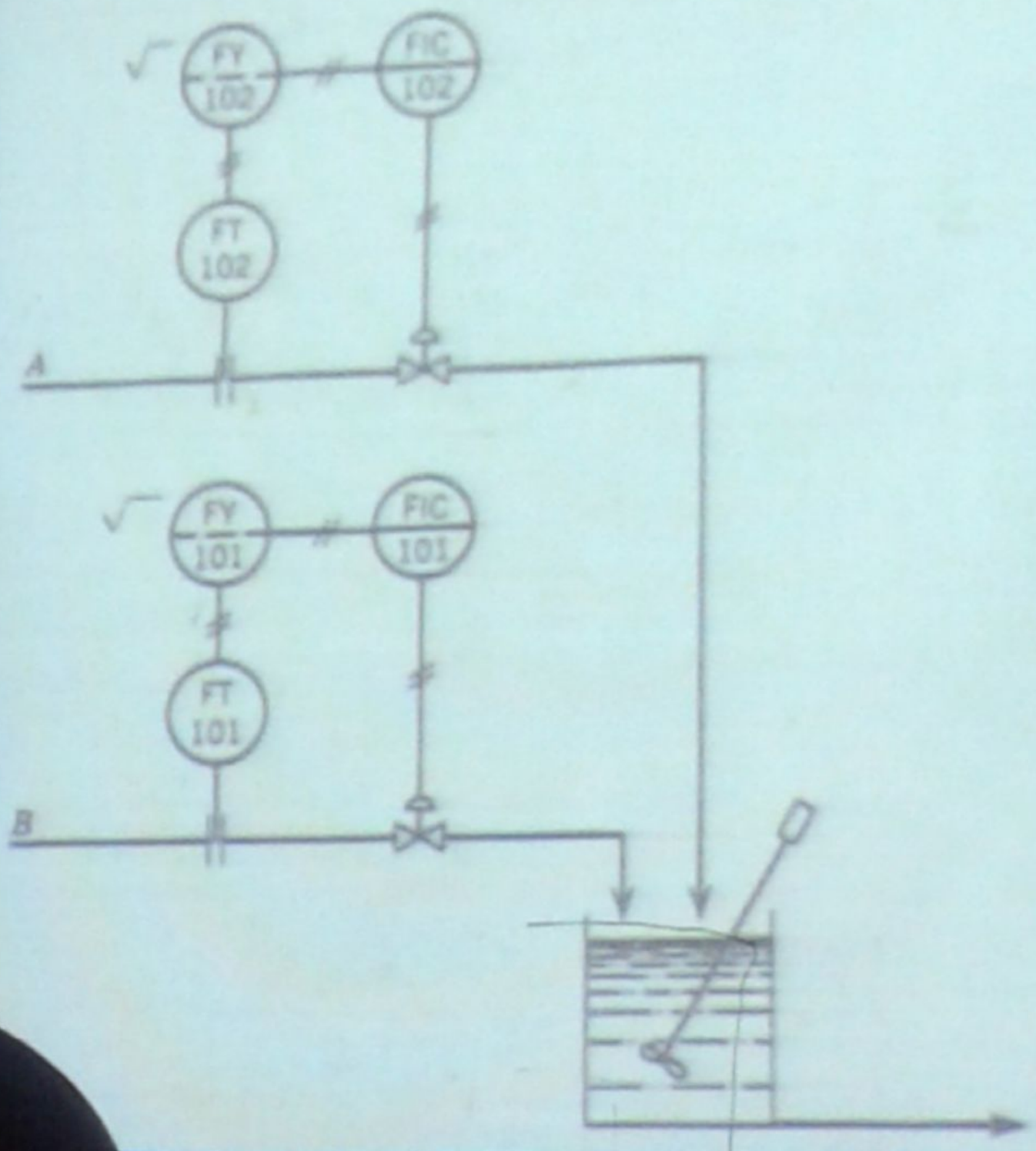


Boiler Drum Control

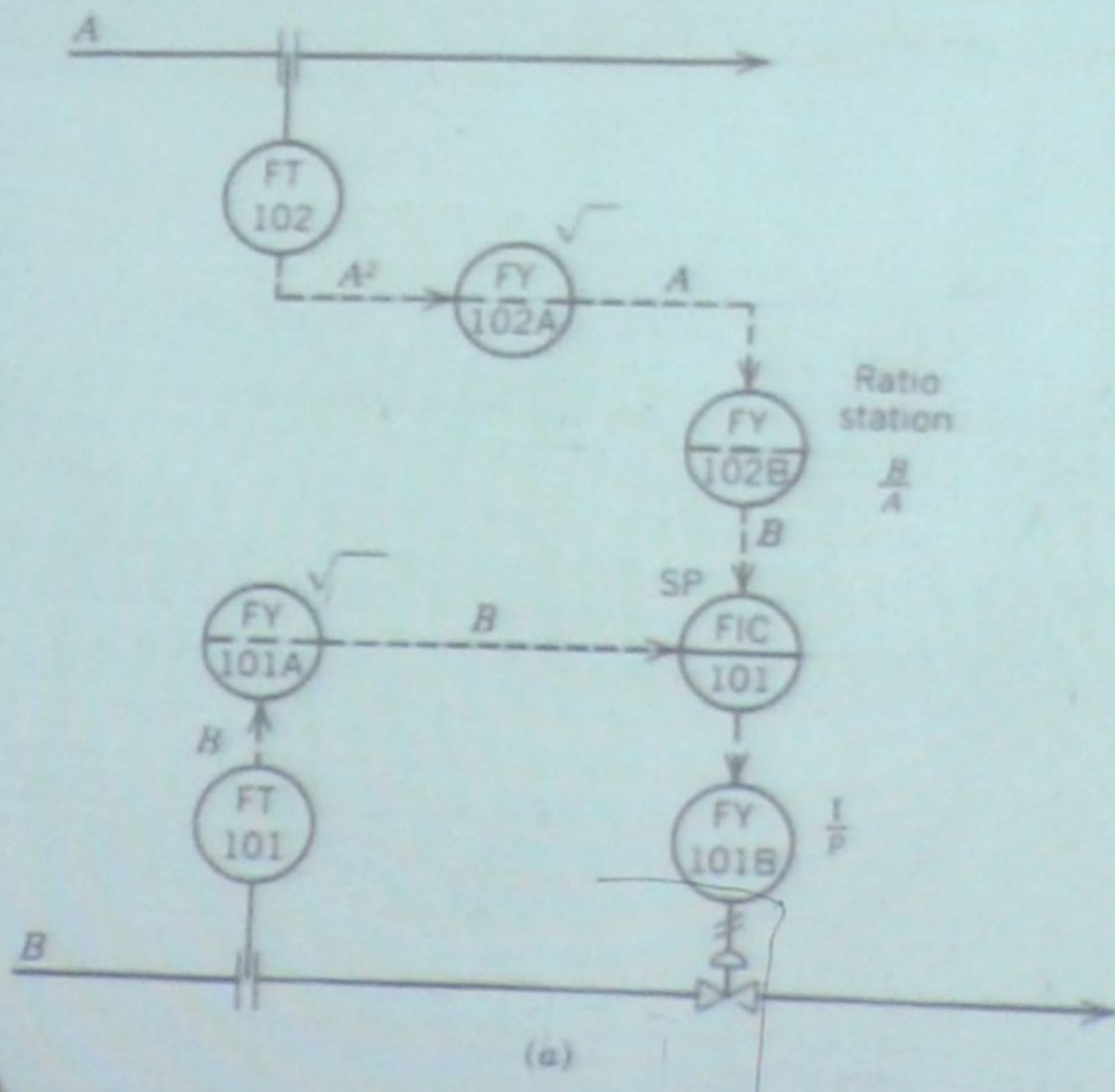
"Two-element control" scheme



An easy way



“wild flow”

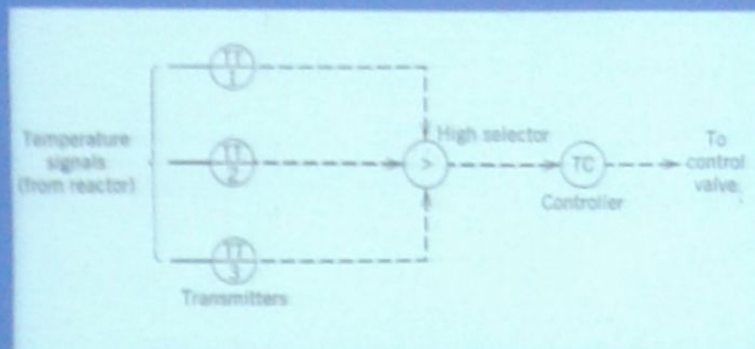


Selective Control / Override Systems

- Most process control applications have an equal number of controlled variables and manipulated variables.
- For control problems with fewer manipulated variables than controlled variables, selectors are employed for sharing the manipulated variables among the controlled variables.

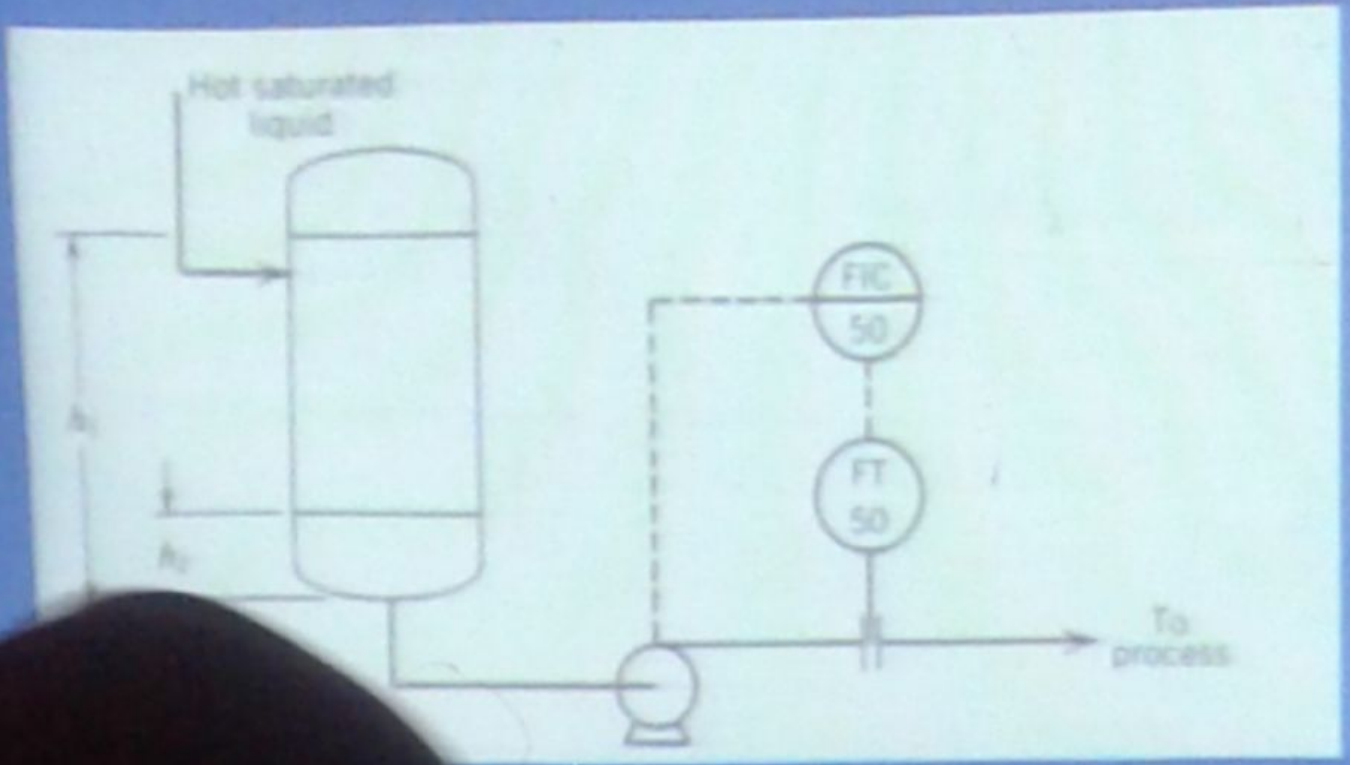
HP Audio Switch

Selectors

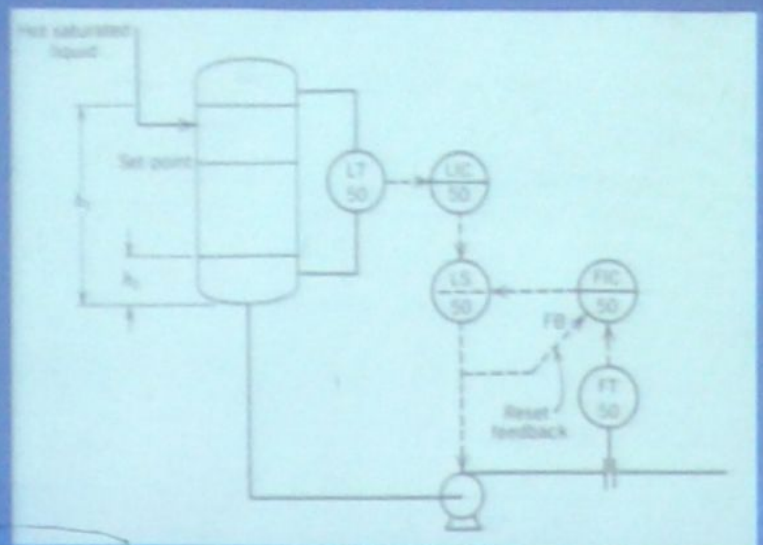
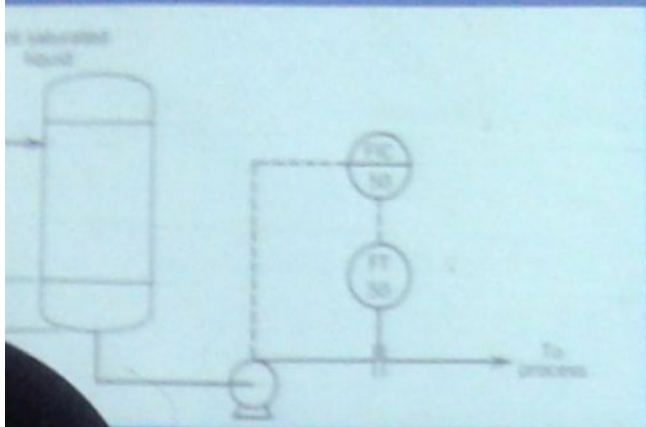


Control of a reactor hotspot temperature by using a high selector

- In this reactor application, the output from the high selector is the input to the temperature controller. In an exothermic catalytic reaction, the process may “run away” owing to disturbances or changes in the reactor, and immediate action should be taken to prevent a dangerous rise in temperature. Because a hotspot can potentially develop at one of several possible locations in the reactor, multiple (redundant) measurement points are employed. This approach helps identify when a temperature has risen too high at some point in the bed.



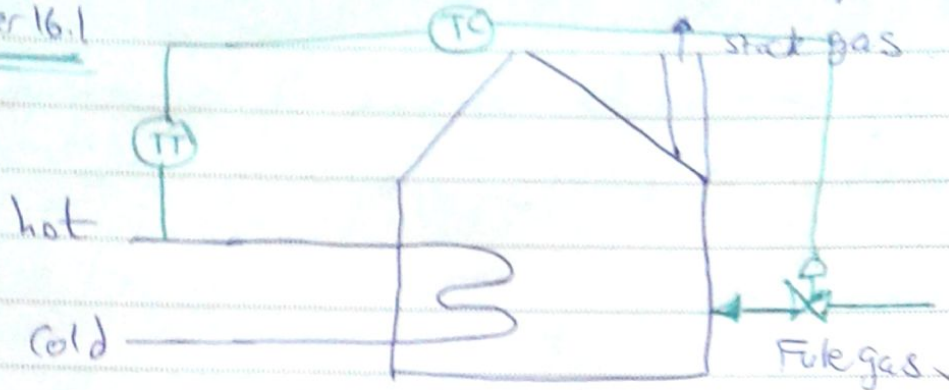
Override Control Systems



HP Audio Switch

Simple single Feed back control loop.

Figure 16.1



صباحاً انیٹر وٹ ریگنٹیکون فرمیکہ ؟
 -- stock gas !! کیا ہوگا اس کے ساتھ اس کے Line سے لے کر

• یہ مسئلہ کاغذ پر ہے نہ ال Flow rate کا ہے Fuel gas کو

منا خط کا ضابطہ n Utility stream سے اس کے ساتھ لے کر
 باقیہ - بالائی شکل اختیار ہے، یعنی

* محاسبہ کرنا ناسی باقیہ انما، Valve

$$F = C_v f(x) \sqrt{\frac{\Delta P}{\rho}}$$

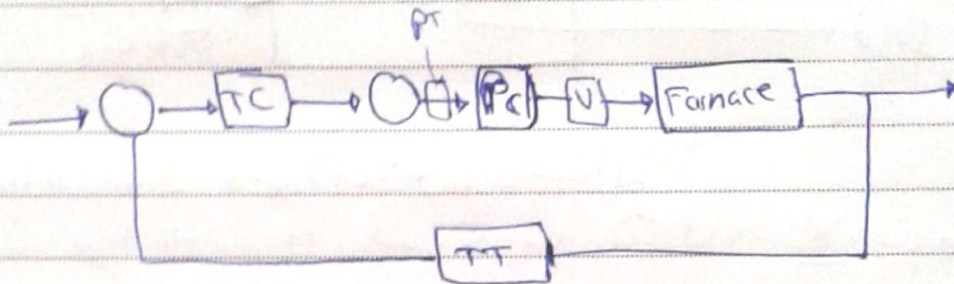
 mechanical Valve
 coefficient Openity

• اس کے ساتھ Flow پر pressure ← pressure
 cascade controller must have ↓

- # two controller and it's connected together one controller is putting the set point to other.
- # two transmitters
- # one control valve

why we might need cascade controller?

if any manipulated variable is subject to deviation or probably subject to variation.



5-12-2017

محاضرة التحكم

لماذا نحتاج إلى متحكم متتابع؟

إنه أفضل كونه يدير level رافد boiler أفضل من
إنه أفضل كونه يدير level رافد boiler أفضل من
لأنه يدير level رافد boiler أفضل من

المسألة بال steam ← disturbance " variable " steam stream
① pressure → multi unit used steam → P ↓
→ block in line or no unit "just boiler" → P ↑

مناظره ال pressure → اکیم اکنام بر ال bubble نیز به
 → ال action منع ال controller → قتل ال Feed
 → کتبه ایام الراضر آخل به فالشخر آکب
 و الیای برجه قتل ایام به و حیا امی یسر ال
 drum ~~فاز~~ فاضی

→ مشکله کسبه [swell/shrink]

→ اکل نازل Control ال pressure of steam stream
 → Feed Forward

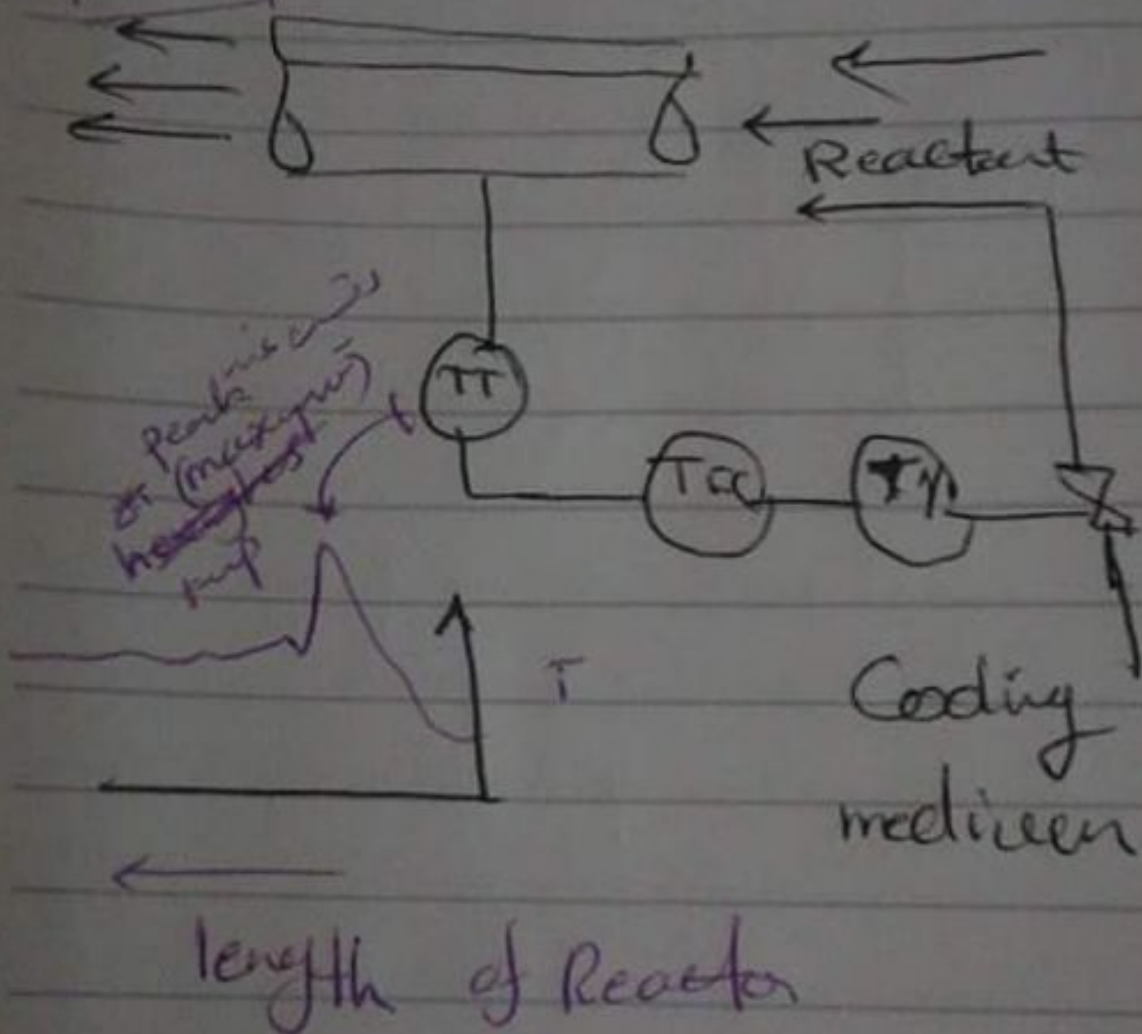
[Feed back word ← Feed Forward]

لازم تفقود ← mass ← لی مقابل کل 1 kg تیفر
 balance
 → ارنل 1 kg ماء #

10-12-2017

~~type~~

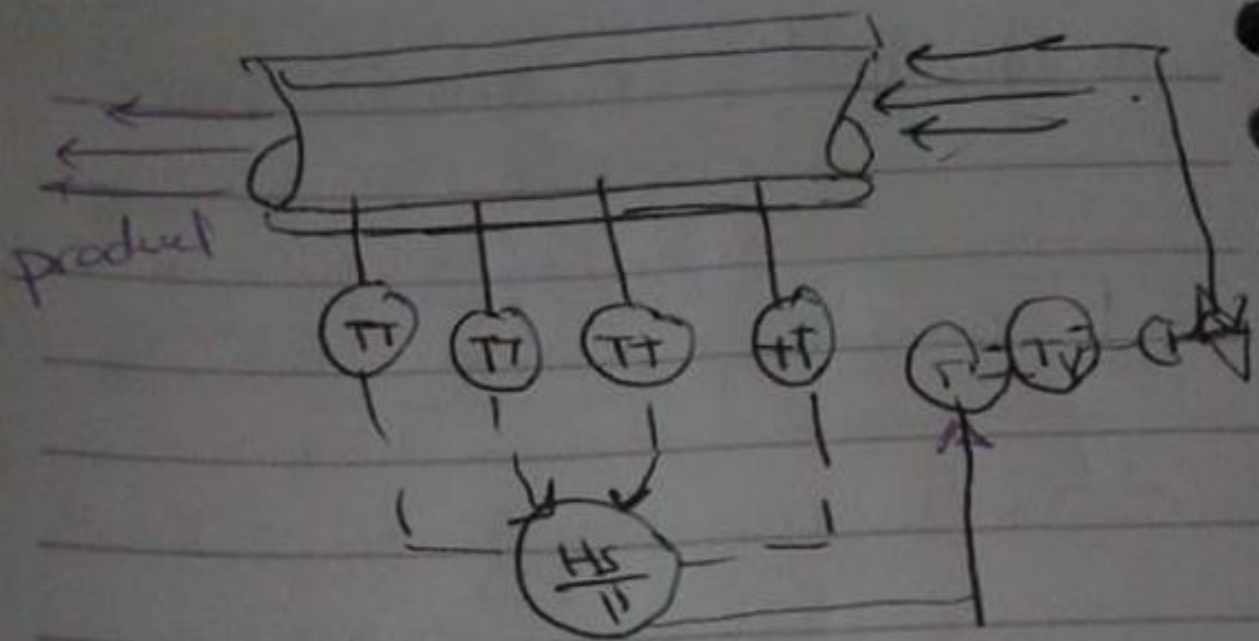
temp Control of a plug
flow Reactor;



⇒ temp profile

1.1.1.1.1.1.1

transfer bsv



من خواصها، وهو

maximum.

وإذا كان الـ (Reactor) في حالة

Selective Control

في هذه الحالة، النظام يعمل على التحكم في المتغير المطلوب فقط، بينما المتغيرات الأخرى تتحكم فيها بطريقة أخرى.

Sample Control

في هذه الحالة، النظام يعمل على التحكم في المتغير المطلوب فقط، بينما المتغيرات الأخرى تتحكم فيها بطريقة أخرى.

في هذه الحالة، النظام يعمل على التحكم في المتغير المطلوب فقط، بينما المتغيرات الأخرى تتحكم فيها بطريقة أخرى.

as chemical engineering

المهندسين الكيميائيين

في الهندسة الكيميائية

! Curve loop

المركبات المختلفة

S length

المركبات

→ Catalyst

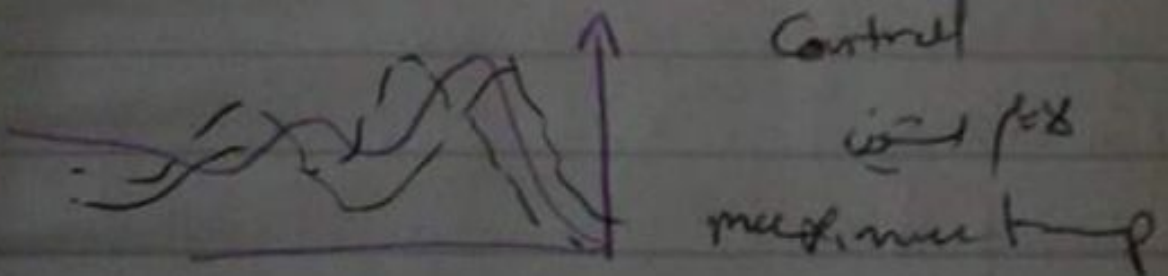
The Catalyst (de activation)

المركبات

المركبات profile

المركبات في واحد

Control



temp

[Sensor]

pressure Control

10-12-2017

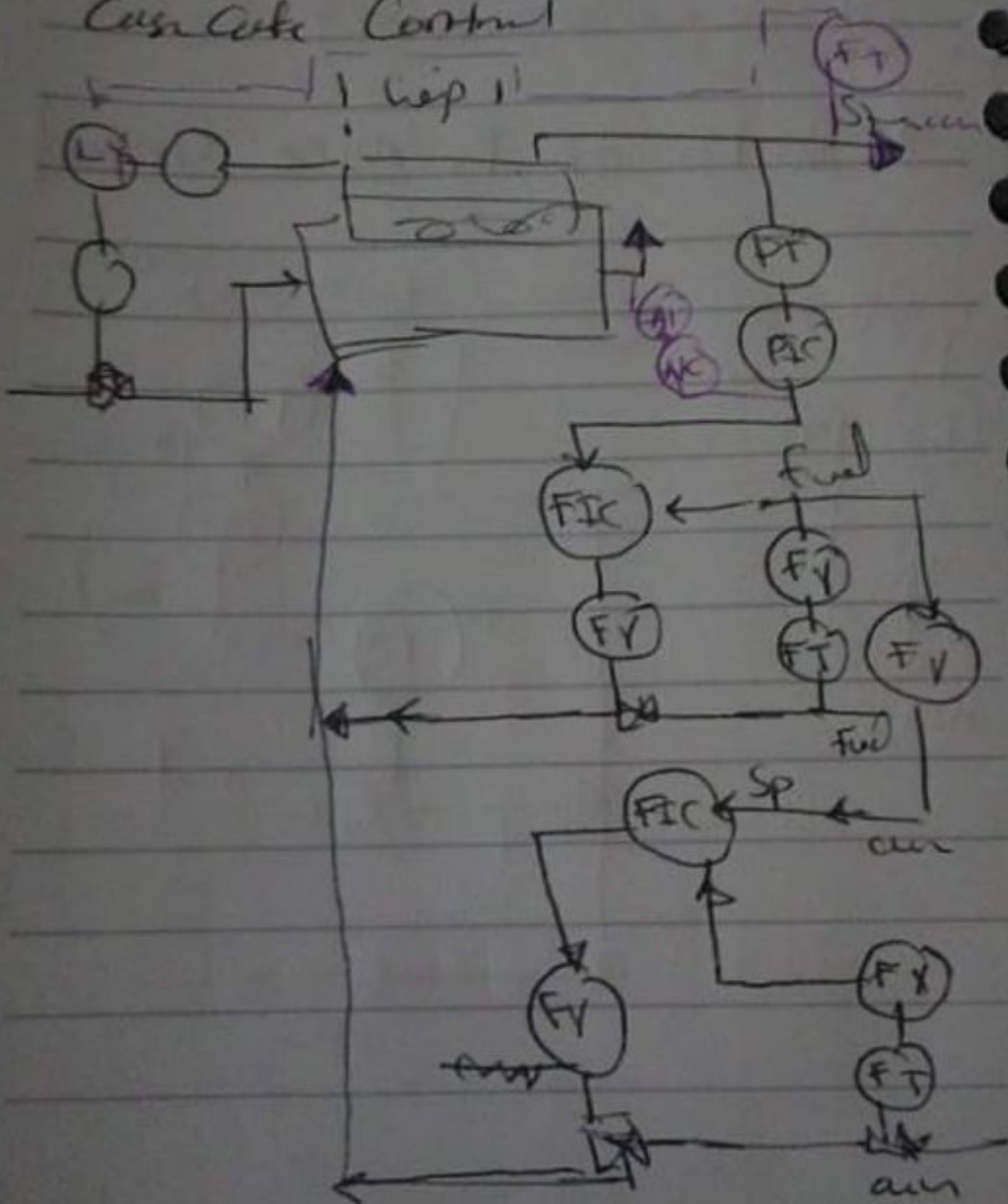
in pressure

2. air flow

3. air flow

Cash Control

1. step 1

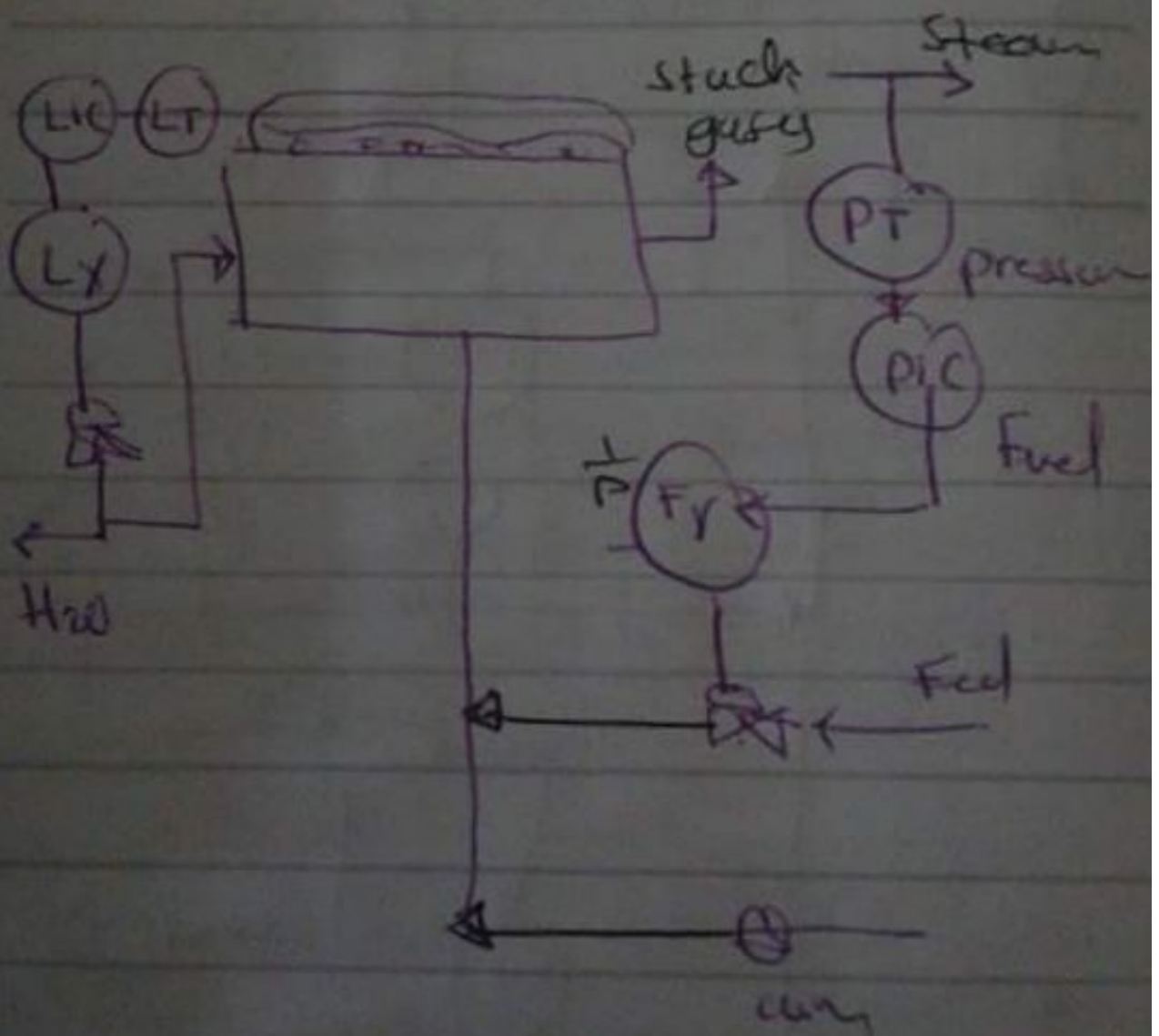


as, ~~introduction~~ selective ~~high~~ ~~low~~ ~~control~~

! ~~high~~ ~~low~~ ~~control~~

As process engineer?

* Boiler or Furnace Control



نقطه (02)

[Lagrange]

ادخل حوض وادخل Fuel

لقد دخلت Fuel وادخل

لقد دخلت (نقطة) !!

نقطة Control في البداية

أو 11 Fuel

نقطة (02) في البداية

نقطة 11 Fuel في البداية

نقطة 11 Fuel في البداية !!

* Optimization

Control

نقطة 11 Fuel

نقطة 11 Fuel Concept

[17 - 19 - 20]

16

1. କେଉଁ ପଦ୍ୟର ଲକ୍ଷଣ ଅଟେ ?

Sys 3 destirbungen

pressure 11, Controlle

↓ Jo press ↓ Eject

→ ~~Cost~~ ↑ Flow ~ ↑ Fuel

[aɪn] 1. to be =

اول پیشی بخور ایم و بعد

Temp $\downarrow \rightarrow \uparrow$ Fuel $\rightarrow \downarrow$ Pressure

→ Fuel ↓
out ↓

↓

فول
اوت

1. Combustion :-

↓ $\bar{u} \bar{v}$

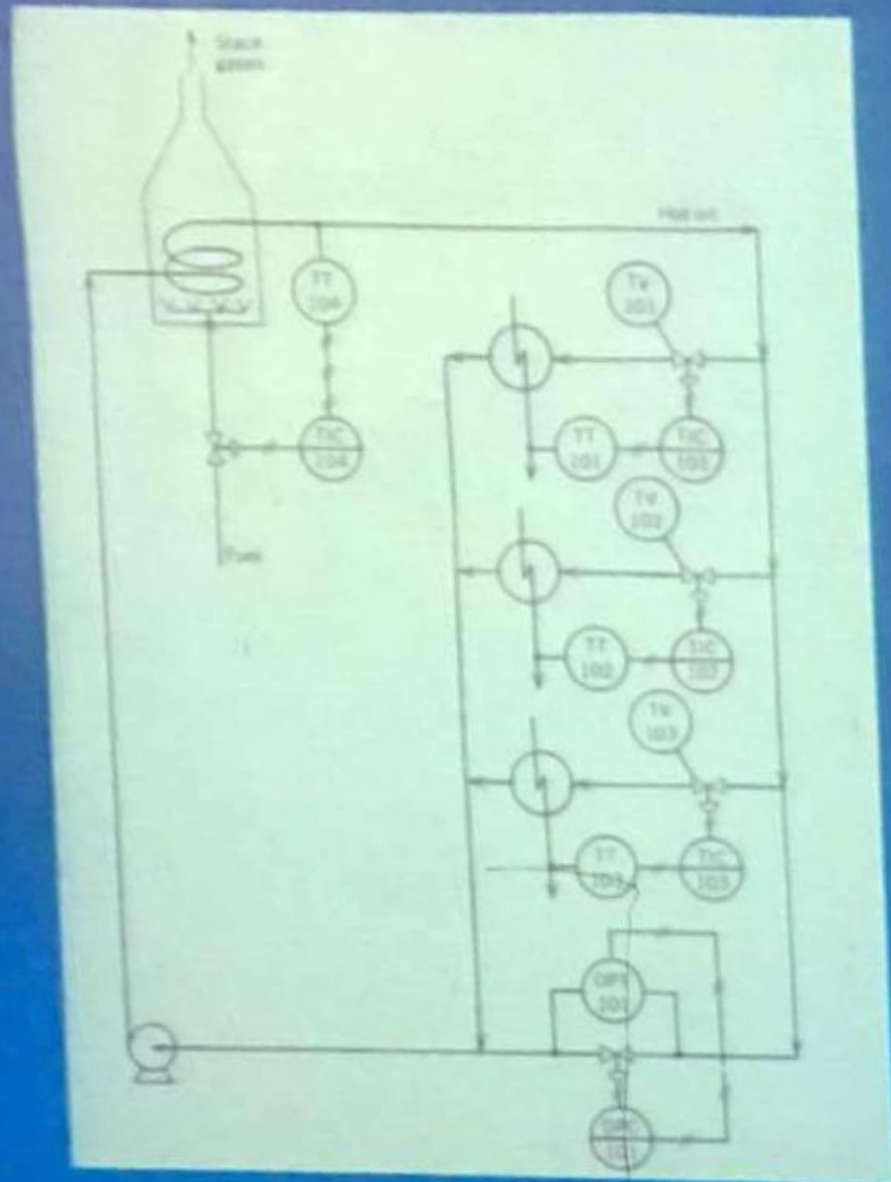
ایسی ایک قدرت ہے!

۱۹

← لا یفنی شیء من لدن اللہ وکونہ کما

تسببوا لا تفرقوا! (التي ظهر لنا أمير المؤمنين عليه السلام)

Optimization Control





يوم الثلاثاء 2017-12-12

”الدكتور عرضلنا تقرير طالب ”

وحكا شوي عن الادابت كونترولر للاسف ما كتبت ولا

صورت

الخميس 2017-12-14 كان لاي استفسار عن المادة

والأحد 2017-12-17 كذلك و بعدها انتهت

المحاضرات